माईनिंग प्लान नागपुर द्वारा अनुमोदित

एसईसीएल कोरबा क्षेत्र के बगदेवा भूमिगत परियोजना(कोयला उत्पादन क्षमता 0.75 मिलियन टन(नोर्मेटिव) एवं 0.76 मिलियन टन(पीक) प्रति वर्ष) का माईनिंग प्लान की प्रति पृष्ट. क्र. 52...में संलग्न है। जो कि सेंट्रल माईन प्लानिंग एंड डिजाइन इन्स्टीच्यूट लिमिटेड(सीएमपीडीआईएल- भारत सरकार का एक उद्यम) द्वारा प्रस्तुत किया गया है एवं कोल ईंडिया लिमिटेड बोर्ड आफॅ डायरेक्टर द्वारा अनुमोदित है।

प्रान प्रबंधक बगदेवा भूमिगत खदान

ाठ-४-२५ सर्वेक्षण अधिकारी बगदेवा भूमिगत खदान

उपक्षेत्रीय प्रबंधक ढेलवाडीह—सिंघाली—बगदेवा उपक्षेत्र वनमण्डलाधिकासी कटघोरा वनमण्डल, कटघोस

क्षेत्रीय महाप्रबंधक एसईसीएल कोरबा क्षेत्र



The information given in this report is not to be communicated to the press or to any person not holding an official position in the CIL/Government

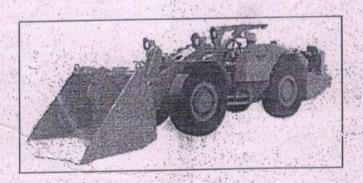
REVISED PROJECT REPORT FOR

BAGDEWA UG MINE

(Capacity-0.75 Mty)

(Job No.-501085)

KORBA AREA
SOUTH EASTERN COALFIELDS LIMITED



REGIONAL INSTITUTE-V
CENTRAL MINE PLANNING & DESIGN INSTITUTE
SECL COMPLEX, SEEPAT ROAD, BILASPUR
CHHATTISGARH, PIN – 495 006

SOUTH EASTERN COALFIELDS LIMITED, SEEPAT ROAD, BILASPUR (CG)

RLE NO SECLIBSP/196BMEXT/11/476

DT 5-4/11

EXTRACT OF THE MINUTES OF THE 196th MEETING OF THE BOARD OF DIRECTOR OF SOUTH EASTERN COALFIELDS LIMITED HELD ON FRIDAY THE 25th MARCH, 201 AT 11:30 A M AT THE REGISTERED OFFICE OF THE COMPANY AT SEEPAT ROAF BILASPUR (CG)

ITEM NO. 196:4:15

Sub Revised Project Report for Bagdeva UG Mine (0.75 MTY)

The Board approved the Revised Project Report (0.405 Mty. to 0.75 Mty.) for Bagdeva U. Mine of Korba Area, at an additional capital of ₹ 87.12 Crores, as recommended by the Technical Sub-Committee of SECL at its 30th Meeting held on 10.03.2011 at Bilaspur.

COMPANY SECRETAL

Distribution

- 1 CGM(P&P)
- 2 GM, KORBA AREA

CC

D1(P8P)

REVISED PROJECT REPORT FOR BAGDEWA UG

CONTENTS

CHAPTER	PARTICULARS	PAGE NO.
	List of Contents	C/1 - C/3
	Summarised Data	SD/1 - SD/6
1	Introduction	1/1 – 1/6
11	Marketability & Justification	11/1 - 11/2
III	Project Site Information	111/1 - 111/2
IV	Geology & Deposit Appraisal	IV/1 - IV/19
٧	Mine Boundary, Reserves & Mine Life	V/1 - V/3
VI	Mine Entries	▼ VI/1 – VI/2
VII	Mining Strategy	VII/1 - VII/6
VIII	Method of Mining	VIII/1 - VIII/10
IX	Mining Schedule	IX/1 - IX/5
X	Underground Transport System	X/1 - X/3
XI	Mine Ventilation	XI/1 - XI/4
XII	Water Management, Pumping & Drainage	XII/1 - XÎI/3
XIII	Coal Handling Plant & Despatch	XIII/1 - XIII/2
XIV	Mine Facilities	XIV/1 - XIV/3
XV	Power Supply, Illumination & Communication	XV/1 - XV/13
XVI	Civil Construction	XVI/1 - XVI/6
XVII	Manpower, Productivity & Training	XVII/1 - XVII/2
XVIII	Safety & Conservation	XVIII/1 - XVIII/6
XIX	Environment Management	XIX/1 - XIX/9
XX	Mine Closure Planning	XX/1 - XX/3
VXXI	Project Implementation Schedule (Land)	XXI/1 - XXI/2
XXII	Financial Evaluation	XXII/1 - XXII/6
ppendices		AN/1 - AN/45

REVISED PROJECT REPORT FOR BAGDEWA UG LIST OF APPENDICES

Appendix No.	Particulars	Page No.
STATEMENT S	SHOWING THE	
Α	HEAD-WISE TOTAL CAPITAL INVESTMENT FOR THE MINE	AN-1
A.1	ESTIMATED ADDITIONAL CAPITAL INVESTMENT ON LAND	AN-2
A.2	ESTIMATED TOTAL CAPITAL INVESTMENT ON CIVIL WORKS	AN-3
A.2.1	ESTIMATED CAPITAL INVESTMENT ON SERVICE BUILDINGS	AN-4
A.2.2	ISTIMATED CAPITAL INVESTMENT ON RESIDENTIAL BUILDINGS	AN-5
A.2.3	ESTIMATED COST INDEX FOR CIVIL WORKS	AN-6
A.3	ESTIMATED TOTAL CAPITAL INVESTMENT ON PLANT & MACHINERY	AN7-AN9
A.3.1	ESTIMATED CAPITAL INVESTMENT ON ELECTRICAL P & M	AN-10
A.3.1.2	ESTIMATED PHASED CAPITAL EXPENDITURE ON ELECTRICAL P & M	AN-11
A.3.2	ESTIMATED CAPITAL INVESTMENT ON WORKSHOP P & M	AN-12
A.3.2.1	ESTIMATED CAPITAL INVESTMENT ON UNIT WORKSHOP P & M	AN13-AN14
A.3.2.1 (a)	ESTIMATED CAPITAL INVESTMENT ON ELECTRICAL P & M	AN15.8-AN1
A.3.2.2	ESTIMATED CAPITAL INVESTMENT ON PROJECT SITE P&M	AN20
A.3.3	ESTIMATED CAPITAL REQUIREMENT FOR PUMPS, PIPES & FITTINGS	AN-21
A.3.4	ESTIMATED CAPITAL INVESTMENT ON CHP	AN-22
A.4	ESTIMATED CAPITAL INVESTMENT ON FURNITURE & FITTINGS	AN-23
A.6	ESTIMATED CAPITAL INVESTMENT ON VEHICLES	AN-24
A.7	ESTIMATED CAPITAL INVESTMENT ON PROSPECTING & BORING	AN-25
A.8.1	ESTIMATED CAPITAL OUTLAY IN MINES	AN-26
A.8.2	ESTIMATED CAPITAL INVESTMENT ON ROADS & CULVERTS	AN-27
A.8.2.1	LISTIMATED CAPITAL INVESTMENT ON COLONY ROADS	. AN-28
A.8.3	ESTIMATED CAPITAL INVESTMENT ON WATER SUPPLY ARRANGEMENT	AN-29
A.8.3(a)	ESTIMATED CAPITAL INVESTMENT ON SEWAGE DISPOSAL SCHEME	AN-30
A.8.3(b)	ESTIMATED CAPITAL INVESTMENT ON WATER DEMAND CALCULATION	AN-31
A.8.4	ESTIMATED CAPITAL INVESTMENT ON EMP	AN-32
В	ESTIMATED JOB-WISE/CATEGORY-WISE REQUIREMENT OF MANPOWER	AN33-AN36
B.1	ESTIMATED CATEGORY-WISE MANPOWER & CALCULATION OF SALARY/WAGES	AN-37
C	ESTIMATED COST OF PRODUCTION PER TONNE OF COAL INCLD. EMP COST	AN-38
C.1	ESTIMATED COST & PROFITABILITY AT VARIOUS LEVELS OF PRODUCTION	AN-39
C.2	ESTIMATED ANNUAL EXPENDITURE ON EMP & IMPACT OF COST/TE ON COAL	AN-40
C.3	SENSITIVITY ANALYSIS AT DEFERENT LEVELS OF CAPACITY UTILISATION	AN-41
D.1	ESTIMATED NET REVENUE CASH OUTFLOW AT 100% LEVEL OF PRODUCTION	AN-42
D.2	ESTIMATED NET REVENUE CASH OUTFLOW AT 85% LEVEL OF PRODUCTION	AN-43
E.1	CALCULATION OF FINANCIAL IRR OF THE MINE AT 100% LEVEL OF PRODUCTION	AN-44
E.2	CALCULATION OF FINANCIAL IRR OF THE MINE AT 85% LEVEL OF PRODUCTION	AN-45

REVISED PROJECT REPORT FOR BAGDEWA UG

LIST OF PLATES

		Scal	e
	Particulars	NTS	5
Plate No.	Location Plan	1:500	00
	a Larical Plan / Surface Plan	1:500	00
	In the stion Dian - (7-11) I Ocalit	1:50	00
111	Panel Projection Plan – G-III B Seam Panel Projection Plan – G-III B Seam	1:50	00
	Panel Projection Plan – II A Seam	1:60	_
٧	Panel Projection Flan	NT	_
VI	LAND USE PLAN Lithologs / Seam Structure of Boreholes	11.1	_
VII	Lithologs / Seam Structure of Barrier		

RPR OF BAGDEWA UG (0.75Mty)

SUMMARISED DATA

SI. No.	Particulars	Unit	Value
Α.	GENERAL Þ		
1	Name of the Report		RPR of Bagdewa UG
2	Mining Area		5.02 sq. km
3	Nearest Railway Station from project	Name km	Gevra Road Railway Station at a distance of 20 Km from Katghora
4	Nearest National / State	Name	Bilaspur Katghora State
	Highway / Approach road	km	Highway.
В.	GEOLOGICAL		
1	Name of geological blocks considered	Name	Bagdewa block
2	Area of the geological blocks	sq. km	10.54 Sq. Km.
3	Borehole Density within blocks	BHs / sq. km	10
4	Description of all coal seams within block		
Bernst	Name of seam	Thickness-range (m)	No. of borehole intersections
ALTERIAL AND	Seam	Add to the	
	G-V	0.10-2.29 (<1.5m)	36
Letters by	Parting	12.27-26.9m	
	G-IV	1.4-2.65	51
etma si	Parting	33.65-50.60	
	G-III (Top)	0.25-3.05(<1.8)	64
	Parting	0.60-15.07	,
	G-III (Bottom)	0.45-7.0	82
	G-III (Comb)	4.74-7.0	
	Parting	1.27-28.0	
BIG INTERNAL	G-II A	0.1-2.64	63
	Parting	17.25-41.00	
	G-II	0.07-0.77	
	Parting	16.74-30.26	
	G-I	0.12-1.35	

C.	TECHNICA	L			-	5.026 sq. km		
1	Area of the	proposed m	ine		-		Hs/sq. km	
2	Borehole density within mine area				-	IU Br	13/34. 1411	
3	Mine paran	eters (seam	1-wise)			1.48-2.18Km		
Ext		vtent along s	strike (m	in. – max.)		1.71 km	
	Ŷ.	Extent ald	ong dip (min,-max.)	3.4-	1.71 KIII	
	Description	of coal sea	ms propo	osed to be	0.83			
4	worked						Extractable	
Name of seam	Mining	Thicknes	Av.	Av.				
Name of Seam	Area	s range	Thick	Grade		dient	(Mt)as on	
	(sq. km)	consider	ness	(UHV/	11	n)	1.4.10	
		ed (m)	(m)	GCV)	4	n16	1.29	
G-III T	1.35	1.5-3.5	2.0	В		n16	5.923	
G-IIIB	5.026	1.5-3.5	2.5	В	-		2.266	
G-IIA	2.50	1.5-3.5	2.4	В	_	in16	Purpose	
Entries Na		Size		Gradien vertica			Fulpose	
Existing Mine Ent	ries	No. 1		herona a	116		Main Intake	
Incline No. 1		4.2x 2.5	4.2X 2.3X104		1 in 4		Belt/coal transport	
incline No. 1					Selection of the least	Main intake		
Incline No. 2		4.2x 2.5	4.2x 2.5x164 1 in 4			Traveling/ Haulage roadway		
ITICITIE 140. 2								
				Vertica	1	Madi	Main Return	
Air Shaft	1.00		5.0 m		1	airways .		
	SET NO.	Diax4	5m	-				
Existing undergr	ound drivage	40-	-	1 in 4		0	SIIA to GIIIB	
Drift No.1		40r	n	1 111 -1		Inta	,Intake & Travelling	
	HAPPEN SE	100	7	1 in 4		1	SIIA to GIIIB	
Drift No.2		401	40m 1 in 4			,Inta	ake & Haulage	
		5.0	m	Vertical			Return	
Staple Pit (16L	/2D)	Dia.X				2		
	,	5.0		Vertical			UG Bunker	
Staple Pit (261	JZD)	- 12	Dia.X1#m		WATE.			
	/Chan	5.0		Vertical			UG Bunker	
Staple Pit (431	Jeu)	Dia.X					Faults	
Proposed Underground		ind To c	Turo		000	101	Faults	
Proposed	Onderg. o				-	11-	ulage / Materia	
Drivage Drift 1 & 1A		4.2x 2	4.2x 2.5X25 1 in		1 in 5		ansport /Intake	
Dill To 17	The state of the				F	ura	Intake	
Drift 2 & 2A	2 12 1 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4.2x 2	.5X25	1 in	5	air	rway/Travelling Roadway	
	to the	1000	5 EV25	1 in	5	Ins	seam Return	
Drift 3 & 3A		ANN DESCRIPTION OF THE PERSON NAMED IN COLUMN 1	2.5X25	Verti			Main Intake	
Air Shaft			5.0 m Diax45m *		Vertical		airways	

Job No.501085

SD-2/6

RPR Bagdewa UG(0.75 Mty)

Strata Bunker (100t)	10mx	2 Vertical	100	al Bunkerage	
6	Method of Mining		7		
7	Panel Parameters		6	Nos.	
I	No of headings in	each panel		1.2 m	
	Size of galleries	/roadways	26m x 26m		
		Pillar sizes			
8	Production Param	neters	TO THE REAL PROPERTY.	Nos.	
0	No of panels to	o be worked		60 TPD	
	Production from	each panels		.75Mty	
9	Target Output		· ·	. 7 Sivily	
9	Normativ	e production	0	.75Mty	
	capaci	ity (at 100%)		.76 Mty	
	Peak product	ion capacity.).64Mty	
	Production capa	city (at 85%)	II Voorli o	year of LHD/UDMs	
10	Year of achieving	Target	If Year(i.e)	roduction)	
10	Production		ulu	Oddonony	
CHARLES OF THE PARTY OF THE PAR	(from zero date)		Mt		
11	Production Phasi	ing (from			
	zero date up to ta	arget year)	Year 3		
Year /	Year 1	Year 2			
Coal Seam		(Target Yea	0.75		
G-III (TOP/ BOT.)	0.62	0.75	0		
II A				13Years	
12	Total Mine Life	distion	E CONTRACTOR		
	(at Normative p	roduction			
	capacity)				
	0	struction perio	od 1Year		
Maria San	Con	build-up perio			
	&Production	roduction perio	od	11 Years	
	Tanoring	/ mine closure		1Year	
	Tapening	riod			
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Degree of Gass	siness (1/11/1	11)		
13	Major Equipme	ent Deployed in	1	Nos.	
14		ill Doping		1000	
	panels	LI DIE LI	HD	7+3	
		UI	DM .	4+4	
	Average Speci	ific Energy		15.83 kWh/t	
15	Consumption			1104 Nas	
-	Total Manpow	er	TO THE LIE	1121 Nos.	
16	Total Manpon	EXIS		1027 Nos.	
25		Additio	nal	94 Nos.	

Job No.501085

		The second secon
	(FIRR)% At 100% production level At 85% production level	692.30 528.85
12	Desired average Selling Price to yield 12% FIRR At 100% production level	Rs1357.63 / tonne
	At 85% production level	Rs1550.99 /tonne
13	Break-even point Production Production level	0.23 Mty 31.42 %
14	Mine Closure Cost (for corpus fund)	683.99 Lakhs
15	Expected Completion Capital	Rs.122.01 Crores

XXXXXX

TEXT

CHAPTER-I

INTRODUCTION

1.1 BACKGROUND OF THE PROJECT REPORT

The Original Project Report for Bagdewa Underground Mine (0.24 Mty) was prepared in February, 1995 and subsequently approved by SECL Board. The Project Report envisaged exploitation of the G-III top, G-III Bottom & G-II A seam in an area of about 3.03 Sq. Km (These seams were earlier nomenclature as G-IV, G-III top & G-III bottom). Later on a scheme was formulated by area for incremental production of 0.242 Mty over RPR (0.405Mty), March, 1999., in July, 2007 covering an area of 4.69 sq. k.m. This RPR is being prepared for incremental production of 0.345 Mty over previous RPR (0.405Mty), March, 1999.

Summary of the earlier approved Project Reports and RPR, Dec 2010, of the mine is as shown in the table below:--

SI. No.	Particulars	OPR (Feb 1995)	RPR (March 1999)	RPR (Dec 2010)
Α.	Mining Parameters	O W T	G-III T	G-III T
1.	Seams to be worked	G-III T G-III B G-II A	G-III B G-II A	G-III B G-II A 9.475
3.	Extractable Reserves (Mt)	9.58 with	B&P with	(as on 01.04.10) B&P with
4.	Method of work	B&P with manual loading	SDL, Pony, conveyor	LHD,UDM and belt conveyor
5.	Mine Entries	2 inclines and an air shaft	2 intakes and 1 return incline	2 inclines and one air shaft as intake and a return air shaft
6.	Targeted Production (Mt)	0.24	0.405	0.75
7.	Mine life (years)	44	35	13

B.	Financial Parameters		1-10 22 3	44700.00
1.	Total Capital (Rs.	1858.89	3845.92	11760.28
2.	Specific Investment (Rs/t)	774.52	949.61	1568.03
3.	P&M Capital (Rs. Jakhs)	765:46	2116.17	4294.27
4.	P&M Capital (Rs/t)	318.94	522.51	. 572:57,
	Cost of Production	name (in the seal)		
a)	At 100%	472.95	677.12	1301:59
b)	*At 85%	544.14	777.05	1483.38
6.	Selling Price (Rs/t)	563:54	808.20	.3658,03
7.	Profit (Rs/t)		The United States	W Washington
a)	At 100%	90.59	131.08	2356.44
b)	At 85%	19.40	31.15	2174.65
8.	IRR			NOTE AND ADDRESS.
a)	At 100%	21.79	45.06	692.30
b)	At 85%	- 197/ed s	21.03	528.85

This RPR has been prepared with a view to enhance the production and further increase profitability of the mine by introducing high capacity LHD and UDM and provision for acquisition of land with all rights as statutorily required for depillaring for abiding by DGMS compliance.

1.2 EXPLORATION STATUS

1.2.1 HISTORY OF MINING IN THE BLOCK :-

Bagdewa Geological block (part of Dilwadih Block, GR prepared in 1985) covers an area of about 10.54 Sq. Km. The original underground PR (0.24 Mty) was prepared on the basis of geological note prepared in August, 1994. Later on, a small OC patch (23 Ha) in the north-western part of OPR has also been planned for 0.20 Mty Production which will be liquidated after closure, of UG working. The Revised Project Report for Bagdewa Underground mine was approved on 21.07.1999 for a production capacity of 0.405 Mty. Bagdewa RPR is a completed project. The date of completion is 31.03.2006.

I-2/6

1.2.2 RECENT STUDIES:-

The detailed exploration has been carried out by CMPDI and DGM (MP) in different phases. In total 105 bore holes have been drilled in an area of 10.54 sq. km. The borehole density works out to 10 per Sq. km.

In view of large geological block area it is proposed to exploit the block in two units. In this RPR, i.e. Unit-I, the original mining boundary has been retained and area lying south of the Kholar nala and fault F7F7 would be annexed. The total mining area in Bagdewa UG will be about 476.88 sq. km.

1.3 MINING ACTIVITIES

The nearby mines in the block are Dhilwadih U/G and Singhali U/G. These are semi mechanized mines working with LHDs/ SDLs and belt conveyors.

1.4 JUSTIFICATION OF PRESENT REPORT

Bagdewa U/G mine is an existing mine and a completed project. This mine has potential to increase production. Earlier there was a prevailing practice to pay crop commensuration to the land owners these days; DGMS has been insisting, acquiring of land before allowing permission for depillaring. Therefore looking to the prevailing practice for procurement of land has also been provisioned. Total mining area, geological reserve and mine plan has not been changed against RPR,99 only addition of one district for increased production has been envisigaged alongwith needed infrastructure and capital provision.

1.5 SALIENT FEATURES OF PREVIOUS AND PRESENT REPORT

In the original Project Report and RPR (1999), G-III (Top), G-III (Bottom) & G-II A seams have been considered for exploitation. The Revised Project Report also envisages exploiting the same seams covering the same mining area. The lower limit of thickness will be 1.5m for deploying low height LHD. The reserves lying between 1.2 m to 1.5 m thickness will be exploited later if some suitable loading machine is proved successful under this thickness range. Bagdewa underground mine is a completed project .Mine is earning net profit since last 5 years.

The OPR had envisaged extraction of reserves by Bord and Pillar System with manual shoveling on face chain conveyors.

As per the latest guidelines issued by Ministry of coal, Finance Division, all the ongoing projects of SECL should have a minimum internal rate of return of 17% at 85% of capacity utilization. In view of this, the Original Project Report had been updated at base price of August 1997 and found it unfavourable due to low IRR. Subsequently, it had been decided to suspend

all the project activities till its financial viability is established by enhancing the project capacity or improving the project economics by improved technology.

The production capacity of Bagdewa Underground Mine was, therefore, revised with an objective to enhance the production capacity up to 0.405 Mty and introduce SDL / low height SDLs to have better productivity and economics. This leads to better return on investment and improved IRR. (RPR-1999)

The reserve statement of proposed mine as per RPR,99 in Rhase-I operation is given below:-

Seam	RESERVES IN MT.				
Jean	Geological (1,2-3.5)	Mineable (1.5-3.5)	Extractable (1.5-3.5)		
G-III T	4.93	2:20	1:29		
G-III-B	13.01	12.39	8496		
G-11-A	6.60	4:044	2.9		
G-1174	24.54	18,634	12.38		

The thickness-wise percentage reserves in Bagdewa Underground Mine area is given as follows:-

2 -
% Reserve
12.13
19.44
13.84
34.39
19.05
1.15

About 3.3 Mte of geological reserves would be available in thickness range of 1.2-1.5m.

1.5.1 The present and current Revised Project Report envisages to deploy extra low height LHD, standard height LHDs and high capacity LHDs (capacity -3cum.) as loading machine, UDMs for face and foof drilling for coal preparation and roof support respectively, gate and trunk belts to improve the transport system, productivity and over all economics of the mine.

From above table, it is inferred presently that major area of the project (about 80% of reserves) offers deployment of low height LHDs and standard height LHDs.

In view of above; the production target of Bagdewa is revised at 0.75 Mty. The revised extractable reserves work out to 9.475 Mt. The mine life with a target production of 0.75 Mty works out to 13 years including development and tapering period.

Job No: 501085

The estimated capital requirement in the present Revised Project Report is Rs.117.60crore. Additional capital requirement will be Rs.87.12 crore. The Project will have an Internal Rate of Return of 528.85 at 85% production level.

The project is techno-economically viable and recommended for approval by the Competent Authority.

1.5.2 SALIENT POINTS OF REVISED PROJECT REPORT:-Salient parameters of the Project are as follows:

Particulars	Values
Target Production / Nominal Production Capacity (Mty)	0.75
Peak Production Capacity (Mty)	0.76
Manpower Requirement (Nos.)	1121
Output Per Man shift - OMS (t)	2.56
Earning Per Man shift - EMS (Rs.)	1631.32
Total Capital Investment (Rs. Lakhs)	11760.27
Additional capital investment (Rs. Lakhs)	8711.95
Specific Investment (Rs./t)	1568.03
Capital Investment on P&M (Rs. Lakhs)	4294.27
Specific Investment on P&M (Rs,/t)	572.57
Cost of Production (Rs./t) (at 100%)	1301.59
Cost of Production (Rs./t) (at 85%)	1483.88
Av. Selling Price (Rs./t)	3658.03
Profit (Rs./t) (at 100%)	2356.44
Profit (Rs./t) (at 85%)	2174.65
Break-even point (%)	31.42
Break-even production (Mty)	0.23
Financial IRR (at 100%)	692.309
Financial IRR (at 85%)	528.847
Desired Selling Price to yield 12% FIRR (at 100%)	1357.63
Desired Selling Price to yield 12% FIRR (at 85%)	1550.99

1.6 RISK / DIFFICULTIES & CONSTRAINTS IN MINING

The difficulties / constraints and risk associated are:

- Presence of village on the surface which has to be shifted and necessary provisions for Rehabilitation & Resettlement have to be made for acquiring the tenancy land before the start of depillaring operations in the mine.
- The parting in the overlapping portion of the G-III T seam and G-III B seam varies from 9.75m to 13.20m and near the boundary it is around up to 3.0m. The panel projections and the layout has been proposed keeping in the mind

superimposition of workings in the seams so that the cracks of lower seam do not propagate to the upper seam.

Large highly cultivated land on surface, which may pose difficultly in acquisition as in the present scenario the land owners are generally reluctant for giving up their rights just by payment of crop compensation.

1.7 PROJECT OBJECTIVES & TARGET BENEFICIARIES

The purpose / objective of the present report is to assess feasibility of increasing underground coal production with a view to further improve the profitability of the mine to contribute to the total coal production from SECL keeping in view overall demand of better quality coal. The coal produced from the Bagdeva UG project would be included in the basket linkages.

(a) Introduction of appropriate man-riding system

It has been envisaged to install man-riding system and the supplier of the system shall also maintain the system. A separate scheme for installation of man riding system has all ready been approved and the capital required has been included in this RPR.

(b) Increased Working Hours

With a view to reduce the arduous traveling distance, to increase working efficiency and working time, installation of man riding system will be highly beneficial during the working of mine.

(c) Equipment / Machinery

Details of requirement of equipment, as per technology suggested have been provided.

(d) Infrastructure Requirement

Modifications needed in the existing infrastructure like, transport, electrical layout, workshop, stores, coal handling etc has been provided.

(d) Manpower

Requirement of manpower-in the district and for the mine has been detailed in appendix-B with their job description.

Job No: 501085

I-6/6

CHAPTER-II MARKETABILITY & JUSTIFICATION

2.1 DEMAND, AVAILABILITY & DEFICIT IN SECL

The sector-wise coal demand for SECL is summarised in Table - 2.1. It may be seen from the table that against the present production level of 108.01 Mty. (2009-10) the total demand as projected for the year 2011-12 is 218.88 Mt. The projected production in the year 2011-12 is 128.85 Mt. resulting in to shortfall of 90.03 Mt.

Table 2.1

T	OTAL COAL DEMAND & AVAILAB	BILITY (SECL)
		(Figures in Mt)
SI. No.	Sector	XI Plan 2011-12
A.	COKING	
Α.	Steel (Indigenous)	0.14
В.	NON-COKING	A STERNING OF THE PARTY OF THE
1	Power (Utilities)	162.17
2	Power (Captive)	21.69
3	Sponge Iron / CDI	7.77
4	BRK & Others / LTC/SSF	3.00
5	Soft Coke	Dec 100 Hillshop
6	Cement	10.36
	Fertilizer	0.85
7 .	Colliery Consumption	0.02
8	E-auction	12.88
9	Total Demand (SECL)	218.88
	Availability	128.85
LUPSING TO	Balance	-90.03



Take a fine to the form to the fine to the fine that the fine to t

2.2 PRODUCTION SCHEDULE

The production schedule of Bagdewa UG is as follows:

Table-2.1: Production Schedule (Mty)

Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7
0.62	0.75	0.75	0.75	0.75	0.75	0.75

2.3 JUSTIFICATION OF OPENING THE PROJECT (ENHANCING PRODUCTION CAPACITY)

The Revised Project Report for Bagdewa U/G Mine has ben planned for a target production of 0.75Mty. The overall grade of ROM Coal from the Project is average grade B. From the above table it can be seen that the gap between demand and availability is -90:03 Mt deficits. As such, there will not be any problem in the off -take of coal from this project. In this project report production capacity has been enhanced keeping all the mining and geological parameters same.

2.4 LINKAGE

Coal from this project is not linked to any specific consumer. It will be included among basket linkages for miscellaneous consumers.

2.5 DESPATCH

It is proposed to sell the coal to miscellaneous consumers from the existing mine CHP. The coal is being presently transported from the CHP to Surakachhar railway siding (located 22.6 km from Bagdewa Mine) with use of tippers. The transportation charges for surface coal transportation from Bagdewa Mine to CHP has been considered as Rs. 61.61/t. respectively. Coal will be loaded into wagons at the railway siding. The cost of loading is included in the report.

Chapter - III

PROJECT SITE INFORMATION

3.1 LOCATION

Bagdewa U/G mine is situated in the Bagdewa block. This Block is situated in the Northwestern part of the Korba coalfield. Administratively, it is located in Korba District of Chattisgarh State. It falls in Survey of India Toposheet no.-64J/11(R.F. 1: 50,000). Bagdeva geological block is measuring 10.54 sq. km. The limiting geographic co-ordinates of the block are as under:

Co-ordinates:

Latitudes: 22° 22′ 34″ N to 22° 23′ 47″ (N) Longitudes: 82° 30′ 37″ E to 82° 33′ 35″ (E)

3.2 ACCESS

The block is located at an approximate distance of 1.5 Km East of Bilaspur-Katghora Road. The approach road to mine already exists. The mine is also approachable from Sutarra by Sutarra-Bagdewa Village road.

The nearest railway station is Gevra Road of SE Railway, at a distance of about 20 Km. Katghora is about 12 Km from Bagdewa Block.

3.3 CLIMATE

The area is characterised by tropical climate, seasons being well defined, summer from mid March to mid June, rainy season from mid June to September and winter season from October to mid March. May is the hottest month during which the temperature raises upto 48°C. In December (during the winter season) mercury falls to as low as 5°C.

3.3.1 RAINFALL

The average rain fall is about 1500mm. The maximum recorded rainfall within a period of 20 hrs, is 252 mm in September, 1973 in last 30 years.

- 3.3.2 The Relative humidity during monsoon ranges from 75-80% and in summer from 18 to 60%.
- 3.3.3 The wind direction is generally westerly to north- westerly, during monsoon, winter & summer, and varies from 5.4 to 8.3 Km/Hr,3.6-4.9 Km/hr and 5.7 to 8.1 Km / hr respectively.

3.4 MINE BOUNDARIES

North - Fault F9-F9 & 15m hard cover line of workable seams.

South - Kholar nalla later on Fault F7-F7 and its extension up to Fault F10 (3 m parting with Seam III top and bottom will follow the extension line).

West- 15m HCL of G-II A seam, working thickness (1.5m lying) and 40m against road to Amarpus village.

East - Fault F8, F10 & workable thickness line (1.5m) of seam.

3.5 TOPOGRAPHY & DRAINAGE

The block is largely characterised by almost plane country, except on both sides of Kholar nala where undulations are there. The altitude varies from 327.38m to 300.18m above MSL.

North & North East is high ground whereas; south west is low area along which the Nala flows. The water from the entire catchments area of the block flows into Kholar nala.

3.6 LAND USE PATTERN

Land for surface facilities / pit facilities have been acquired and an amount of Rs 45:27 lakes has been incurred.

The EMP of original Project Report is approved by MOEF for 502.60 fila. Within 1-2 years, an Action Plan may be drawn to process the acquisition of Land covering total mining area upto fault F7-F7. Total land is to be acquired for depillaring of coal and statutory compliance.

The existing capital (Gross block) as on 31.3.2010 is Rs.3048.26 lakhs. The head wise details are given in Appendix-A.

TYPE OF LAND	AREA (Ha)
Tenancy Land	143.51
Government Land	7.6.81
Forest Land	282.28
Total Land	502.60

Job No: 501085

111-2/2

CHAPTER - IV GEOLOGY AND DEPOSIT APPRAISAL

4.1 BACKGROUND / INTRODUCTION

Geological exploration in Dilwadih geological block covering an area of about 26 Sq. Km has been done during 1979 to 1984 and a geological report on Dilwadih bock, Korba coal field has been prepared in March, 1985. Based on this geological report, two underground mines viz., Dilwadih and Singhali have been prepared in Sector-E and Sector-A, G respectively. Later on, detailed exploration in Sectors H I J K L M N have been explored in details by CMPDI covering an area of about 10.54 sq. km and a final G.R. on Bagdewa block, Korba coal field have been made in February, 1998.

4.2 EXPLORATION STATUS

A total of 105 Nos. of boreholes has so far been drilled by various agencies within Bagdewa block area. The details of which is given below:

Year	Agency	Number of Boreholes	Meterage
1070 1005	CMPDIL	93	10447.15
1979-1995	DGM(MP)	12	1017.42
1996-1998 TOTAL	DGW(WIF)	105	11464.58

During 1979 to 1995 CMPDI (Code-CMKD) has drilled 93 boreholes involving 10447.15 m in Dilwadih Block.

DGM (MP) carried out exploration by drilling 12 boreholes during 1996 to 1998 involving 1017.42 m in covering an area of 10.54 sq. km. with density of 10 boreholes per sq. km.

In 1977 GSI also drilled 9 boreholes of KL series in the eastern part of the block.

4.3 GEOLOGY AND STRUCTURE OF BLOCK AREA

4.3.1 Structural setting within the block area

Korba coalfield has a well defined east-west trending southern boundary fault. The northern margin is a normal sedimentary contact. Thus the Korba basin corresponds to a half garben configuration. The boundary fault defines a

prominent lineament. Beside the boundary fault, the coalfield is affected by several intra -basinal fault of varying magnitude and direction. Most of the intra basinal faults are strike faults, aligned in east-west or NW-SE directions. The faults usually hide towards north resulting in repetition of coal seams. A major southerly throwing fault having more than 300 m throw has preserved thick coal seams of middle and upper Barkars in the southern part of the coalfield.

4.3.2 STRUCTURE OF THE BLOCK

4.3.3. Structural setting within the block area

Bagdewa block is covered by thick soil cover in major part and rock exposures are only along the Kholar Nala section. Hence the structural interpretation presented in this report is based on subsurface data obtained by drilling.

The Bagdewa block structurally represents the western limb of a doubly plunging synclinal sub-basin with the axis running NW-SE. The part of the southern limb of this sub-basin is faulted.

Due to rolling nature of strata the amount of dip varies in different part of the block. In the northern part, dip is very gentle about 3°. In the central part of block, the dip of strata is 4°. In the area just south of Kholar nala the dip is steeper and become 7°. Again in the south-eastern part of the block the dip is 4°.

4.3.4 FAULTS

A total of 12 Nos. of faults named F1 to F12 have been interpreted in the block on the basis of available subsurface data. However, taking into considerations the frequent swing in strike direction, rolling nature of dip and sudden variation in parting of seam, the presence of some minor faults cannot be ruled out.

IV-2/19 Job No: 501085

THE THE PARTY OF T

4.4 DESCRIPTION OF COAL SEAMS

The sequence of coal seam in the block is as given below:-

Seam	Depth (m)	Thickness	Grade	GCV	No. of BH	Geological Reserves (Mte)
G-V	15.17-64.70	0.10-2.29	F-B (D)	4095-	36	5.86
		(<1.5m)		568		
Parting	Similar to the	12.27-26.9m	Ma mais		51	
G-IV	14.2-85.0	1.4-2.65	G-C (C)	4005- 5256		6.62
Parting		33.65-50.60	Territoria.	Anthony S		
G-III (Top)	10.60- 132.50	0.25-3.05	F-A (B)	4720- 6.346	64	13.93
Parting		0.60-15.07		Talk Liller		
G-III (Bottom)	13.2-136.49	0.45-7.0	E-A(B)	4607- 6540	82	29.44
G-III		4.74-7.0			SEDE	
(Comb)		4.07.00.0		July 1		. "
Parting		1.27-28.0	= 4/5	5040	62	8.097
G-II A	13.2-158.6	0.1-2.64	F-A(B)	5643- 6195	63	8.097
Parting	The desired of	17.25-41.00	ill uniqu			
G-II	ED BURGES	0.07-0.77				
Parting	reference Fall	16.74-30.26		The street		Not estimated
G-I		0.12-1.35				Not estimated
	MACHINE MACHINE	TOTAL		Municipal		67.9

Description of individual coal seams

4.4.1 Seam -GV

Seam GV is the youngest coal seam encountered and it has been intersected in 36 boreholes. The seam is intersected at the minimum and maximum depths of 15.17ms (CMKD-122) and 64.70ms (CMKD-57) respectively.

In crop

The seam GV does not crop out at any place in the block.

Thickness

The including band thickness of the seam varies from 0.10m to 2.29m. However, the normal range of thickness falls between 0.9m to 1.5m.

Roof & Floor

The roof of Seam-GV is predominantly coarse grained sandstone. In small patches, it is Carb. shale or gray shale. Floor of the seam is predominantly coarse grained sandstone. Occasionally, fine grained sandstone, Grey shale & Carbonaceous Shale form the floor.

Dirt Bands

Out of 36 boreholes in which Seam-GV has been encountered, the seam is banded only in 3 boreholes; their cumulative thickness varies from 0.20 to 0.37m.

Quality Parameter

The number of band-by-band analysis, Proximate Overall analysis and special test obtained are given in the following table.

Details of band by band analysis of seam are given in Annexure-III and have been graphically presented as the structure of seam in Plate-IV.

Proximate overall analysis at 60% RH & 40° C has been determined for 10 bore holes and calculated for 11 boreholes out of 21 boreholes where it has developed workable thickness of 0.90m and above. The ranges of different quality parameters are tabulated below:-

Job No: 501085

1V-4/19

Parameter	M%	Ash %	VM%	FC	GCV	UHV	Grade
			100		K. Cal/Kg	K. Cal/Kg	Mark
E/Bcs	100000						
Sample			The sales				
No. of	21	21	, 11	11	10	21	21
Sample			10.1	B TOLET	IC SHEW		Land
Minimum	4.5	13.4	19.2	36.4	4075	2773	F
Maximum	9.4	39.6	31.6	52.0	5680	6112	В

Workability:-

On perusal of isochors of G-V Seam indicates that it has attained a thickness of more than 1.2m in very small patch, having no definite pattern of development. The grade in this workable thickness range is D to E and a total geological reserve in free area is 2.24 Mte which do not offer economic potentiality.

4.4.2 Seam- G-IV

Seam GIV underlies seam GV with a parting of 12.27m to 26.90m.

The depth of occurrence of Seam G-IV varies from 14.20 to 85.00m.

Thickness

The stratigraphic thickness of the combined seam varies from 1.4m to 3.50m. But from the nature of bands developed in the middle of the seam, for all practical purposes the seam is considered into 2 sections, i.e. Seam GIV Top and G IV Bottom.

Seam G IV is split up into top and bottom section in 42 bore holes and combined thickness is observed in 9 boreholes.

The thickness of GIV Top varies from 0.07m to 1.30m and unworkable in entire area.

The thickness of GIV bottom varies from 0.13 to 1.65m and major area does not offer any workable patch.

Roof & Floor:-Job No: 501085

IV-5/19

Roof of Seam GIV is predominantly coarse grained sandstone.

Floor of the seam is also coarse grained sandstone in major part; however, in the northern part it is argillaceous.

As the seam was considered composite earlier, therefore, proximate analysis on 60% RH & 40°C is available for the entire composite seam for 20 boreholes, for GIV Bottom Seam – the quality data is available for 13 boreholes, and for GIV Top seam for 5 bore holes only. The different parameters of quality are presented in Table below:-

PROXIMATE ANALYSIS (on 60% RH 40°C) of Seam GV, Bagdewa Block

Parameter	M%	Ash%	VM%	FC%	GCV	UHV .	Grade
n denten	of thereal		TEN IEU SI	FIX.3 me	K.c al/Kg	K. Cal/Kg.	
GIV	Penul s	THE WAY	de la company	in sta	ortificadismo.		
Composite	Tab Tal	aler_is	100	d see a			
I Sample							
Minimum	4.0	40.9	16.5	30.3	3375	1517	G
Maximum	5.3	48.8	18:4	33.5	3927	2514	F
G IV Top		S M LT	A VO 10	3 84(12)	en la sona		
I ₃₀ Sample	E felly part	and Vale			lo daley all		
Minimum	5.3	22.0		-	4207	2514	F
Maximum	7.1	38.5	10 - 10		,5251	4981	С
G IV	Bala s			STANDER			
Bottom	And the same of	alei se		1500	SPECIAL S	iner.	
E/Bcs				Telesia.	a reputation	Phone Li	
Sample		- Tartella	131.00	M. Sien	No. of the last		
Minimum	4.2	17.4	20.0	35.1	4242	2290	G
Maximum	7.4	43.5	27.4	47.2	5478	5560	C

The overall grade of Seam IV Composite seam varied between G-F on I sample, that of GIV Top is F to C and GIV Bottom Seam G-C.

Workability :-

Job No: 501085

IV-6/19

A perusal of Isochors line indicates that Seam G-IV is split-up in two sections in the entire block except in four small isolated patches.

Due to inconsistent nature of Seam G IV Top and GIV Bottom, both the seam does not attract attention from the workability point of view.

4.4.3 Seam G III

Seam G III is the most potential seam of the block from the view point of quality and thickness. It underlies seam G IV at a parting varying from 33.65 to 50.60m. The seam generally occurs in two splits except for a small patch around bore hole CMKD-115, 124, MPDJ- 1,2,3,9 in the southern part of block where it occurs as combined seam varying in thickness for 4.74 to 7.00m.

4.4.4 Seam G III Top

Seam G III Top underlies Seam GIV after a parting of 33.65m to 50.60m.

The minimum depth of occurrence of Seam G-III Top is 10.60m and the maximum depth of Seam is 132.50m.

Thickness

The range of seam thickness is between 0.9 and 2.5m. In south-eastern part of the block, seam thickness is less than 0.9m and unworkable.

Roof & Floor

The roof of Seam G-III Top is predominantly coarse grained sandstone. In the northern and southern part it is alternate shale and sandstone to carb.shale.

Floor of the seam varies in lithology. In the northern most part floor is Fine grained sandstone. It is comprised of Shaley sandstone, alternate shale and sandstone and Grey sandy shale in the central part. Therefore, the floor of seam in major part of the block is argillaceous.

Dirt band

Out of 64 bore holes in which seam G III Top has been encountered, the seam is banded only in 5 boreholes.

Quality

The number of band by band analysis, proximate overall analysis and special tests obtained given below:-

Proximate analysis (on 60% RH & 40°C) of Seam G III Top

Job No: 501085

IV-7/19

Parameter	M%	Ash%	VM%	FC%	GCV K. Cal/Kg	UHV K. Cal/Kg.	Grade
E / Bcs Sample							
No.of Sample	42	42	19	19	13	42	42
Minimum	3.1	12.0	21.0	34.3	4720	2989	F
Maximum	÷9.8	39.4	31.0	54.0	6346	6224	A

The overall grade of Seam G-III Top varies between A and F.

Ultimate Analysis, Ash Fusion range ash analysis and HGI of the seam is given in table below:-

Ultimate Analysis of Seam G III Top

Borehole No.	Sample Type		Constituer	nts (on Unit (Coal basis)	
	Internal	C%	H%	N%	S%	0%
CMKD-146	Bcs	81.5	4.6	1.7	0.8	11.4
EVENE LE	430	81.6	4.5	1.7	0.9	11.3
CMKD-150	Bcs	80.2	5.0	1.6	0.6	12.6
CMKD-168	130	70.2	3.3	1.2	0.5	23.6
CMKD-180	Bcs	80.8	5.0	1.9	0.6	11.7

Ash Fusion Range of Seam G III Top Ash Analysis of Seam G III Top

Content	Borehole No.						
	CMKD-146	CMKD-146	CMKD-167	CMKD-180			
	Bcs	1 30					
SiO ₂	58.46	58.48	59.62	60.14			
Al ₂ O ₃	31.26	30.86	26.76	28.26			
Fe ₂ O ₃	5.34	5,65	4.06	3.98			
TiO ₂	1.58	1.56	2.20	2.06			
P ₂ O ₅	0:05	0.06	Traces	0.01			

Content	Borehole No.						
	CMKD-146	CMKD-146	CMKD-167	CMKD-180			
	Bcs	1 30		Inchie			
MnO	0.45	0.48	0.92	0.9			
CaO	0.96	0.95	2.96	2.16			
MgO	1.00	0.94	2.24	1.28			
SO ₃	0.12	0.10	CHARLE CONTRACT	-			
Alkalis	0.78	0.92	1.24	1.21,			

Hard Grove Index of Seam GIII Top

Borehole Number	H.G.I	
CMKD-168	51	
CMKD-180	53	

On perusal of ultimate analysis, it may be seen that the Sulphur content (in GIII-Top Seam is higher (0.5 to 0.9%) in comparison with the-other seams). Workability

Seam G III Top is an important seam of the block after G III Bottom seam. The Seam G III Top can be mined in the northern and southern part of the mining block, where it attains workable thickness and grade.

The seam G III Top has a parting with the underlying GIII Bottom seam less than 3m in the east-southern part of block. This portion will be exploited in Unit-2.

4.4.5 Seam G III Bottom

Seam G III Bottom is the most important seam in the block. The seam has been intersected in 82 boreholes. It is developed in the entire block Seam GIII Bottom underlies the GIII Top seam at parting varying in thickness from 0.60m (MPDJ-4) to 15.07m (CMKD-145). Most of the area considered for working lies within 10m parting with G-III top.

The seam is intersected at the minimum and maximum depth of 13.20m (CMKD-184) to 136.49m (CMKD-26).

Thickness

The thickness of seam varies between 0.45m and 7.00m. The normal range of seam thickness varies between 2.00m and 3.00m (in Phase-I).

Roof & Floor

The roof of Seam G III Bottom is predominantly argillaceous, consists of Grey Shale, Grey Sandy Shale, Shaly Sandstone and Alternate Shale & Sandstone.

The floor of the seam is predominantly arenaceous comprised of Fine to Coarse grained sandstones.

Dirt Bands:-

Out of 82 borehole intersections, the seam is banded in 9 boreholes. Details of dirt bands observed in the seam in 9 bore holes are given in the following table.

Borehole wise details of dirt band in G III Bottom / Combined

B.H. No.	Hayaya,	Combustible		Non-Combustible			
	No. of	Total Thickness	% of-	No. of bands	Total Thickness	% of	
CMKD-43	1	10.13	2.6	2	0.86	17.2	
CMKD-107	শ	0.60	13.0		len sireesi		
CMKD-115	ব	0.11	1.6	2	0.44	6.3	
GMKD-127	1	0.16	-6.1	100- 120		-	
CMKD-132	Carl to State		ma de Sand	1	0.30	12.5	
CMKD-180	7 m		10 1 Tarilla	1	0.30	13,8	
MPDJ-3	র	0.22	4.6	ale Strife	5 - 5 5 10	-	
MPDJ-4			and the	1 1	0.08	1.5	
MPDJ-9	610-108			1	0.30	3.6	
MPDJ-12	100 m	- 4		1	0.22	7.5	

Proximate Overall analysis as stated above has been determined for 50 boreholes and calculated for 17 boreholes. The ranges of various parameters of Proximate Analysis are given below:-

PROXIMATE ANALYSIS (On 60%RH 40°C) of GIII Bottom / Combined

RPR Bagdewa UG(0.75 Mty)

Parameter	M%	Ash%	VM%	FC%	GCV	UHV	Grade
					K. Cal/Kg	K. Cal/Kg.	
E / Bcs Sample							
No. of Sample	68	68	4 5	45	7	68	
Minimum	3.6	10.0	22.0	44.9	4607	3523	E
Maximum	8.0	33.5	29.9	57.4	6540	6733	А
I ₃₀ Sample	(Includin	g E/Bcs Sa	amples whe	ere C, Sh	band is not d	eveloped)	
No. of	72	72	45	45	1	4	
Sample							
Minimum	3.6	10.0	22.0	44.9	4607	3523	E
Maximum	8.0	33.5	29.9	57.4	6540	6733	A

Ultimate Analysis of Seam G III Top

Borehole	Sample	Constituents (on Unit Coal basis)						
No.	Туре	C%	H%	N%	S%	0%		
CMKD-168	E	80.8	4.8	1.8	0.3	12.3		
CMKD-180	E	80.2	4.9	1.8	0.5	12.6		
CMKD-188	E	81	5.1	1.9	0.4	11.6		
MPDJ-1	BCs	84.6	4.3	1.4	0.6	9.1		
MPDJ-2	BCs	85.2	4.4	1.4	0.3	8.7		
MPDJ-3	130	85.7	4.4	1.6	0.2	8.1		
MPDJ-4	1 ₃₀	81.7	4.3	2.1	0.4	11.5		
MPDJ-9	130	83.2	4.3	1.4	0.4	10.7		

Ash Fusion Range of Seam G III Top

B.H. No.	Ash fusion range °C								
	Sample Type	IDT	нт	FT					
MPDJ-1	E	1340	>1400	>1400					
MPDJ-2	Е	₹1390	>1400	>1400					
MPDJ-3	1 ₃₀	>1400	>1400	>1400					
MPDJ-4	130	>1400	>1400	>1400					
MPDJ-5	130	>1400	>1400	>1400					

Ash Analysis of GIII Bottomil Combined

Content	1	Contract of the last		Boreh	ole No.			
	CMKD-	CMKD- 180	CMKD-	MPDJ-1	MPDJ-2	MPDJ-3	MPDJ-4	MPDJ-9
SiO ₂	59.46	57.34	56.72	55.86	57.84	57.44	58.46	58.23
	26.23	28.92	27.68	30:50	28.90	28.60	29.00	29.50
Al ₂ O ₃	4.18	4.40	5.06	6.92	5.80	6.40	5.46	5.00
Fe ₂ O ₃	2.08	1.98	2.16	1.6	1.60	1.70	1.6	1.70
TiO ₂	A STATE OF THE STA	Traces	0.01	0.2	0.22	0.16	0.22	0.20
P ₂ O ₅	0.01	Traces	0.01	0.3	0.30	0.12	0.30	0.26
MnO	-	2.02	2.94	2.10	2.00	2.20	1.90	1.90
CaO	3.24	-3.02		1.7	1.7	1.40	1.40	1.60
MgO	2.56	2.26	3.13		0.22	0.11	0.20	0.18
SO ₃	0.94	0.96	0.88	0.16			1:46	1.43
Alkalies	1.30	1.12	1.42	0.66	1.42	1.87	1,40	1.40

Workability

Seam G III is combined in a small patch in the south-western part of the block where the thickness of seam (Ex-band) varies from 4.74m to 6.56m with grade C-D. The seam splits towards the in crop zone. In the northern most part of the block, the parting between the G III Bottom and the underlying G II A seam reduces, below 3m.

4.4.6 Seam-G II A

Job No: 501085

IV-12/19

Seam G IIA underlies seam G III Bottom with a parting of 1.27 to 28.00m. In most of the area parting is 10m. In the western most part of Bagdewa block, workable thickness of seam with good quality was observed, which is correlated as Seam G IIA. This seam has been encountered in 63 boreholes. Out of which 3 boreholes fall in the in crop zone.

Seam G II A shows splitting tendency throughout the block.

The minimum and maximum depth of occurrence from surface is 16.71m and 158.60m respectively.

Thickness

The thickness of the seam varies from 0.10m (CMKD-114) to 2.64m (CMKD-147). Out of the three splits of Seam G-II A, the middle section is consistent in thickness and is considered for drawing of Isochors. However, in the northern part of the block, the Top & Middle sections are well developed.

From the perusal of isochors plan of G IIA seam it is observed that the seam thickness reduces abruptly along a north south alignment which corresponds very much with the abrupt increase in parting between Seam G II A and G III Bottom.

In the south of Fault F7-F7, the seam again abruptly deteriorates in thickness and become less than 0.9m in thickness.

Roof & Floor

The roof of Seam G II A is predominantly coarse grained sandstone except in the northern part where roof is argillaceous.

Floor of the Seam is predominantly argillaceous comprised of grey shale, grey sandy shale and intercalation of shale and sandstone.

Dirt band

Out of 63 borehole intersection of Seam G IIA, in 15 bore holes seam has developed band. Details of dirt bands observed in 15 bore hole is given in the following table.

IV-13/19 Job No: 501085

Details of dirt band in Seam G II A Bagdewa Block

B.H. No.		Combustible		Non-Combustible			
	No. of bands	Total thickness	% of band	No. of bands	Total thickness	% of band	
CMKD-147	-		-	1	0.15	5.60	
CMKD-150			-	1	0.17	8.90	
CMKD-#52	-	- 1		1	0.12	11.20	
CMKD-153	-	-	-	1	0.20	7.70	
CMKD-161	- 188	AUDIO EST		1	0.03	1.80	
CMKD-474		- 1		1	0,20	14.80	
CMKD-176	S R. T.			1	0.11	8.90	
CMKD-179	-			1	0.10	7.10	
CMKD-180	1	0.18	7.00	1	0:20	13.2	
CMKD-184	CORD TIES		-	1	0.16	8.60	
CMKD-190	1	0.14	17.70	-		-	
CMKD-193	dict-plan	4-24	-V15#	1	0.20	12.50	
CMKD-202	1	0.22	8.80			-	
CMKD-203	1	0.11	4.90	-	-	-	
CMKD-205	-			1	0.15	670	

Proximate overall analysis has been determined for 26 bore holes and calculated for 10 boreholes. The ranges of different parameters of proximate analysis are given below:-

PROXIMATE ANALYSIS (On:60%RH 40°C) of Seam G II A

Parameter	M%	Ash%	VM%	FC%	GCV K.Cal/Kg	WHV K. Cal/Kg.	Grade
E Sample		A 0.00 E			Linke is		
No. of Sample	38	38	30	'30	4	38	38
Minimum	.5.1	10.1	20.9	42.7	5643	2994	F
Maximum	7.6	37.4	31.7	53.7	6195	6678	Α
I ₃₀ Sample	(Includin	g E/Bcs Sa	mples whe	re C, Sh t	oand is not de	eveloped)	

Job No: 501085

IV-14/19

19999999999999999999999999999999

RPR Bagdewa UG(0.75 Mty)

Parameter	M%	Ash%	VM%	FC%	GCV K.Cal/Kg	UHV K. Cal/Kg.	Grade
No. of Sample	42	42	32	32	4		
Minimum	4.7	10.1	20.9	37.5	5643	2994	F
Maximum	7.6	37.4	31.7	53.7	6195	6678	А
I Sample			**************************************				
No. of Sample	3	3	3	3			
Minimum	6.2	28.1	22.4	39.3		3739	E
Maximum	6.5	31.2	25.1	41.6		4125	E

Ultimate Analysis, ash fusion range as well ash analysis of Seam G II A is given in the following table :-

Ultimate Analysis of Seam G II A

Borehole No.	Sample	- Constituents (on Unit-Coal basis)							
	Туре	C%	Н%	N%	S%	0%			
CMKD-150	E	80.4	4.6	1.1	0.4	12.9			
CMKD-168	BCs	81.1	4.9	1.8	0.4	11.8			
CMKD-180	I ₃₀	82.1	4.7	1.8	0.4	11.0			
CMKD-188 (Top)	E	80.0	4.9	1.7	0.3	13.1			
CMKD-188 (Bottom)	E	80.5	5.0	1.8	0.4	12.3			

Ash Fusion Range of Seam G II A

B.H. No.	Ash fusion range °C						
80°5	Sample Type	IDT	HT	FT			
CMKD-150	E	1100	1390	>1400			

Ash Analysis of Seam G II A

			Borehole No.	
	CMKD-168	CMKD-180	CMKD-188 (Top split)	(Bottom split)
SiO ₂	57.2	56.92	59.01	60.18
Al ₂ O ₃	27.35	27.74	26.58	25.72
Fe ₂ O ₃	4.68	· .4.52	4.84	5.12
TiO ₂	1.98	2.09	2.11	1.86
P ₂ O ₅	Traces	Traces	Traces	Traces
CaO	3.63	3.68	2.86	2.70
MgO	2.92	2.86	2.31	2.02
SO ₃	0.86	0.88	0.93	0.95
Alkalis	1.38	1,31	1.36	1.45

HARD GROVE INDEX OF SEAM G II A

Borehole Number	H.G.I
CMKD-168	50
CMKD-180	-51
CMKD-188 (Top)	51
CMKD-188(Bottom)	54

Workability

A perusal of the isochors of Seam II A indicates that the seam attains workable thickness only in Sector A and part of Sector D. In other sectors the seam has deteriorated in thickness below workable limit. However, in Sector A the seam G II A and overlying GIII Bottom has a parting thickness less than 3m in the northern most part in a small reserve.

4.5 HYDROGEOLOGICAL DETAILS

4.5.1 SURFACE WATERS

The block is largely characterised by almost plane country, except on both sides of Kholar nala where undulations are there. The altitude varies from 327.38m to 300.18m above MSL.

North & North East is high ground whereas; south west is low area along which the Nala flows. The water from the entire catchments area of the block flows into Kholar nala.

4.5.2 PROBABLE IMPACT OF MINING ON GROUNDWATER SYSTEM

- (a) Impact on Topography & Drainage: Subsidence due to total extraction of coal causes changes in topography and drainage by developing micro basins, subsidence fractures, ridges, pot holes etc. This alters the drainage of the area in micro level. Care is taken during mining activity to leave enough pillars in underground as barriers below main drainage/water body to avoid any damage to surface water bodies. In deeper underground mines, the subsidence is barely noticeable on the surface.
- (b) Impact on Aquifer System: Various methods of U/G mining activities may cause changes in aquifer geometry, water level in the vicinity of the mine and disturb ground water flow direction. This can also create secondary fractures and higher permeability zones within the aquifer system. Thereby, the aquifer units maintain continuity. After the mining activity, the aquifer restores its original water level and mined out area acts as a good reservoir. In the present case, as the Bagdeva U/G project is a shallow U/G mine, the impact of mining activity on unconfined aquifer, will be observed only near to the mine mouth and shallow workings. However, the impact will be marginal to negligible towards north-east, i.e. in the deep dip direction.
- (c) Impact of Water Levels: During mining, the formation near to the mine mouth only get disturbed and marginally dewatered. With the presence of low permeable beds such as clay (shale) and younger coal seams (Ghurdeva) in the formations lying above the top working seam, the water level in the phreatic aquifer is not affected during the Bord and Pillar mining activity. In case of total extraction of coal (depillaring) and resultant subsidence cracks, the water may drain into the mine causing lowering of water table at the vicinity of the mine. Draw down thus created may be limited to lesser area since the mine pumped out water is re-circulated into the phreatic aquifer by natural recharge. It was also observed that after mining activity is over the water level restores to its original level after one or two monsoons.

The radius of probable impact on groundwater level under caving conditions was predicted to vary from 255m to 462m. With variation in aquifer/mine geometry, return flow for mine discharge, abundant recharge potential and

improved subsidence management, the zone of disturbance will be reduced further.

Due to this impact, the groundwater levels in the nearby villages close to the mine workings are marginally affected. The water levels in other areas maintain the natural fluctuations and even the tube wells are operating in villages without any problem. This clearly indicates that the impact is limited close to the mine operating area only.

(d) Impact on Ground Water Quality: The groundwater chemistry indicates that the groundwater in the area is potable and does not contain any toxic elements. The underground mining activity does not induce any unwanted chemical or elements into the groundwater affecting the water chemistry except for Total Suspended Solids (TSS), no serious pollutant has been observed in the mine water discharge. The discharge water conforms to the MOEF standards. After necessary treatment, mine water from adjacent Singhali UG and Dhelwadih tgoan UG has been gainfully jutilised for drinking purposes.

4.5.3 CONSERVATION MEASURES

- The effected habitation has been provided with suitable drinking water supply by sinking hand pumps/deep tube wells.
- The entire mine industrial water demand, would be met from the treated mine discharge. The wastage of water will be minimized.
- The surplus treated mine water will be discharged into the local ponds or agricultural fields. Thereby, the mine water will behave as constant source of recharge and improves the water levels in the mine area. This will also become a resource for irrigation and increase agriculture output in the area.
 - To assess the impact on local water levels, in time and space coordinates, a
 monitoring net work of dug wells in the zone of influence base established
 and the water levels are monitored quarterly (February, May, August and
 November).

Job No: 501085

IV-18/19

4.6 GEOLOGICALRESERVES

4.6.1 The geological reserve statement in the block is given in the following pages:-

Seam	Under	Blocked	15 M	Total	Remarks
	free Area	Nala Village	HCL		
G-V	2.978	0.846	2.036	5.86	Not considered in RPR Patchy Deposit
G-IV:-					
IV Top	1.157	0.118		1.275	Not considered
IV Bott.	2.656	1.07		3.726	Poor Grade
IVC	0.852	0.772		1.624	
G-III					
III Top	10.119	1.657	2.115	13.891	4.934 Mt considered
III Bott.	22.05	3.445	3.947	29.442	13.01 Mt considered
III C	3.966			3.966	Available in Phase-II Block
G-II A	6:47	1.625		8.095	6.6 Mt considered
Total	50.248	9.533	8.098	67.879	24.54 Mt considered in RPR

About 24 Mte of coal would be available in Unit-2 of mine operation lying south of the fault F7-F7.

4.6.2 GEOLOGICAL LOSSES / SURFACE CONSTRAINTS

The reserve estimation has been done on the basis of the plans of the seams provided and reserve calculated in previous RPR of the Bagdewa Block. Geological losses has been calculated which is blocked in 15M HCL, Nalla, and villages.



Job No: 501085

IV-19/19

STATEMENT OF GEOLOGICAL RESERVES IN UNIT-I PROPERTY

	Thickness						-		Total
	Range	A	В	C	. 0	E	Reserves	Area	Reserves
Brucolars		Reserves	Reserves	Reserves	Reserves	Reserves	Reserves	1	
Seam III T								1	
ector-A			0.3321	0.2801	0.2124	0.3269	0.1071	0.6874	1.2586
a) Free Area	1.2-1.5		0.3022	-	0,0955	0.2318	0.1309	0.4487	1.0038
4.3	1.5-1.8	-	0.2496	THE RESERVE THE PERSON NAMED IN COLUMN 2 IS NOT THE PERSON NAMED I	0.1404	0.0035		0.2134	0.5325
	1.8-2.0 2.0-2.5		0,0684	The state of the s	0.0302			"0.1124	0.3332
	12.5-3.0	1	1	0,0138	The state of	4		0.0038	0.0138
2 M (4-14-1	12.5-5.0	1	0:9523	0.9109	+0.4785	0.5622	0.238	. 1.4657	3,1419
Sub Total(a)		1 1	3.4	1 4			1	4	The Table
b) Within 60m			c	k	150000	-		0.0498	0.0895
Barrier Area	1.2-1.5	To the same of	0:0017	0,0693			-	0.1481	0.3217
7 2 2	1.5-1.8		0.137					0.0231	0.0571
The second second	1.8-2.0	1	0.027			. 6	-	0.0696	0:2027
-	2.0-2.5	The state of the s	0.127			-	0	0.2906	0.671
Sub Total(b)			+0,293	0.2586	0.1188	0	- 0	0.2300	0.0
Within Village			-	1					
Area			- 34	1	-	-		0.013	0.0224
	1.2-1.5		0.022			7		0.0213	0.0457
The same of the	1.5-1.8	Town to the				0	0	010343	0.0681
Sub Total(c)		350	0.044			0.5622	0.238	1.7906	3.881
TOTAL SECTOR-A			1.290		0.0315	U.UULZ	3	4 1	
II. SECTOR-B		1						- Me	
(a) FREE AREA		1	0.000	2	6		Contract of the	.0.033h	0.0633
4.	1.2-1.5		0.063					0,192	\$ 0.45
PERSONAL PROPERTY AND ADDRESS OF THE PERSONAL PR	1.5-1.8	1	0.118		1			0.044	10.1187
	1.8-2,0	1	0.03		1			0.01075	₹0.032
- desta comment	2.0-2.5		0.66		0	0	0	0.27975	. 0.664
Sub Total(a)		1	0.00		-	-		-	
(b) Within 60m					-				W. O. C. C.
Barrier Area	1510	-	0.055	5	1	-		0:0263	0.0555
San	1.5-1.8	-	0.042					0.0175	0.0425
	1.8-2.0		0.006					0.0023	0.0066
21 2 1 10 1	2.0-2.5		0.104		0 0	0	0	0.0461	0,1046
Sub Total(b)				to the	1		11/18/11/20	No.	
Within Village		1		8	ů ·		-	0.0921	0.17634
Area	1.2-1.5		0.14864	16 0.027	7		-	0.0464	
	1.5-1,8		0,07460	0.025	1			0.0013	0.00841
	1.8-2.0			0.00841	100	1	0	0.1398	0.28446
Cub Tetal/cl	110 210		0.2232			0	0	0:46565	The state of the s
Sub Total(c) TOTAL SEGTOR-	3	2	0.9916	0.06.121	2 0	. 0	0	0,4000	
III.SECTOR-C	History & III		1	- 5		-		0,1563	0.271
(a) Free Area	1.2-1.5	I TOTAL	-0.18				1000	0.1293	0,2733
(4)310071100	1.5-1.8		: 0.2		13		1	0.0488	
GOVERNMENT TO	1.8-2,0	-10.0031	0.73	53	-	2 P. C. C. C.		0.0375	
10 E	2.0-2.5	19	10.10		6 0	0	0	5 0.3709	0.7705
Sub-Total(a)	接一一人	0.0031	0.85	the same of the sa	1	THE DATE OF	THE PARTY NAMED IN		The Contract of
(b) Within 60m	The state of	1	4	1	1 2 2 2			11	1. 4
Barrier Area		4	.0.01	55 0.04	79	78		0.0358	The second secon
Figure 81 (per se te	1.2-1.5		-1.0.01	-		100		0.0228	
	, 1.5-1.8		0.03	NAME AND ADDRESS OF THE OWNER, WHEN PERSON NAMED IN		0	- 0	0.0586	
Sub Total(a)		-	1,1305	The second secon	-	0	0	0.5617	5 -1.27346
TOTAL SECTOR-	C	1	tarous	0.1120	100				-
TOTAL		-						100	A 6 400
3. SE		0.0167	0.17	765		12 15 215		0.1121	
(a) F 'Area	1.2-1.5	The second second			2			0.3098	Total Street Street Street Street
*	> 1.5-1.8	And in case of the last of the	The second name of the second	71	1	19 0	100	0.3248	and the second second second
1 15	1.8-2:0	The second second second	the same of the same of the same		73		1	1.1948	
St. C. F.	2.0-2.5		The second second	and the same of th	68			0.739	Name and Address of the Owner, where the Owner, which is the Owner, where the Owner, which is the Owner
	2,5-3.0		> 0.00	Additional Property and Publishers a	95	WE SHELL	HAT PARKET	0.033	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TO T
	3.0-3.5	2,179	-	-		0	0	2.714	7.805
Sub Total(a)		11.				1	A	1	
(b) Within 60m				- 4	1		357		

Job No.501085

Particulars	Thickness Range	A	В	С	D	E	F		Total
		Reserves	Reserves	Reserves	Reserves	Reserves	Reserves	Area	Reserve
	1.5-1.8		0.097					0.046	0.097
	1.8-2.0	0.033	0.0728		1.00	and the same	The state of	0.0438	0.1058
INCOMEDIA SE	2.0-2.5	0.0349	0.0684					0.0361	0.1033
	2.5-3.0		0.3156		0	0	0	0.1758	0.6285
Sub Total(b)	TO STATE SHAPE	0.0679	0.5538	0.3129	0	0	0	0.2557	0.9346
© Within Village	Stored Style	1577000	2000年第二日	N. H. A. S. S.	COLUMN TOWN	PERIOD PO	发展的建筑		
Area		1		F				0.0400	0.0057
	1.5-1.8	0.0177	0.008					0.0123	0.0257
	1.8-2.0	0.0371	0.0141	0.4000	-			0.0213	0.0512
	2.0-2.5	0.0666	0.2223	0.1399	^		-	0.1478	0.4288
Sub Total(c)		0.1214	0.2444	0.1399	0	0	0	0.1814	0.5057
TOTAL SECTOR-A		2.3689	5.5803	1.2964	0	0	0	3.1972	9.2456
II. SECTOR-B							-		-
(a) Free Area	1.2-1.5					-			
	1.5-1.8			1	A THE RESERVE		-	Continue to	
	1.8-2.0		4 250					0.4039	1.258
	2.0-2.5 2.5-3.0	7.00	0.5816	8				0.4039	0.5816
	3.0-3.5		0.5616		The second		-	0.1043	0.0010
		1	1	0.00				0.71	
	4.0-4.5					- An - 1/2			
Cub Total/a)	4,5-5.0	0	1.8396	0	0	0	0	0.5684	1.8396
Sub Total(a) (b) Within 60m Barrier Area		0	1.0330				1 3 3 3	0.5004	1.0330
Darrier Area	1.2-1.5				0.0079		100	0.0043	0.0122
	1.5-1.8				0.0214	510 100		0.0095	0.0214
	1.8-2.0	VIII CONTRACTOR	100000	DOALDER N	0.039			0.015	0.039
	2.0-2.5	100000000000000000000000000000000000000		The state of the state of	0.1108	7.7 S 0 1 1 1	UNITED STORY	0.036	0.1108
NAME OF TAXABLE PARTY.	2.5-3.0	V	0.0063	0.1182		E TOWN		0.0343	0.1245
WHITE OF STREET	3.0-3.5	EZ IFE EN	0.0054	0.0408		(10-5mm/s+m	A 100 100 100 100 100 100 100 100 100 10	0.0108	0.0462
Sub Total(b)	William Co.	TO PORT HIND	0.0117	0.159	0.1791	0	0	0.1099	0.3541
© Within Village Area									
	1.2-1.5		0.0302	The second second				0.0175	0.0302
	1.5-1.8		0.0886			LE SIN		0.042	0.0886
	1.8-2.0		0.0554					0.0228	0.0554
	2.0-2.5		0.0267	1				0.0093	0.0267
Sub Total(c)			0.2009	0		0	0	0.0916	0.2009
TOTAL SECTOR-B		0	2.0522	0.159	0.1791	0	0	0.7699	2.3903
III.SECTOR-C					WEST STREET,		The Part of the Pa	HELL HALL	
(a) Free Area	1.2-1.5			CAR TOTAL	PROPERTY.		THE WATER		
Shields	1.5-1.8	Semin 30	0.038			100		0.0196	0.038
	1.8-2.0	A DOUBLE B	0.115	0.0908				0.0705	0.2058
	2.0-2.5	MAN (1973)	0.0063	0.27				0.0778	0.2763
	2.5-3.0	220	0.031	0.64			The second second	0.1698	0.671
	3.0-3.5								
	3.5-4.0		0.4002	4.0000	0	0	0	0 2277	4 4044
Sub Total(a)			0.1903	1.0008	0	0	0	0.3377	1.1911
(b) Within 60m									
Barrier Area	1011			-	0.0407			0.0058	0.0107
	1.2-1.5				0.0107	THE REAL PROPERTY.			0.0107
	1.5-1.8		0.0073		0.026	CHARLES TO SERVICE STATE OF THE PARTY OF THE		0.0115	0.026
	1.8-2.0		0.0073	0.0039	0.0047			0.0048	0.012
	2.0-2.5	-	0.0101	0.0039				0.0076	0.022
	2.5-3.0			0.0218	THE RESERVE	Sales Inc		0.000	0.0218
Cub Tetal/h)	3.0-3.5		0.0254	0.0937	0.0414	0	0	0.0216	0.1862
Sub Total(b)		16-	0.0254	1.1202	0.0414	0	0	0.3952	1.3773
TOTAL SECTOR-C		589	7.847773	2.5756	0.2205	0	0	4.3623	13.01277
TOTAL SEAM-III B		909	1.041113	2.0700	0.2200	-	-	1.0025	10.01211
SEAM-II A	1	7					7	-	
1. Sector A	1,2-1,5	0.362	0.2878	0.1675	0.1034	0.0182		0.5389	0.9389
a) Free Area	1.5-1.8	0.2356	0.7338	0.1786	0.2117	0.2311	0.0198	0.7434	1.6106
	1.8-2.0	0.2556	0.7336	0.4223	0.1235	0.0305	0.0100	0.4913	1.2178
						0.000		0.7114	2.0971
	2.0-2.5	0.0043	0.7672	1.1246	0.201		The second second second	U. / 1114 I	/ UN / I

and the second s	Thickness Range	A Reserves	B Reserves	C Reserves	D	E Reserves	F Reserves	Area	Total Reserves
1 12 2 2 1)	Reserves			1			1	
(b) Within 60m			1300	L	The state of		1	0.0198	0.0284
Barrier Area	1		-	0.0393	0.0582				0.0975
	1.2-1.5		0.0027	°. 0.0629	0.0677			0.0535	The second second second
	-1.5-1.8		0.0021	And in case of the last of the	0.00	4		0.0601	0.1333
0.00	1.8-2.0		14	0.0817	1			0.0325	0.081
-	2.0-2.5		0.0684	0:056	-	1		0.0426	0.124
	14 6 7.		. 2	0.0000	0.1259	10	0	0.2085	0.4653
Sub Total(b)	A		0.0711	0.2399	0.1233	1	the property of the con-		
Within Village	5 SZ 4 ()	1		\$2.50 ft.		100		1 19 19 19 51	
A CONTRACTOR OF THE PARTY OF TH	1	K.	9			-	With the same of t	0.0826	0.1437
Area	1.2-1:5	0.0345	0:0592	0:05	4	-	4	0:054	- 0.1136
	1:5-1:8	0.027	0.0822	0.0044	4			0.0066	0.0159
	1.8-2.0	0.0079	0.008		1	1	. 0	0.1432	0.2732
	1:0-210	0.0694	0.1494	.0.0544	0	0		2:6282	6.1376
Sub Total(c)		0.7288	2.5222	1.9474	0!6396		0.0198	9.45525	24.5497
TOTAL SEAM-II A	1	3.0977	12.72833	6.0172	1.5833	0/842	0.2578	9.45525	24,5457

Job No.501085

CHAPTER-V

MINE BOUNDARY, RESERVES & MINE LIFE

5.1 SELECTION OF MINING AREA

A. Blocks considered for finalizing mining area:

The following geological blocks have been considered while evaluating and finalising the proposed mine boundaries of Bagdewa UG project and indicated future extension of project boundaries:

- (a) Bagdewa Block (GR on Bagdewa Block, Korba Coalfield, February, 1998)
 - (b) Additional 93 no. Boreholes of CMKD Series drilled by CMPDI have been considered. Based on the data of the boreholes, isochores and iso-grades of the property have been drawn for the calculation of reserves and for lying of panel projections in the area to be developed in the mine.

B. Criteria for selection of mining area & seams :

The following criteria have been used for selection of mining area:-

- a. Proved coal reserves
- b. Large workable area or patches
- c. Hard cover thickness of more than 15m
- d. Workable seam thickness of 1.2m & above

5.2 MINE BOUNDARIES

The Bagdewa geological block is located in the West of Dilwadih underground mines. The area proposed to be exploited in Unit-I by underground mining will be about 4.69 sq. km. The additional area lying up to fault F7-F7 has been annexed and environment clearance from MOEF has been obtained. The underground extraction will be limited up to 4.69 sq. km (the rest of area Unit -II will be exploited only after (later on stage) clearance from the competent authority). The ultimate mine boy by has been demarcated same as mining area proposed in previous RPR (1999), which is given below:-

North - Fault F9-F9 & 15m hard cover line of workable seams.

South - Kholar nalla later on Fault F7-F7 and its extension up to Fault F10 (3 m parting with Seam III top and bottom will follow the extension line).

West - 15m HCL of G-II A seam, working thickness (1.5m lying) and 40m against road to Amarpur village.

East - Fault F8, F10 & workable thickness line (1.5m) of seam.

JUSTIFICATION OF BLOCKING :

As mentioned earlier the geological block covers an area of about 10.54 sq. km, if the entire block is considered for exploitation in one unit, the length of strike panel will be more than 3 Km each side of main dip. This may lead to poor ventilation and transport system. Moreover, the geological structures also favours in exploitation of block in two units as fault F7-F7 divides the block in almost two parts and the extent of G-II-A Seam has been limited up to Fault F7.

Extractable reserves:

Table 5.1: Summary of Geological and Extractable Reserve

Seam	Geolog	Mineable Reserves (Mt)		
Cardiana.	FREE AREA	BLOCKED	TOTAL	
G-III TOP	10.119	3.772	13.891	4.934 considered
G-(II	22,050	7.392	29.442	13.01 considered
G-III C	3.966		3.966	Available in Phase-II
II-A	6.47	1.625	8.095	6.6 MT considered
TOTAL	36.18	11.164	51.428	24.54 MT considered

Grade of coal: Grade of coal is A-C average saleable grade of coal is B.

Mineable reserves: Comprises of reserves in seam thickness >1.5m and hard cover more than 15m.

Job No: 501085

V-2/3



Table 5.2: Summary of Geological and Mineable Reserve

Seam	Area considered (Ha)	Thickness range (m)	Geological Reserve (Mt)	Mining Losses Barr.(Mt)	Blocked coal losses, if any	Mineable Reserve (Mt)
	2	3	4	6	7	8
1 3	2	0	40.004	0.314	3.772	2.20
G-III	135	1.5-3.5	13.891	0.314	5.772	2.20
TOP		1505	20 442	1.767	7.392	12.39
G-III	469.08	1.5-3.5	29.442	1.707	1.002	
BOTTAM		1505	8.095	0.583	1.625	4.044
II-A	2.5	1.5-3.5				
		Busines AT	51.428	2.664	11.164	18.634
TOTAL		8 - 95 5 610	01.420		BURE PURE	TO THE REAL PROPERTY.

5.3 PRODUCTION TARGET & LIFE OF THE MINE

In this RPR it is proposed to deploy additional four LHDs and four UDMs in the second year for an incremental production of 0.345Mty. The existing LHDs will be replaced in accordance with their balance life. The mine has a flat gradient, and favorable roof conditions. The productivity of total machineries deployed has been assessed to be 2460 tpd.

TOTAL - 0.75 Mty

Considering the extractable reserves and the production schedule, the life of the mine is expected to be about 13 years (including production built-up & tapering periods).

MINE LIFE

The balance extractable reserves considered in RPR of Bagdewa UG mine is 9.475 Mte (in the 4.69 sq. km area) inclusive of all three workable seams. With a targeted output of 0.75 mty the life of the mine works out to 13 years including development and depillaring.

CHAPTER-VI

MINE ENTRIES

6.1 SELECTION OF MINE ENTRIES

It was proposed to approach and work the seams IIA and III T, III B by the Existing two inclines and one air shaft in addition; two drifts and staple pits required for ventilation at dip most part. One additional air shaft 5.0m diameter as intake is being proposed up to G-II A seam.

The details of the existing mine entries along with proposed underground mine drivages is shown in Table 6.1.

6.2 JUSTIFICATION FÖR LOCATION OF PROPOSED DRIFTS

The location of the proposed drifts has been fixed considering the following factors:

The existing inclines have been driven up to seam II.A. Trunk belts are installed in main incline. Coal from top seams is loaded through bunker in trunk belts in II.A seam. Therefore two drifts were driven to make approach from II.A. seam to III. Bottom seam. Staple pits were required for better ventilation location as shown in Table 6.1. Six additional drifts are being proposed to cross two faults F2-F2 and F3-F3 of 5m throw each. Two strata bunkers are being proposed between II.A seam and III seam on both sides of trunk belts i.e. northern and southern side. Two drifts and one staple pit is being proposed to inter in G-III.T seam from G-III.B seam from rise side of overlapping G-III.T &G-III.B seam.

6.3 DIMENSION & PURPOSE OF MINE ENTRIES

The detail of the existing & proposed entries is shown in Table 6.1 along other underground drivage.

6.4 DETAILS OF DRIFTS & STRATA BUNKERS

The brief description of mine entries, underground drivages and other drivages / strata bunkers is given in Table 6.1.

Job No: 501085

CONTRACTOR CONTRACTOR

Table - 6.1: Brief Description of Mine Entries & Drivage

Entries Name / No.	Size (X-section /length) (m_x m /m)	Length/Depth (m)	Gradient (1 in / vertical)	Purpose
Existing Mine Entries				
Incline No. 1	4.2x 2.5	164 m	1 in 4	Main Intake Belt/coal transport
Incline No. 2	4.2x 2.5	164m.	1 in 4	Main intake Traveling/ Haulage roadway
Air Shaft	5.0 m Dia	45m	Vertical	Main Return airways
Existing underground drivage				
Drift No.1	40m	40m	1 in 4	GIIA to GIIIB ,Intake & Travelling
Drift No.2	40m	40m	1 in 4	GIIA to GIIIB ,Intake & Haulage
Staple Pit (16L/2D)	5.0m Dia.	11m	Vertical	Return
Staple Pit (16L/2D)	5.0m Dia.	11m	Vertical	UG Bunker
Staple Pit (46L/2D)	5.0m Dia.	11m	Vertical	UG Bunker
Proposed Underground Drivage	To cross		Two	Faults F2-F2 & F3-F3
Air shaft	5 m dia.	45m	vertical	Intake airways
Drift 1 & 1A	4.2x 2.5	25m	1 in 5	Haulage / Material transport /Intake
Drift 2 & 2A	4.2x 2.5	25m	1 in 5	Intake airway/Travelling Roadway
Drift 3 & 3A	4.2x 2.5	25m	1 in 5	In seam Return
Drift G-III B TO G-IIIT	4.2x 2.5	50x2m	1 in 5	Intake and transport
Staple pits for ventilation	4.8 m dia. 2 no	20 mx2	Vertical	In seam
Strata Bunker (100t), 2	4.8 m dia	10	Vertical	Coal Bunkerage

CHAPTER-VII

MINING STRATEGY

7.1 SURFACE CONSTRAINTS DURING DEVELOPMENT

The EMP report has been prepared and approved for development and depillaring for a mining area of 5.02 sq. km. The surface of the proposed mine take is occupied by forest, agricultural land, village and basties. Few village roads and forest roads also exist within the proposed mining area.

7.2 MINE BLOCKING

As mentioned earlier the total Block area is 10.54 sq. km. Out of which, about 9 sq. km area is considered to be workable. The average length of dip is about 2 Km where as total strike is about 7 Km. For such an extensive property, it is not advisable to work through single unit keeping in view of length of strike panel more than 3 km. It is proposed to work this property in two units which will ease the mine transport and ventilation system. At the same time, traveling of men will be about 6 Km to and fro as envisisaged in RPR 99.

In the <u>Unit-I</u> of mine operation (presently considered for) the boundaries are:-

North - Fault F9-F9 & 15m HCL of seam.

South - Fault F7-F7 and its extension up to Fault F10 and

3meparting with III top & III-bottom.

West - 15m HCL of GIIA seam, Road to mine.

East - Fault F8, F10. Mining area. - 4,69 sq. km.

Unit-2

North - Fault F7-F7 and its extension up to fault F10.

South - Fault F12, F4 & F11

East - Fault F10 & F11.

West - 15M HCL of G-III Seam

Area - 4.25 sq. km (approx.) geological

This unit may be exploited through separate mode of entry or from the same unit, to be decided in later stage.

7.2 GEO-MINING CHARACTERSTICS:-

Seam G-III Bettom has attained its workable thickness in the entire area whereas workability in G-II A is limited up to Unit-I (2.5 sq. km). G-III top is workable in small patch of 0.35 Sq. km area in north side and 1 Sq. Km in the southern side of main dip. The seams are

Job No: 501085

dipping towards east. Seams are occurring at a depth of minimum 35m to maximum 120 m from the surface. Seam G-II A and G-III bottom and G-III top are contiguous in some portion of mining area and they are proposed to be worked as per statutory provisions of Coal Mines Regulations.

7.3 MODE OF ENTRY

The original PR has envisaged driving two inclines (4.2x2.5 sq. m 1 in 4) and one return air shaft (5m dia, 45 m depth). Due to non-availability of land, the sets of inclines had been re-located near B.H.No.179. These two inclines have been driven at 1 in 4 having a cross section area of 4.2x2.5 sq. m. After driving 200m along main dip in G-II A seam a pair of rising incline have been driven at suitable gradient 1 in 4 having cross section of 4.2 x 2.5 sq. m. up to G-III bottom seam.

An airshaft has been sunk to serve as main return.

The details of existing entries are given below:-

SI. No.	Shaft / Incline	Purpose	Dimension (width, height & length)
11- 1	Incline No.1	Coal transport & traveling, Main Intake airway.	4.2 x 2.5 Gradients 1 in 4, 164m.
2.	Incline No.2	Material transport, main Intake airway to G-III B & G-II A.	4.2 x 2.5 Gradients 1 in 4, 164m.
3.	Air shaft	Main return airway up to G-IIA	5m dia, 45m depth.
4	Air shaft (PROPOSED)	Main Intake airway up to G-II A	5m dia, 45m depth.

The location of the entries was considered by the following considerations:-

- (a) Coal seam should touch as early as possible to reduce the gestation period.
- (b) Entries should be away from Geological disturbances and adequate hard cover is available.
- (c) The area should be free from surface constraints like village, nalla etc.
- (d) Entries should not touch the seam at a point where the seam is thin, otherwise heightening of roof in stone would be required.

The length of main dip heading would be around 2.3 km in G-III Bottom.

The Unit-2 area can be worked through a separate pair of inclines, preferably in an area where land can be acquired easily and the topography suits for pit infrastructure development.

7.4. MINING & MINE DEVELOPMENT STRATEGY

After touching of coal seam G III Bottom & G-II A, main dip drivage of five headings in each seam have been continued up to the eastern boundary. The total length of main dip in Seam G II (A) is about 1.4 Km and that of G-III Bottom is 2.3 Km.

Bottom Approach to G-III & G-III top seams:-

The original PR envisaged driving a pair of drifts from G-II A seam to G-III bottom seam. At present, the site of inclines is lying in the 15m Hard cover line of G-II A seam & G-III B Seam. The existing inclines had been driven at 1 in 4 and touched seam G-III B at about 30m and G-II A seam at 40m depth from surface. The Hard cover available at G-III Bottom seam is about 14.75m composed of coarse grained sandstone and shale. From these point entries to Seam G-III Bottom is not possible due to unconsolidated strata. The drift driven to G-II A seam and main dip have been driven for 200m, further rising drift at 1 in 4 was driven to touch G-III B Seam.

Five headings main dip panel in G-III Bottom is driven which is super imposed with the workings of main dip of G-IIA Seam.

The overlying seam of Seam-III bottom is G-III top which occurs in two workable patches. The northern most patches are about 0.35 sq. km of poor grade (D, E &F) and southern patch is about 1 sq. km. The parting between workable southern patch of G-III top seam and G-III Bottom seam varies from 9m to 3m (limiting the boundary of mine). It is proposed to enter the G-III top seam, from the level galleries of G-III bottom seam through drifts and staple pits from rise side of the overlying portion. A pair of rising drift for intake and transport and one staple pit for return will be driven. One more workable patch in III top seam exists above the main trunks headings of the mine. To connect both, workable patches for transport and ventilation network, thin seam drivage is involved for which capital provision has been made in A-8.1

Beneath the ponds, nalla, development will be the final operation. As a safety measures, about 60m barrier pillar will be left against nallas. The HFL of Kholar nalla shall be determined and marked and monitored for precautionary observations.

Job No: 501085

7.5 PANEL WISE RESERVES STATEMENT

The panels have been projected in all workable seams. The reserves statement for Seam III T, III B and Seam II A are enclosed in the following pages as given below in Table.

Job No: 501085

VII-4/6

PANEL-WISE RESERVE OF BAGDEWA UNDERGROUND MINE

(In Tonne)

Panel No.	Length	Width(m)	Thickness (m)	Sp.Gravity	Reserve	DEV	DEP	Barrier
MD	400	200	100					
17	::550	132	1.9	1.52	231040	74348.67	23925.4	
17	175	132	2.0	1.52	220704	71022.55	121077.3	41933.7
TO	200	132	1.8	1.52	63201.6	20338.27	A COLUMN TO	12008
T8		450 .	1.6	1.42	59980.8	19301.82	32905.23	11396.3
Т9	250		2.4	1.47	396900	127722.4		754
T1	500	132		1.47	164934	53075.76	90482 13	31337.
T2 .	₹500	132	1.7		168696	54286.37	92545:95	
, T3	250	132	1.8	1.42	89034			16916.
T4	250	132.	1.9	1.42			43702:25	15135.
MDT	500	76.5	1.7	1.42	79662	25635:23	50654.88	17543.
	250	76.5	1.7	. 1.42	92335.5	29713.56		8771.8
T5	550	102	1.9	1.40	46167,75	14856.78	25327.44	
T6	450	102	1.9	1.42	149226	48020.93	81864.78	28352.
					123838.2	39851.13	67937.14	23529.
		4			1885719.9	606824.6	679266.2	314389
-					100		1.5	
-	100000000000000000000000000000000000000	TOTAL	EXTRACTABLE	E (MT)	1.2861		37	V
EAM-III BOT	TOM:	William Control of			No all divines in	5/20		
Panel No.	Length	Width(m)	Thickness (m)	Sp.Gravity	Reserve	DEV	DEP *	Barrier
		102	2.2	1.42	525769.2	169192.5	54446.16.	10
MD-IIIA 17	1650	76,5	2/25	1,42	366626:25	117980.3	37966.07	
MD-IIIB	1500		2.75	1.47	432951.75	139323.9	44834.42	5
MD-UIC "	1050	102	1.8	1.42	320522.4	103324.1	175837.3	60899.
dII-1	950 "	132		1.42	416116.8	133906.4	- 228280	79062
111-2	1925	132	2.4		438609.6	141144.6	240619.5	83335
- III-3	975	132	2.4	1,42		29734.32	50690.27	175
111-4	250	132	2	1.4	92400		141903.8	49146.
-111-5	1600	132	- 2.3	1.42	258667.2	83239.1	The second secon	
111-6	950	132	12	1.42	356136	114604.6	.195374.8	67,665
111-7	550	132	2.1	1.47	224116.2	72120.59	122949.2	42582
	150	132	2 1	1.42	56232	18095.46		10684
	550	132	2.2	1.4	223608	7.1957.05	122670,4	42485
111-8	950	. 132	1.9	1.42	-338329;2	108874.3	185606	64282
-III-9	550	132	2	1.42	206184	66350.01	113111.7	39174.
-11	150	132	. 2	1,42	56232	18095.46	118767.3	10684.
- 3	550	132	2.1	1.42	216493.2	69667.51	218982	41133.
111.40	900	132	2.4	1.4	399168	128452.3	131731.3	75841.
-III-10 °	and the same of th	132	2.25	1.47	2401245	77272.06	4	745623
III-11: * :	550	132	2.3	1.47	78101.1	25032,93	103788.3	44839
Contract to	175		.3	1.47	189189	60881.02	164012	35945
	{325	132	2.2	1.42	298966.8	96207:52		-50803
111-12	725	132		1.42	76976	24127.28	29273.63	14245
	200	132	2	1.47	53364	17171757.	180978.7	10138
	125	132.	2.2		The second second second	106160	1000102	-62679
III-13	7800	132*	2.2	1.42	329894.4		1216200	25346
A.	250	132 -	2:75	1,47	133402.5		131620.9	and the second second section
III-13A	800 -	132	- 1.6	1:42	The second secon		138818.9	
311-14	675	132	2	1.42	253044	81429.56		48078
	175	132	2.1	1.47	71309.7	22947.46	172752.4	13548
·III-15 .	700	132	2.4	1.42.	314899.2	101334.6	128537.8	
III-16	525	132	2,3	1.47	234303.3	75398.8	1	44517
110	150	132	2.4	1.47	69854.4	22479.15		13272
111-17	475	132	1.9	1.42	169164.6	54437.17	374811.4	
111-17	1350	132	2.7	1.42	. 683218.8	219859.8	P4	12981
		132	2.7	1.42	101217,6	32571.82	156480.9	19231
111.40	200	132	2.8	1.47	285238.8	91789.85	98972.75	54195
111-19	525	Name and Address of the Owner, where the Publisher of the Owner, where the Publisher of the Owner, where the Owner, which is the Owne	275	1.42	180411	58056 26	49357.84	34278
111-20	350	132		1.42	89971.2	28952.73		
111-21	200	132	2.4	And in concession in concessio	The second second second	174168.8	2000,012	10283
111-22	1050	132	275	1.42	541233		239511.5	
140	475	132	3	1.42	38400	81007.05	209011:0	8295
111-23	750	132	3	1.47	436590	140494.7	1400000	-
	175	132	3	1.47	101871	32782:09		- Annual Contract of the local division in t
/III-24	420	132	3.2	1.47	260789.76		92020.12	
111-25	-350	125	2.7	1.42	167737.5		- IV	31870
					10567354	3419241	4777496	17670

TOTAL MINEABLE (MT)
TOTAL EXTRACTABLE (MT)

12.39236 8.19649

VII - 5/6

RESERVE OF BAGDEWA UNDERGROUND MINE

Panel No.	Length	Width(m)	Thickness (m)	Sp.Gravity	Reserve	DEV	DEP	Barrier
Drift	600	90		The strains			10 E 88 7	
Main Dip	1350	102	2.0	1.41	388314	124959.4	213027.5	
11-1	125	132	1.6	1.4	36960	11893.73	20276.11	7022.4
11-2	215	132	2.2	1.147	71614.092	23045.41.		13606.68
11-3	310	132	2.4	1.42	139455.36	44876.73	76504.65	26496.52
11-4	225	132	2.4	1.42	101217.6	32571.82	55527.57	19231.34
11-5	950	132	2.0	1.47	368676	118639.9	202254.2	70048.44
11-6	600	132	2.0	1.45	229680	73911.02	126001.5	43639.2
11-7	600	132	1.6	1.52	192614.4	61983.31	105667.5	36596.74
11-8	175	132	2.0	1.47	67914	21854.73	37257.35	12903.66
11-0	325	132	2.0	1.47	126126	40587.35	69192.22	23963.94
	150	132	2.0	1.47	58212	18732.62		11060.28
11-9	600	132	1.9	1.42	213681.6	68762.74	117224.9	40599.5
II-10	600	132	1.9	1.42	213681.6	68762.74	117224.9	40599.5
II-10A	150	132	2.4	1.45	68904	22173.31	37800.46	13091.76
11-10/4	150	132	2.4	1.45	68904	22173.31		13091.76
	650	132	2.4	1.45	298584	96084.33	163802	56730.96
II-11	550	132	1.7	1.4	172788	55603.18	94790.8	32829.72
11-11	175	132	2	1.42	65604	21111.37		12464.76
	575	132	2.5	1.47	278932.5	89760.48	153021.2	52997.18
11-12	800	132	2	1.42	299904	96509.11	164526.1	56981.76
11-12	000	102	275-394-397-4032		3461767.2	1113997	1793386	583956.1

MINEABLE (MT) EXTRACTABLE 4.044 2.9094

	RESERVES (MT)		
SEAM	MINEABLE	EXTRACTABLE	
SEAM-III T	2.2	1.286	
SEAM-III B	12.39	8.19	
SEAM- IIA	4.044	2.9	

18.63 12

CHAPTER-VIII

METHOD OF MINING

8.1 PROPOSED MINE DEVELOPMENT

A. Approach to Seams

The existing approach to the G-III B and G-II A Seam is through two inclines and one return air shaft. Two rising drift has been made from G-III B to G-III T from main incline. One additional air shaft has been provided in this RPR for fulfilling the ventilation requirement of the mine.

B. Trunk Roadways Development

It is proposed to form main trunk roadway in the all the three seams through the center of the property. The central main dip would rationalize the transportation of coal & materials. This would rationalize the ventilation system of the mine with reasonably long panels. The galleries in the seams have been developed superimposed. Staple pits have been provided for better ventilation.

C. Panel Development:

In all the three seams, it is proposed to form panels on either side of the main trunk roadways, wherever possible. The panels have been kept self draining as far as possible taking into consideration the superimposition.

D Sequence of Development :

Immediately after the development in the main dip has reached the dip most point, development is proposed in the G-III T seam. After development and depillaring of panels in seam G-III T the depillaring in panels of G-III B Seam would commence in the overlying superimposed area and area free of overlying G-III T seam will be depillared simultaneously. The final extraction of the trunk-roadways would be taken up from the dip most side only after final extraction of working panels, on either side of the trunk roadways. After exhaustion of reserves in panels, the standing pillars in these trunk roadways would be depillared. The extraction sequence would be from dip to rise.

E EXISTING PANEL'S:

N-8, N-9 and S-9 are being worked in G-III B seam producing 0.62Mty.

N-8- 130mX680m N-9- 130mX560m S-9- 130mX1400m

Job No: 501085

VIII-1/10

8.1.1 BOARD AND PILLAR:

Mining parameters (B&P)

The various mining parameters envisaged in a panel are:

No. of headings - 6
Gallery width - 4.2 m

(Subject to permission from DGMS)

Development height - Full seam thickness up to 3.0 m

Extraction Height - Full seam thickness
Depth of proposed workings - 30-120m (mining area)

Pillar size - 26mx26m (centre to centre)

Panel width - 134.2m

Panel length - Ranging 400 to 1500m

The geo-mining parameters of mining area have great influence on the choice of mining method. Following are some of the parameters that have been taken in account while making selection of mining methods:-

(a) Workable Seams :-

As mentioned earlier, the Bagdewa mine envisages to exploit three seams viz., G-III top, G-III bottom. & G - II A.

(b) - Surface features :-

The following surface features are present in the proposed mining area:-

- a) Villages Amarpur (part), Bagdewa, Vijaypur & some basti.
- b) Kholar nala
- c) Roads

Due precautions and all relevant statute should be taken in to consideration during exploitation of seams to protect these surface features.

(c) Dip & Strike :-

The seams and the associated coal measures strata exhibit gentle dip of 3° to 4° towards East to SE in North & NE to NNE in South portion.

(d) Dirt Bands :-

Though all the seams considered for exploitation are generally free of bands at places it has bands of less than 30 cm mostly composed of shaly to carb shale.

(e) Roof & Floor:-

The seam wise roof and floor are given in the following table :-

Seam	Roof	Floor	
G-III Top	Coarse grained SST to shale and SST at intervals	Fine grained SST, shaly SST argillaceous.	
G-III Bottom	Argillaceous	Fine to medium coarse grained SST	
G-IIA	Coarse grained sandstone in North argillaceous	Predominantly argillaceous, shale / sandy-shale.	

(f) Cavability of immediate roof:-

The immediate roof is generally coarse to medium coarse grained sandstone and the floor consists of sandy shale / carb. shale to sandstone, argillaceous nature. In considerable area, the seams are occurring as contiguous seam which has to be extracted simultaneously.

(g) Depth of coal seam:-

Seam-wise depth range is given as below:-

Seam	Workable Depth range (m	
G-III Top	30-120 30-120 35-110	
G-III Bottom		
G-IIA		

(h) Thickness & grade of coal seam :-

The seam wise thickness & grade are as under:-

iai All and a second	Workable Thickness range (m)	Grade
G-III Top	1.2-2.4	C-A
G-III Bottom	1.2-3.5	A-B
G-IIA	1.2-2.64	C-A

(i) Faults:

Five number of faults have been deciphered in the proposed mine area. Rest of seven faults will be falling outside the present considered area.

Job No: 501085

VIII-3/10

(j) Incubation Period:

The incubation period is yet to be determined. However, based on the experience of this coalfield it is considered to be six to nine months.

(k) Gassiness of the Seam :-

The gassiness of all the workable seams have been determined and seams have been classified as Degree-I.

8.2 PROPOSED METHOD OF MINING

Opencast Mining:-

A small quarriable patch North West of approved Bagdewa UG had been planned in a area of 23 Ha. Earlier a scheme was prepared to exploit G-III Bottom & G-II A seam lying in lower cover zone having 1.17 Mt of reserve with stripping ratio of 6 cum/te. The target capacity of OC patch was kept as 0.20 Mty. On detailed exploration one more patch in the southern most geological boundary (falling in Phase-II) was also identified which may be amenable for opencast. This reserve will be exploited in the later stage after completion of underground working.

8.3.1 UNDERGROUND MINING:-

Long wall Mining:-

Considering the various geo-mining characteristics of the deposit, Seam G-III bottom is not amenable for long wall mining because of presence of stone band in coal seam G-III B. Thickness and reserve does not suggest for deployment of capital intensive long wall system.

8.3.2 Bord & Pillar Mining :-

Continuous Miners:-

This system of mining is well established in other countries. SECL is in the process of introducing this technology in many mines. On detailed study of nature of the floors of workable seams at Bagdewa it is found that the nature of floor is argillaceous to areneceous comprising gray shale, sandy shale and alternate shale and coarse grained sandstone to fine grained sandstone. These strata are generally considered to be inadequate in strength to bear the kinetic thrust / pressure of heavy machines like C.M and plying of shuttle car. The shale normally contains clay which absorbs water and will make the floor unfit for application of such machines. Also a stone band of thickness 30 cm exists in major seam i.e. G-III. This is one of the reasons which do not provide adequate confidence level in selecting continuous miner machines and thereby, Continuous Miner technology is not being envisaged at Bagdewa mine.

LHD:-

Keeping in view the above, this mine is proposed to exploit by Bord & Pillar system of mining deploying LHD as loading machine.

At places where the thickness of seam is less than 2m, extra low height SDL/LHD will be deployed.

8.3.3 Panel Formation / Development

Panel Layout & System of Panel Development:

It is proposed to develop each panel by driving six headings galleries from main dip trunk roadways, in a similar manner as currently practised in Indian underground coal mines. In a strike panel, the pillar size will be 26m (centre to centre) with gallery width of 4.2m. Uniform pillar size & gallery width have been envisaged in the panels for smooth operation), during development of a panel, height of extraction would be the seam height up to a maximum of 3.0m. The panel layouts would be made as favourable for self draining.

System of Mining:-

Main dip development:-

Five headings dip panel is proposed with 25.5m x 25.5m pillar and 4.2 m gallery. Full thickness of coal will be extracted. Blasting of solids will be adepted for winning coal. LHD will be used as a loading machine to discharge coal onto gathering/gate belt. Which will discharge coal in G-II A seam whereas trunk belts will be used in G-III bottom seam. The main dip will have full thickness of seam or moof will be heightened up to 2.5m where seam thickness is less than 2.5m.

Production Parameters:-

Panel in G-III Bott. Seam:-

Height = 2.5m (average) Sp. Gravity. = 1.45

Gallery width = -4.2m

Pull = 1.9m (av.)

No. of faces = 13 (maximum)

No. of panels = 4 No. of blast/shift/panel = 13

Coal/Blast = 4.2x2.5x1.0x1,45

= 15.225 t

No of blast/shift = 13.5

Coal/panel/shift = 15.225 x 13.5

Job No: 501085

G-III / G-II A Seam:-

No. of face = 13 (maximum)

Gallery width = 4.5m Pull = 1 m Sp. gr. = 1.45

Full thickness

Height = 2.0m (av. thickness) Coal / blast = 2.0x4.5x1.45x1

= 13.05 t

No. of blast /shift/panel = 15-16

Coal per day = $15.7x \ 3 \ x \ 13.05x4$

= 2460 t

Say = 2460 t/day.

8.3.4 Proposed System of Depillaring

After development of rise side panels, it shall be effectively sectionalised. The depillaring of these panels would be carried at a later date. The dip most panel will be developed and depillaring will be carried out simultaneously.

The inter-partings between G-III top, G-III bottom and G-II A varies from few meters to 15m. The area lying in contiguity will be developed and depillared simultaneously.

During depillaring operation, each pillar would be divided into two equal rectangular halves by driving a level split gallery having width of 4.5m. The half pillar on dip side is to be sliced first from this split gallery whereas the remaining half pillar on rise side would be extracted from original gallery.

In each half of spitted pillar, number of slices would be three, having width 4.6m, by leaving a rib thickness of 1.8m against Goaf sides. While retreating, rib would be judiciously robbed.

8.3.5. Production from depillaring panel:-

From Split galleries:
Average seam thickness - 2.5m

Width of split gallery - 4.5m

Specific gravity - 1.45

No. of splits - 3 (average)
Coal produced per blast - 4.5x2.5x1x1.45

(pull per blast - 1m)

Considering 1 blast shift/split - 16.31 te
No. of blast/split(3)/panel = 8
No. of panels = 4

Coal/panel/shift-split = 16.31 x 8 Coal per day - 16.31 x 3 x 8x4 - 1565.76 te.

Job No: 501085

VIII-6/10

	luction from slice:-		4 (average)
1.	No. of slices available		4.6m
2.	Width of slice		
3.	Specific gravity	Juli 6	1.45
4.	Pull per blast	-	1.0m
		=	4,
5.	Coal produced per blast per slice	-	4:6x2.5x1.0x1.45
J.	Soci, process	-	16.675 te
6.	No. of shifts per day	-	3
7.	No. of blast / shift/panel-slice	-	5 (average)
8.	Coal produced per day	-	16:675 x 5 x 3x4
9.	Coal from Slice	-	1000.5 Te.
9.	GOAL HOLL SHOOL		
Tota	al coals available from each depillari	ng.p	anel:1
100	Split production	-	1565.76 Te.
	Slice production	-	1000.5 Te
	Coal produce per day		2566.26 te

Considering 96 % recovery,

Coal production from Four depillaring districts = 2460 tpd

In G-II A & G-III Top Seam :-

Coal from Split :-

No. of splits - 3
Av. thickness - 2m
Sp. gravity - 1.45
Width of split - 4.5m

Coal/blast - 2 x 1.45 x 4.5 x 1 (panel)

No. of panels = 4 Taking 8 blast / shift,/panel

Coaliper day -=13.05 x 3 x 4x8 =1252.8 te

Coal from Slices:-

Width of slice - 4.6m
Thickness - 2.0m
- 1.0m
Sp. grade - 1.45
No. of panels = 4

No. of slices available- 4 (average)
No. of blast / shift/panel - 8

Coal / blast - 4.6 x 2 x 1.0 x 1.45

13.34 t

Coal / day - 4 x 3 x 13.34x8

240 t.

Job No: 501085

VIII-7/10

The bolting density in junctions would be enhanced by 25%. Timbers will be placed over steel cogs members to adjust the height and use as indicator of roof movement. Anchorage testing for 10% of roof bolt should be carried out at regular intervals to monitor the efficiency of bolting operation. Strata movement monitoring should also be carried out by using convergence recorder at vulnerable places.

8.6 SUPPORT SYSTEM AT SPLIT GALLERY & SLICE:-

In the split gallery, two pillars ahead of pillar under extraction would be supported by using quick setting resin bolts or cement grouted bolts and steel channels as mentioned earlier to facilitate the movements of SDLs.

In slice, support system should be predominantly being of roof bolting. Occasional timber props may be used as indicator prop and by the side of ribs, steel cogs will be used. Goaf edges will be supported by skin to skin cogs. Goaf edges may be supported with two rows of pit props (mild steel) closely spaced at interval of 0.6m.

It is proposed that once the coal in all seams is touched, RMR study is to be carried out for formulating the systematic support rule and it will be continued after certain period of intervals for preparing fresh support plan when the mine workings gradually progress.

SAFETY ASPECTS

Major safety considerations involved in the mining operations are:

A. Spontaneous Heating & Fire

After depillaring, there is a risk of spontaneous heating in the Goaf area. To prevent such risk, it is necessary to avoid any stray air current in the Goaf by sealing off properly all abandoned accesses to a panel, steadily check the atmosphere in the vicinity of the caving zone (carbon monoxide, carbon atmosphere in the vicinity of the caving zone (carbon monoxide, carbon dioxide, oxygen, methane) by daily samplings and measurements and avoid high levels of head losses in the ventilation circuit. In case of spontaneous heating, a quick sealing procedure (from surface and underground) must be implemented and the required equipment and materials should be ready for use.

Considering that about 20-30% coal will be left in the Goaf, chances of spontaneous heating especially in the depillaring panels is not ruled out. It is desirable that studies may be carried out for spontaneous heating characteristics of the seams. As a precautionary measure, solid barrier between panels has been suggested. Each panel will be connected to the minimum number of airways so that in case of heating, quick sealing off is possible.

Job No: 501085

The bolting density in junctions would be enhanced by 25%. Timbers will be placed over steel cogs members to adjust the height and use as indicator of roof movement. Anchorage testing for 10% of roof bolt should be carried out at regular intervals to monitor the efficiency of bolting operation. Strata movement monitoring should also be carried out by using convergence recorder at vulnerable places.

8.6 SUPPORT SYSTEM AT SPLIT GALLERY & SLICE:-

In the split gallery, two pillars ahead of pillar under extraction would be supported by using quick setting resin bolts or cement grouted bolts and steel channels as mentioned earlier to facilitate the movements of SDLs.

In slice, support system should be predominantly being of roof bolting. Occasional timber props may be used as indicator prop and by the side of ribs, steel cogs will be used. Goaf edges will be supported by skin to skin cogs. Goaf edges may be supported with two rows of pit props (mild steel) closely spaced at interval of 0.6m.

It is proposed that once the coal in all seams is touched, RMR study is to be carried out for formulating the systematic support rule and it will be continued after certain period of intervals for preparing fresh support plan when the mine workings gradually progress.

SAFETY ASPECTS

Major safety considerations involved in the mining operations are:

A. Spontaneous Heating & Fire

After depillaring, there is a risk of spontaneous heating in the Goaf area. To prevent such risk, it is necessary to avoid any stray air current in the Goaf by sealing off properly all abandoned accesses to a panel, steadily check the atmosphere in the vicinity of the caving zone (carbon monoxide, carbon dioxide, oxygen, methane) by daily samplings and measurements and avoid high levels of head losses in the ventilation circuit. In case of spontaneous heating, a quick sealing procedure (from surface and underground) must be implemented and the required equipment and materials should be ready for use.

Considering that about 20-30% coal will be left in the Goaf, chances of spontaneous heating especially in the depillaring panels is not ruled out. It is desirable that studies may be carried out for spontaneous heating characteristics of the seams. As a precautionary measure, solid barrier between panels has been suggested. Each panel will be connected to the minimum number of airways so that in case of heating, quick sealing off is possible.

Job No: 501085

and the contraction of the contr

B. Caving and Strata Control

The seams in the mine are at generally low to moderate depth of cover with a maximum depth of around 120 m. Moreover, parting between the seams is also low. The characteristic of roof rock indicates moderate nature and is not likely to pose difficulty in caving.

It is proposed to undertake scientific studies to determine the cavability characteristics & determination of rock & coal strength properties before commencement of depillaring. Even while depillaring operation, it is proposed for suitable studies to ascertain the parting stability. Appropriate method of strata control should be adopted and practiced in the panels. It would be necessary to experiment and adopt a wider and more effective & efficient strata management. It should form the integral part of the method of mining.

C. Scientific Studies

Considering the above, it is proposed for undertaking scientific studies before commencement of panel extraction and for monitoring during and after the panel extraction. The following studies may be undertaken before commencement of the operations.

- Study of parting stability between the seams for minimum safe parting necessary in case of final pillar/panel extraction.
- Investigation /study for incubation period for seams
- Study of cavability characteristics and establishment of optimum panel size.
- Studies to be undertaken for establishment of method of strata management and control during panel extraction.
- Any other studies as found necessary.
 - It is desirable to have in-house organization & set up as well as engage scientific bodies for monitoring the following:
- Monitoring & study of roof behavior & the strata movement
- Environmental monitoring within and outside the panel under extraction.

CHAPTER-IX

MINING SCHEDULE

9.1 PRODUCTION SCHEDULE

A. Extractable Reserves

Following considerations have been taken into account for estimation of extractable coal reserves in working panels and trunk roadways:

i) Panel layout:

In trunk roadways, 5-headings and 6 headings in the working district have been envisaged. However, some panels have been formed with varying headings owing to disposition of faults and / or block boundary. Presently three no of panels namely N-8, N-9 and S-9 with 7 LHDs and 4 UDMs are operating in the mine.

ii) Working height during development & depillaring :

The B&P panels have been proposed to be developed with full seam thickness (max. thickness 3.0 m). It is proposed that while extraction full seam thickness would be extracted. The gallery width of 4.2m has been considered for reserve estimation in the B&P panel with LHDs & UDMs combination.

iii) Sectionalisation & panel / sub-panel formation :

The formation of sub-panels and sectionalisation of the panels would be done based on the incubation period or other technical requirement. To account for reserves lost in these barriers, average percentage of final extraction has been considered.

iv) Extraction percentage:

The target production from Bagdewa ⊌G mine is proposed to be 2460 TPD and this production can be achieved working four numbers of Strike Panels or three strike panels and two main dip panels. During initial periods of the mine, workings will be concentrated in G III top & bottom seam. G-IIA seam will be depillared where it occurs in contiguity of overlying seam as a simultaneous operation. The production from the development depillaring panel has been considered as 615 tpd deploying 3/2 LHD in G-III bottom seam in each panel. The production from G-II A and G-IIIT will be considered by deploying low/ extra low height/standard height LHD as per requirement and actual condition encountered during operation. The existing productivity in area has been given due consideration.

It is proposed to depillar the developed panel preferably from the bottom / dip most point of the property. DGMS also insists to follow this sequence of operation. This ensures safety as well as smooth operation of the panel extraction. It is also recommended that as soon as panels are developed it should be extracted to avoid repetition of many operational

Job No: 501085