

# Transys Consulting Pvt. Ltd

## Geotechnical Investigation work for Proposed Greenfield project from Spur to Haridwar.

Job No 2152

*Report*  
*MJB, MNB, VUP & Flyover-R1*



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## 1.0 INTRODUCTION

M/s Transys Consulting Pvt Ltd has awarded the work of Geo technical Investigation for the proposed Greenfield project from Spur to Haridwar to M/s Soil Engineering Consultants, New Delhi.

Geotechnical investigation was conducted to characterize and assess the subsurface conditions at the locations of various Structures viz. proposed Major Bridges, Minor Bridges, ROBs, Elevated Viaduct, Vehicular Underpass (VUP). The overall objectives of the exploration were to study and evaluate the stratigraphy of the said project corridor and to obtain geotechnical / geological parameters of the subsurface formations for design and construction of various foundations.

This report presents the details of Geotechnical investigations carried out and data obtained from various field and laboratory tests, their presentation in graphical form, and their compilation for the proposed Structures.

## 2.0 SCOPE OF WORK

- a) Drilling bore holes upto the maximum depth of 30.0 m as per IS code of practice and as per the direction of the Engineer-in-Charge.
- b) Conducting Standard Penetration tests in the bore holes at regular intervals of 1.50m or wherever possible as per IS Code of Practice.
- c) Collecting undisturbed soil samples / core samples from the bore holes at regular intervals or change of strata or wherever possible as per IS Code of Practice.
- d) Recording of water table level in the bore holes after completion of borehole.
- e) Preparation of report summarizing the details of soil classification, analysis of test data, type of foundation etc.

### 3.0 FIELD WORK

#### 3.1 Boring

Bore holes of 150 mm dia. were drilled as per IS code of practice (IS 1892-1979) and as per the directions of the Engineer in charge. The details of Bore holes drilled, Depth of bore hole and the depth of water table are as given below:

**Table 1 : Detail of the Boreholes.**

<b>Chainge</b>	<b>BH No.</b>	<b>Structure</b>	<b>Depth of Borehole (m)</b>	<b>Water Table (m)</b>
0+800	BH 1	Flyover	30.00	4.50
1+530	BH 2	MJB	30.00	2.70
6+380	BH 3	VUP	20.00	13.80
8+020	BH 5	Flyover	30.00	14.10
16+690	BH 6	VUP	20.00	13.30
21+810	BH 7	MNB	20.00	11.30
22+980	BH 8	VUP	20.00	14.20
25+430	BH 9	VUP	20.00	12.25
29+260	BH 11	MNB	20.00	5.50
32+170	BH 12	Flyover	30.00	13.20
33+420	BH 13	MJB	30.00	2.10
33+490	BH 14	MJB	30.00	3.20
35+860	BH 15	MJB	30.00	5.30
38+010	BH 16	MNB	20.00	8.75
39+510	BH 17	MJB	30.00	4.50
39+690	BH 18	MJB	30.00	4.50
40+940	BH 19	VUP	20.00	11.80
42+550	BH 20	MJB	30.00	3.35
43+910	BH 21	Flyover	30.00	10.25
47+950	BH 22	MJB	30.00	3.80
49+900	BH 23	Flyover	30.00	9.80

### **3.2 Standard Penetration Test (SPT)**

These tests were conducted at every 1.50m intervals and every change of strata or wherever possible. The tests were performed by driving into the soil (bore holes cleaned of any loose material) a standard split spoon sampler with the help of a standard hammer with a free fall of 75 cms on a driving head as described in IS: 2131. This head was attached to "A" drill rod to the other end of which the sampler was fitted. The number of blows needed to penetrate the first, second and third stages (each of 15 cms) depth of the sampler length, were noted. The number of blows (N - value) as given in the bore hole data sheets is the numerical sum of blows counted during the second & third stage only i.e. for a depth of 30 cms.

### **3.3 Collection of Samples**

Disturbed and Undisturbed soil samples were collected from the boreholes at regular intervals as per IS Code of practice.

### **3.4 Recording of water table**

Water table was met at varying depth in the boreholes at the time of Soil investigation which was carried out during the month of April 2021. The details are given at Table I above. Fluctuations may occur in measured water levels due to seasonal variation in rainfall and surface evaporation rates as well as flow of water.

## **4.0 LABORATORY TESTS**

A visual and discrete examination of all the soil samples collected was carried out for deciding the number and type of tests to be tested from each bore hole. Based on the strata met at site the following tests were conducted on samples to classify them and to evaluate their index and Engineering properties.

### **4.1 SOIL SAMPLES & BIS CODES**

- a) Grain size distribution as per IS: 2720(Part IV).
- b) Hydrometer Analysis as per IS: 2720(Part IV).

- c) Specific gravity as per IS: 2720(Part III).
- d) Bulk density and dry density as per IS: 2720(Part II).
- e) Moisture content as per IS: 2720(Part II).
- f) Liquid and plastic limits as per IS: 2720(Part V).
- g) Unconsolidated undrained shear tests as per IS: 2720(Part XIII).
- h) Direct Shear Tests as per IS: 2720 (Part XIII).
- i) Consolidation test as per IS: 2720 (Part XII).

## 5.0 General Geology of the Area

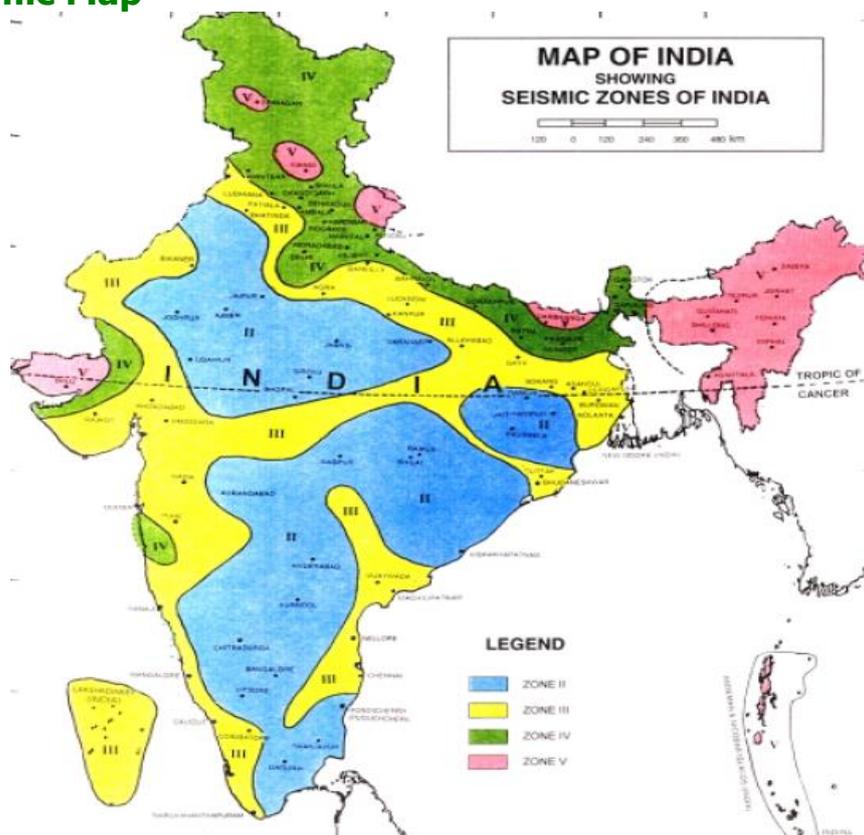
The present location is in the state of Uttarakhand situated on the northern Gangetic plains of India. Most of the state of Uttarakhand lies in the Gangetic Plain. This is a fore-deep, a downwarp of the Himalayan foreland, of variable depth, converted into flat plains by long-vigorous sedimentation. This is known as a geosyncline and the Gangetic Plain is the Indo-Gangetic Geosyncline. This has shown considerable amounts of flexure and dislocation at the northern end and is bounded on the north by the Himalayan Frontal Thrust. The floor of the Gangetic trough (if seen without all the sediments) is not an even plain, but shows corrugated inequalities and buried ridges (shelf faults). Beneath Uttar Pradesh, run the Delhi-Haridwar Ridge (DHR), trending NNE-SSW along New Delhi to the Gharwal region. The Delhi-Muzaffarnagar Ridge (DMR), which trends east to west, running from New Delhi to Kathgodam, in Nepal. The last ridge is the Faizabad ridge (FR), which runs in a curved manner, first east to west from Allahabad to Kanpur and then starts to bend towards the north-east towards Lucknow and carries on in this direction towards the Himalayas in Nepal. The depression that forms between the DMR and the FR, forms the West Uttar Pradesh shelf in the west and the Sharda Depression in the east. The region to the south of the FR, forms the East Uttar Pradesh shelf. There are several faults in the region, among them the Moradabad Fault which trends NE-SW and the Bhairwan Fault in the vicinity of Allahabad. Apart from these there are east-west running tear faults in the region that control

the courses of the main rivers. Earthquakes have occurred in mostly all parts of Uttarakhand. Major earthquakes in the neighbouring states of New Delhi, Uttaranchal, Bihar and from across the Indo-Nepal border have also shaken many parts of Uttar Pradesh. However, it must be stated that proximity to faults does not necessarily translate into a higher hazard as compared to areas located further away, as damage from earthquakes depends on numerous factors such as subsurface geology as well as adherence to the building codes.

## 6.0 SEISMICITY

The seismic hazard map of India was updated in 2016 by the Bureau of Indian Standard (BIS). The project site lies in Zone IV. The tectonic elements of the area are considered capable of generating an earthquake of intensity MSK 7.0. In Seismic design Zone factor,  $Z$  of 0.24 is recommended.

### Seismic Map



## 7.0 LIQUEFACTION

Liquefaction is a process in which a saturated soil loose strength during an earthquake and acquires a degree of mobility sufficient to permit significant movements. In general, fine uniform sands are found to be most susceptible for liquefaction in terms of grain size. It can be stated that soils containing less than 10% fines,  $D_{60}$  between 0.20 mm to 1.0mm, uniformity coefficient between 2 to 5 are most susceptible to liquefaction for given relative density of soil and intensity of earthquake. Thus, uniformly graded materials are more susceptible to liquefaction than well graded materials. Also fine sands are more susceptible than gravelly soils, silty sands, silts or clays.

Assessment of liquefaction potential of foundation strata is made by simplified approach proposed by Seed & Idriss (1983 - 1985) from the SPT data and peak ground acceleration likely to occur at the site. In this method, cyclic shear stress likely to be induced in the foundation strata is first evaluated. Next threshold cyclic shear stress, which is good enough to cause liquefaction, is determined from SPT data and the empirical relations. Finally, comparison of these two stresses is used in the estimation of liquefaction susceptibility of the foundation strata

### 7.1 Liquefaction Analysis:

#### Cyclic Stress Ratio under Earth Quake (CSR)

Stress ratio under earth quake (CSR)

$$= (\tau / \sigma_o)_{\text{earthquake}} = 0.65 (\gamma h a_{\text{max}} / \sigma_o g) \lambda$$

$\sigma_o$  = Effective overburden pressure at depth h

$\gamma$  = Bulk density of soil

$a_{\text{max}}$  = Max. Ground acceleration = 0.24g

#### Evaluation of Liquefaction Resistance (CRR)

$$CRR_{7.50} = 1 / \{ (34 - (N_1)_{60CS}) + (N_1)_{60CS} / 135 + 50 / \{ 10 * (N_1)_{60CS} + 45 \}^2 - 1 / 200$$

$$(N_1)_{60} = NC_{60} C_N$$

N = Uncorrected SPT count

$C_N$  = factor to normalize  $N_m$  to a common reference effective overburden stress =  $(p_o / \sigma_o)^{0.5}$

$$C_{60} = C_{HT}C_{HW}C_{SS}C_{RL}C_{BD}$$

$C_{HT}$  = Correction for Hammer Energy Ratio

$C_{BD}$  = Correction factor for the borehole diameter

$C_{RL}$  = correction factor for rod length

$C_{SS}$  = Correction for samples with or without liners

Correction for Fineness content

$$(N_1)_{60cs} = \alpha + \beta (N_1)_{60}$$

$$CRR_L = CRR_{7.50} * k_m$$

$k_m$  Correction factor

For earthquake magnitude other than 7.5 =  $10^{2.24} / (M_{7.5})^{2.56}$

Liquefaction occurs if  $CSR_L \geq CRR$

**Data considered for Liquefaction:**

Magnitude of Earth quake = 7.0.

$$a_{max}/g = 0.24$$

Water table assumed for Calculation = considered 3.0m rise water table encounter at the time investigation.

The Liquefaction analysis has been calculated and given at **Annexure II.**

## 8.0 SUB SOIL PROFILE & STRENGTH CHARACTERISTICS OF SOIL

### Flyover @ 0+800

At this structure One Borehole namely (BH 1) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto the depth drilled. However from 14.50m to 17.50m depth a layer of Silty Clay of

Medium Plasticity (CI) was observed. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 5 to 30 upto the depth drilled. For evaluating the shear parameters Direct shear Tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is susceptible to liquefaction.

#### **MJB @ 1+530**

At this structure One Borehole namely (BH 2) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto the depth drilled. However from 14.0m to 20.5m depth a layer of Silty Clay of Low to Medium Plasticity (CL-CI) was observed. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 6 to 30 upto the depth drilled. For

evaluating the shear parameters Direct shear Tests/Unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is susceptible to liquefaction.

#### **VUP @ 6+380**

At this structure One Borehole namely (BH 3) was drilled upto 20.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelog. It can be seen from the plot that the SPT values are generally varying from 10 to 26 upto the depth drilled. For evaluating the shear parameters Direct shear Tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is not susceptible to liquefaction.

#### **Flyover @ 8+020**

At this structure One Borehole namely (BH 5) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting

sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto the depth drilled. However from 10.0m to 12.0m depth a layer of Silty Clay of Medium Plasticity (CI) was observed. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 9 to 14 upto 8.0m depth and below 8m depth SPT values are varying from 17 to 34 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is not susceptible to liquefaction.

#### **VUP @ 16+690**

At this structure One Borehole namely (BH 6) was drilled upto 20.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of alternate layers of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) and Silty Clay of Medium Plasticity (CI) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and

High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 11 to 34 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ Unconsolidated undrained shear test were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is not susceptible to liquefaction.

#### **MNB @ 21+810**

At this structure One Borehole namely (BH 7) was drilled upto 20.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 8 to 29 upto the depth drilled. For evaluating the shear parameters Direct shear Tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is not susceptible to liquefaction.

### **VUP @ 22+980**

At this structure One Borehole namely (BH 8) was drilled upto 20.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of Silty clay of Medium Plasticity (CI) upto 5.0 m depth followed by medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 17 to 30 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ Unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is not susceptible to liquefaction.

### **VUP @ 25+430**

At this structure One Borehole namely (BH 9) was drilled upto 20.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of alternate layers of Silty Clay of Medium Plasticity (CI) and medium dense

Sandy Silt with Gravel (SM-ML) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 6 to 22 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ Unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is not susceptible to liquefaction.

#### **MNB @ 29+260**

At this structure One Borehole namely (BH 11) was drilled upto 20.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML) upto the depth drilled. However from 0.0m to 2.0m depth and from 15.50m to 17.50m depth a layer of Silty Clay of High plasticity (CH)/ Silty Clay of Medium Plasticity (CI) was observed. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 6 to 19 upto the

depth drilled. For evaluating the shear parameters Direct shear Tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is not susceptible to liquefaction.

#### **Flyover @ 32+170**

At this structure One Borehole namely (BH 12) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of alternate layers of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) and Silty Clay of Medium Plasticity (CI) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 10 to 35 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is not susceptible to liquefaction.

#### **MJB @ 33+420**

At this structure One Borehole namely (BH 13) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular

intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of alternate layers of medium dense Silty Sand with Gravel (SM) and Silty Clay of Medium Plasticity (CI) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 2 to 6 upto 12.0m depth and below 12 m depth SPT values are varying from 15 to 40 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is susceptible to liquefaction.

#### **MJB @ 33+490**

At this structure One Borehole namely (BH 14) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of alternate layers of medium dense Silty Sand with Gravel (SM) and Silty Clay of Medium Plasticity (CI) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to

presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 6 to 41 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is susceptible to liquefaction.

#### **MJB @ 35+860**

At this structure One Borehole namely (BH 15) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of alternate layers of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) and Silty Clay of Low to Medium Plasticity (CL-CI) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 9 to 29 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at

Annexure II. It can be seen from the results that the strata is susceptible to liquefaction.

#### **MNB @ 38+010**

At this structure One Borehole namely (BH 16) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto 6m depth followed by Silty Clay of Low to Medium Plasticity (CL-CI) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 4 to 26 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is susceptible to liquefaction.

#### **MJB @ 39+510**

At this structure One Borehole namely (BH 17) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the

classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto 16m depth followed by Silty Clay of High Plasticity (CH) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 6 to 21 upto 22m depth and below 22m depth SPT values are varying from 23 to 35 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is susceptible to liquefaction.

#### **MJB @ 39+690**

At this structure One Borehole namely (BH 18) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of alternate layers of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) and Silty Clay of Medium Plasticity (CI) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been



plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 6 to 37 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is susceptible to liquefaction.

#### **VUP @ 40+940**

At this structure One Borehole namely (BH 19) was drilled upto 20.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of Silty Clay of Medium Plasticity (CI) upto 8.0 m depth followed by medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto 17.50m depth. Below 17.50m depth the strata is classified as Silty Clay of High Plasticity (CH) upto the depth drilled. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 7 to 11 upto 7.0 m depth and below 7m depth SPT values are varying from 19 to 35 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been

carried out and the details are given at Annexure II. It can be seen from the results that the strata is not susceptible to liquefaction.

#### **MJB @ 42+550**

At this structure One Borehole namely (BH 20) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto the depth drilled. However from 17.50m to 20.50m depth a layer of Silty Clay of Medium Plasticity (CI) was observed. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 9 to 28 upto the depth drilled. For evaluating the shear parameters Direct shear Tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is susceptible to liquefaction.

#### **Flyover @ 43+910**

At this structure One Borehole namely (BH 21) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the

classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto the depth drilled. However from 5.0m to 9.0m depth and from 14.50m to 16.0m depth a layer of Silty Clay of Medium Plasticity (CI) was observed. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 8 to 28 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ Unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is susceptible to liquefaction.

#### **MJB @ 47+950**

At this structure One Borehole namely (BH 22) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto the depth drilled. However from 6.0m to 9.0m depth a layer of Silty Clay of Medium to High Plasticity (CI-CH) was observed. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic

strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 10 to 32 upto the depth drilled. For evaluating the shear parameters Direct shear Tests/ Unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is susceptible to liquefaction.

## 9.0 DESIGN CRITERIA

Any foundation is to be safe against possible failure against

- a) Excessive Shear failure (the bearing pressure should be within permissible limits) and
- b) Excessive settlement.

The latter depends upon not only on the type of soil in the foundation but also on the type of foundation, material used for construction and functionality of the structure.

### 9.1 Design Methodology

#### **Flyover @ 0+800, 8+020, 32+170, 43+910 & 49+900**

Bored - Cast - in situ Piles of 1.0m and 1.20m diameter are analyzed.

#### **VUP @ 6+380, 16+690, 22+980, 25+430 & 40+94**

Bored - Cast - in situ Piles of 1.0m and 1.20m diameter are analyzed. Scour levels provided by the client.

#### **MNB @ 21+810 & 29+280**

Raft foundation has been analysed at 1.0 m depth below bed level with an allowable settlements of 75 mm has been considered.

#### **MNB @ 38+010**

Bored - Cast - in situ Piles of 1.0m and 1.20m diameter are analyzed. Scour levels provided by the client.

### **MJB @ 1+530, 33+420,33+90,35+860,39+510,39+690,42+550 & 49+900**

Bored - Cast - in situ Piles of 1.0m and 1.20m diameter are analyzed. Scour levels provided by the client.

#### **9.1.1 Open foundation**

The safe bearing pressure from Shear failure criteria can be obtained, using the Equation given below

$$Q_u = q ( N_q - 1 ) S_q D_q I_q + 0.5 B \gamma N_\gamma S_\gamma D_\gamma I_\gamma W'$$

where,

B = Width of the footing in m

$D_q, D_\gamma$  = Depth factors

$S_q, S_\gamma$  = Shape factors

$I_q, I_\gamma$  = Inclination factors

$N_q, N_\gamma$  = Bearing capacity factor

q = Effective overburden pressure at foundation, in t/sqm

W' = Water table correction factor

$\gamma$  = Bulk unit wt. of foundation soil, in t/cu.m

#### **b) Settlements:**

i) Soil profiles are given for each bore hole. The Soil profile which is likely to cause greater settlements is to be considered for calculations.

ii) The imposed load at the foundation level is likely to compress the soil upto a depth of approximately equal to 1.5 B below the foundations.

iii) The settlements can be calculated using IS-8009 part-I.

#### **When the strata consists of Plastic strata**

when the Foundation resting on plastic strata and its influence within the plastic strata the settlements can be obtained using the equation as per

#### **IS: 8009 (part I)**

$$S_f = H * m_v * \Delta P$$

Where

H = thickness of layer under consideration (cm).

$m_v$  = volume of compressibility

$\Delta P$  = Increase in the effective stress due to external load.

### 9.1.2 Bored cast in-situ concrete pile

The ultimate load carrying capacity ( $P_u$ ) of piles is given by the following formula:

$$P_u = A_p ( N_c \cdot C_p + \frac{1}{2} D \gamma N_r + P_d N_q ) + \sum K P_{di} \tan \delta A_{si} + \alpha c \cdot A_s$$

$$P_u = P_{pu} + P_{su}$$

$P_{pu}$  = Ultimate bearing resistance

$$= A_p ( N_c \cdot C_p + \frac{1}{2} D \gamma N_r + P_d N_q )$$

$P_{su}$  = Ultimate shaft resistance

$$\sum K P_{di} \tan \delta A_{si} + \alpha c \cdot A_s$$

$A_p$  = Cross sectional area of the pile toe  $m^2$

$D$  = Stem diameter in mm

$\gamma$  = Effective unit weight of soil at pile toe in  $t/m^3$

$P_d$  = Effective overburden pressure at pile toe in  $t/m^2$   
i.e 20 X diameter (as per IRC 78-2014).

$N_r$  &  $N_q$  = Bearing capacity factors depending upon the angle of internal friction  $\phi$  at toe

$\sum$  = Summation of n layers in which pile is installed

$K$  = Coefficient of earth pressure  
= Taken 1.5 (as per IRC 78- 2014 Appendix 5)

$P_{di}$  = Effective overburden pressure in  $t/m^2$  for the  $i^{th}$  layer where  $i$  varies from  $i$  to  $n$

$\delta$  = Angle of wall friction between pile and soil (may be taken equal to  $\phi$ )

$A_{si}$  = Surface area of pile stem in  $m^2$  in  $i^{th}$  layer where  $i$  varies from 1 to  $n$ .

FOS= Factor of Safety considered as 2.5 ( as per IS 2911 part 1 sec 2)

For vertical Capacity of pile, weight of pile has not been considered.

## 10.0 COMPUTATIONS

The Net Safe bearing capacity for the Box foundation, Vertical, Uplift and lateral carrying capacities of the Bored Cast in Situ Piles of 1.0m and 1.20m dia are calculated and are given at **Annexure I**.

## 11.0 RECOMMENDATIONS

### Flyover @ 0+800, 8+020, 32+170,43+910 & 49+900

Bored Cast in-situ Pile Foundation of 1.0 m and 1.20m dia are recommended at cut off level of 2.0m and 2.30m respectively. The Length of pile and Safe load carrying capacity of the pile can be taken as given below:

Chainage	BH No.	Pile Dia (cms)	Length of Pile (m)	Safe Load carrying capacity of Pile (t)		
				Vertical	Uplift	Lateral
0+800	BH 1	100	29.0	300.0	160.0	10.0
		120	29.0	400.0	210.0	18.0
8+020	BH 5	100	20.0	330.0	150.0	20.0
		120	20.0	400.0	180.0	40.0
32+170	BH 12	100	24.0	140.0	100.0	30.0
			26.0	160.0	110.0	30.0
			28.0	170.0	120.0	30.0
		120	24.0	180.0	130.0	50.0
			26.0	200.0	140.0	50.0
			28.0	220.0	150.0	50.0
43+910	BH 21	100	21.0	300.0	150.0	20.0
		120	21.0	400.0	180.0	30.0
49+900	BH 23	100	23.0	330.0	150.0	20.0
		120	23.0	400.0	190.0	35.0

**VUP @ 6+380, 16+690, 22+980, 25+430 & 40+940**

Bored Cast in-situ Pile Foundation of 1.0 m and 1.20m dia are recommended at cut off level of 2.0m and 2.30m respectively. The Length of pile and Safe load carrying capacity of the pile can be taken as given below:

Chainage	BH No.	Pile Dia (cms)	Length of Pile (m)	Safe Load carrying capacity of Pile (t)		
				Vertical	Uplift	Lateral
6+380	BH 3	100	18.0	280.0	120.0	20.0
			19.0	300.0	140.0	20.0
		120	18.0	370.0	160.0	40.0
			19.0	400.0	170.0	40.0
16+690	BH 6	100	18.0	250.0	110.0	20.0
			20.0	300.0	140.0	20.0
		120	18.0	340.0	140.0	50.0
			20.0	400.0	180.0	50.0
22+980	BH 8	100	18.0	300.0	140.0	35.0
		120	18.0	400.0	170.0	50.0
25+430	BH 9	100	18.0	250.0	110.0	25.0
			19.0	270.0	120.0	25.0
		120	18.0	330.0	140.0	40.0
			19.0	360.0	160.0	40.0
40+940	BH 19	100	18.0	160.0	100.0	15.0
			21.0	180.0	120.0	15.0
		120	18.0	200.0	130.0	25.0
			21.0	220.0	150.0	25.0

**MNB @ 38+010 & MJB @ 1+530, 33+420, 33+490, 35+860, 39+510, 39+690, & 42+550**

Bored Cast in-situ Pile Foundation of 1.0 m and 1.20m dia are recommended at cut off level of 2.0m and 2.30m respectively. The Length of pile and Safe load carrying capacity of the pile can be taken as given below:

Chainage	BH No.	Pile Dia (cms)	Length of Pile (m)	Safe Load carrying capacity of Pile (t)		
				Vertical	Uplift	Lateral
1+530	BH 2	100	27.0	300.0	150.0	10.0
		120	27.0	400.0	200.0	20.0
33+420	BH 13	100	31.0	280.0	150.0	5.0
		120	31.0	400.0	200.0	10.0
33+490	BH 14	100	30.0	300.0	150.0	10.0
		120	30.0	400.0	200.0	18.0
35+860	BH 15	100	28.0	300.0	150.0	10.0
		120	28.0	400.0	190.0	18.0
38+010	BH 16	100	24.0	70.0	60.0	10.0
		120	24.0	95.0	80.0	18.0
39+510	BH 17	100	28.0	110.0	70.0	9.0
			30.0	120.0	80.0	9.0
		120	28.0	150.0	90.0	15.0
			30.0	160.0	110.0	15.0
39+690	BH 18	100	29.0	210.0	150.0	15.0
		120	29.0	270.0	190.0	30.0
42+550	BH 20	100	29.0	300.0	160.0	10.0
		120	29.0	400.0	200.0	20.0

### MNB @ 21+810 & 29+280

Box foundation is recommended considering Bed protection work. The Depth of foundation below bed level , Size of foundation and the Net safe bearing pressure are as given below:

Chainage	BH	Depth of Foundation below Bed level (m)	Size of foundation (m)	Net Safe bearing pressure (t/m <sup>2</sup> )
21+810	BH 7	1.0	10.0 X 20.0	10.0
			12.0 X20.0	11.0
29+280	BH11	1.0	10.0 X 20.0	9.0
			12.0 X20.0	10.0

**For Soil Engineering Consultants**

**(A.V.S. RANGA RAO)**  
**Consultant**

Annexure I  
(Calculation)



**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile" as per IRC 78-2014**

Name of Project	<b>Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.</b>			Structure @ Chainage	0+000	Location	FLYOVER	Based on Bore Hole No	<b>BH 1</b>	Pile Cut -off level (m)	2.0	
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	2.70	water Level considered (m)	0.00	Scour Level @ RL(m)		
Pile Diameter (mm)	1000	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	Liquefaction depth below Ground level (m)	10.00	RL of the Borehole (m)		
Maximum effective overburden pressure= 20*Diameter of pile. Assuming the strata @ 30 m and below to be same.						Liquefaction depth below cut-off level(m) :						<b>8.000</b>

Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	r (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>sp</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance $P_{pu} = Ap * (cN_c + P_d N_q + 0.5 \gamma_r D N_{\gamma})$					Ultimate Shaft Friction $P_{su} = \sum (K_s P_{di} \tan \delta) + a.c.A_s$					Total Ultimate Capacity, $P_u = P_{pu} + P_{su}$ (tonnes)	Weight of pile, $W_p$ (Tonnes)	Total Safe Capacity, $P_s$ (Tonnes) $P_s = \frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5 <sub>r</sub> .D.N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer "P <sub>di</sub> " (t/m <sup>2</sup> )	A <sub>si</sub> (m <sup>2</sup> )	(K <sub>s</sub> P <sub>di</sub> Tan δ) A <sub>si</sub>	Adhesion Factor, a	a.c.A <sub>s</sub>						P <sub>su</sub>
1	SM-ML / SM	4	0.00	0	25	25	1.79	0.92	0	0	10	10.9	0.79	0	0	5.000	0	0	12.6	0	0	0	0	0	4.39	0	4.39	4
2	SM-ML / SM	4	0.00	0	25	25	1.74	0.88	0	0	10	10.9	0.79	0	0	4.780	0	0	12.6	0	0	0	0	0	8.78	0	8.78	8
3	SM-ML / SM	4.5	0.00	0	29	29	1.74	0.89	4	0	18.1	19.3	0.79	0	72.31	8.600	63.51	2	14.1	23.49	0	0	23.49	87	13.72	34.8	20.29	12.5
4	Cl	3	0.00	8	0	0	1.74	0.90	6.7	9	0	0	0.79	72	0	0.000	56.52	5.35	9.42	0	0.3	22.6	46.09	102.61	17.01	41.04	29.91	15.5
5	SM-ML / SM	2	0.00	0	29	29	1.74	0.89	8.48	0	18.1	19.3	0.79	0	153.29	8.600	127.08	7.59	6.28	39.63	0	0	85.72	212.8	19.2	85.12	43.2	17.5
6	SM-ML / SM	2	0.00	0	29	29	1.74	0.89	10.26	0	18.1	19.3	0.79	0	185.47	8.600	152.34	9.37	6.28	48.92	0	0	134.6	286.98	21.39	114.79	59.08	19.5
7	SM-ML / SM	3	0.00	0	29	29	1.74	0.89	12.93	0	18.1	19.3	0.79	0	233.74	8.600	190.23	11.59	9.42	90.77	0	0	225.4	415.64	24.68	166.25	87.79	22.5
8	SM-ML / SM	2	0.00	0	29	29	1.74	0.89	14.71	0	18.1	19.3	0.79	0	265.92	8.600	215.49	13.82	6.28	72.16	0	0	297.6	513.06	26.87	205.22	110.18	24.5
9	SM-ML / SM	2	0.00	0	30	30	1.74	0.89	16.49	0	20.9	22.4	0.79	0	345.44	9.960	278.98	15.6	6.28	84.84	0	0	382.4	661.39	29.06	264.55	136.13	26.5
10	SM-ML / SM	1	0.00	0	30	30	1.74	0.89	17.38	0	20.9	22.4	0.79	0	364.09	9.960	293	16.93	3.14	46.03	0	0	428.4	721.44	30.15	288.57	150.11	27.5
11	SM-ML / SM	1.5	0.00	0	30	30	1.74	0.89	17.38	0	20.9	22.4	0.79	0	364.09	9.960	293	17.38	4.71	70.89	0	0	499.3	792.33	31.79	316.93	171.6	29

**Recommendation :**

a) Pile Diameter (mm)	1000
b) Pile cut off level (m)	2.0
c) Pile Shaft Length from Cut off Level (m)	29.0
d) Vertical Pile Capacity ( tonnes)	300.0
e) Uplift pile capacity (Tonnes)	160.0

\* For vertical Capacity of Pile weight of the pile has not been considered.



**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile" as per IRC 78-2014**

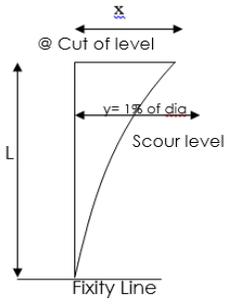
Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	0+000	Location	FLYOVER	Based on Bore Hole No	BH 1	Pile Cut -off level (m)	2.3	
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	2.70	water Level considered (m)	0.00	Scour Level @ RL(m)		
Pile Diameter (mm)	1200	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	Liquefaction depth below Ground level (m)	10.00	RL of the Borehole (m)		
Maximum effective overburden pressure= 20*Diameter of pile. Assuming the strata @ 30 m and below to be same.						Liquefaction depth below cut-off level(m) :						7.700

Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	r (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>sp</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance P <sub>pu</sub> = Ap* (cN <sub>c</sub> +P <sub>d</sub> N <sub>q</sub> +0.5γ <sub>v</sub> D.N <sub>γ</sub> )					Ultimate Shaft Friction P <sub>su</sub> = [Σ(K <sub>s</sub> P <sub>ai</sub> tanδ).A <sub>s</sub> +α.c.A <sub>s</sub> ]					Total Ultimate Capacity, P <sub>u</sub> =P <sub>pu</sub> + P <sub>su</sub> (tonnes)	Weight of pile, W <sub>p</sub> (Tonnes)	Total Safe Capacity, P <sub>s</sub> (Tonnes) P <sub>s</sub> = $\frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5γ <sub>v</sub> D.N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer P <sub>ai</sub> (t/m <sup>2</sup> )	A <sub>si</sub> (m <sup>2</sup> )	(K <sub>s</sub> P <sub>ai</sub> Tanδ).A <sub>si</sub>	Adhesion Factor, α	α.c.A <sub>s</sub>						P <sub>su</sub>
1	SM-ML / SM	3.7	0.00	0	25	25	1.79	0.92	0	0	10	10.9	1.13	0	0	6.000	0	0	13.9	0	0	0	0	0	5.85	0	5.85	3.7
2	SM-ML / SM	4	0.00	0	25	25	1.74	0.88	0	0	10	10.9	1.13	0	0	5.740	0	0	15.1	0	0	0	0	0	12.17	0	12.17	7.7
3	SM-ML / SM	4.5	0.00	0	29	29	1.74	0.89	4	0	18.1	19.3	1.13	0	72.31	10.320	93.37	2	17	28.18	0	0	28.18	121.55	19.28	48.62	27.17	12.2
4	Cl	3	0.00	8	0	0	1.74	0.90	6.7	9	0	0	1.13	72	0	0.000	81.36	5.35	11.3	0	0.3	27.12	55.3	136.66	24.02	54.66	39.5	15.2
5	SM-ML / SM	2	0.00	0	29	29	1.74	0.89	8.48	0	18.1	19.3	1.13	0	153.29	10.320	184.87	7.59	7.53	47.52	0	0	102.8	287.69	27.18	115.07	55.96	17.2
6	SM-ML / SM	2	0.00	0	29	29	1.74	0.89	10.26	0	18.1	19.3	1.13	0	185.47	10.320	221.24	9.37	7.53	58.66	0	0	161.5	382.72	30.34	153.08	75.55	19.2
7	SM-ML / SM	2.8	0.00	0	29	29	1.74	0.89	12.75	0	18.1	19.3	1.13	0	230.49	10.320	272.11	11.5	10.6	100.87	0	0	262.4	534.46	34.76	213.78	108.21	22
8	SM-ML / SM	2	0.00	0	29	29	1.74	0.89	14.53	0	18.1	19.3	1.13	0	262.67	10.320	308.47	13.64	7.53	85.39	0	0	347.7	656.21	37.92	262.48	135.28	24
9	SM-ML / SM	2	0.00	0	30	30	1.74	0.89	16.31	0	20.9	22.4	1.13	0	341.67	11.960	399.6	15.42	7.53	100.55	0	0	448.3	847.89	41.08	339.15	166.6	26
10	SM-ML / SM	1	0.00	0	30	30	1.74	0.89	17.2	0	20.9	22.4	1.13	0	360.32	11.960	420	16.75	3.76	54.54	0	0	502.8	922.83	42.66	369.13	183.45	27
11	SM-ML / SM	2	0.00	0	30	30	1.74	0.89	18.98	0	20.9	22.4	1.13	0	397.6	11.960	462	18.09	7.53	117.96	0	0	620.8	1082.79	45.82	433.11	219.64	29

**Recommendation :**

a) Pile Diameter (mm)	1200
b) Pile cut off level (m)	2.3
c) Pile Shaft Length from Cut off Level (m)	29.0
d) Vertical Pile Capacity ( tonnes)	400.0
e) Uplift pile capacity (Tonnes)	210.0

\* For vertical Capacity of Pile weight of the pile has not been considered.

Project no : 2152	Lateral Load Capacity of pile		
	[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :	Flyover @ 0+800		
Borehole no :	BH 1		
Type of pile :	Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :	1000	1200	
Cut off Level of the Pile in "m" :	2.000	2.300	
Length of the Pile below the cut off level in "m" :	29.0	29.0	
Type of Pile Head :	fixed	fixed	
Crossection of the Pile :	Circle	Circle	
Gade of the concrete (M):	35.0	35.0	
Type of Soil :	Granular	Granular	
Condition of Soil with w.r.t Ground water :	Submerged	Submerged	
No. of Blow (N)	15.00	15.00	
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m3 :	2.12E+03	2.12E+03	
Stiffness factor for Cohesionless soil (T) in m :	3.67	4.25	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	8.000	7.700	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	2.18	1.81	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	21.00	21.30	
Reading from the graph L <sub>F</sub> /T or L <sub>F</sub> /R [As per Appendix C, Clause 5.5.2 Fig 2]:	1.92	1.94	
Depth of Fixity L <sub>F</sub> in "m":	7.06	8.26	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>F</sub> ) in "m"	15.06	15.96	
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>			
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>	
Horizontal Deflection on the top of the pile (x) " in mm" :	22.1	22.8	
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :	11.25	20.25	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	10.00	18.00	
Equations :			
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$			
<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>			



**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile" as per IRC 78-2014**

Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	1+530	Location	MJB	Based on Bore Hole No	BH 2	Pile Cut-off level (m)	2.0
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	2.70	water Level considered (m)	0.00	Scour Level @ RL(m)	248.021
Pile Diameter (mm)	1000	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	6.42	Liquefaction depth below Ground level (m)	8.00	RL of the Borehole (m)	256.432
Maximum effective overburden pressure= 20*Diameter of pile. Assuming the strata @ 30 m and below to be same.							Scour level below cut-off level(m) :	6.420			

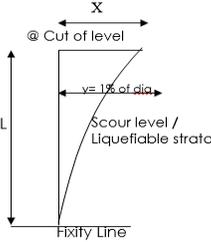
Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	γ (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance P <sub>pu</sub> = Ap* (cN <sub>c</sub> +P <sub>d</sub> N <sub>q</sub> +0.5γ <sub>v</sub> D <sub>v</sub> N <sub>γ</sub> )					Ultimate Shaft Friction P <sub>su</sub> = [Σ(K <sub>s</sub> P <sub>d</sub> Tanδ) <sub>s</sub> + a.c.A <sub>s</sub> ]					Total Ultimate Capacity, P <sub>u</sub> =P <sub>su</sub> + P <sub>pu</sub> (tonnes)	Weight of pile, W <sub>p</sub> (Tonnes)	Total Safe Capacity, P <sub>s</sub> (Tonnes)	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5γ <sub>v</sub> D <sub>v</sub> N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer P <sub>d</sub> ' (t/m <sup>2</sup> )	A <sub>s</sub> (m <sup>2</sup> )	[K <sub>s</sub> P <sub>d</sub> Tanδ) <sub>s</sub>	Adhesion Factor, a	a.c.A <sub>s</sub>						P <sub>su</sub>
1	SM-ML / SM	6.42	0.00	0	29	29	1.83	0.93	0	0	18.1	19.3	0.79	0	0	8.000	0	0	20.2	0	0	0	0	0	7.05	0	7.05	6.42
2	SM-ML / SM	4	0.00	0	30	30	1.86	0.95	3.8	0	20.9	22.4	0.79	0	79.6	10.640	70.83	1.9	12.6	20.66	0	0	20.66	91.49	11.44	36.59	17.22	10.42
3	SM-ML / SM	1.58	0.00	0	30	30	1.86	0.95	5.3	0	20.9	22.4	0.79	0	111.02	10.640	95.5	4.55	4.96	19.54	0	0	40.2	135.7	13.17	54.28	24.42	12
4	CL-CI	3	0.00	11	0	0	1.89	0.97	8.21	9	0	0	0.79	99	0	0.000	77.71	6.75	9.42	0	0.3	31.08	71.28	148.99	16.46	59.59	36.41	15
5	CL-CI	3.5	0.00	11	0	0	1.89	0.97	11.6	9	0	0	0.79	99	0	0.000	77.71	9.9	11	0	0.3	36.26	107.5	185.25	20.3	74.1	50.41	18.5
6	SM	1.5	0.00	0	30	30	1.89	0.97	13.05	0	20.9	22.4	0.79	0	273.38	10.860	223.12	12.32	4.71	50.25	0	0	157.8	380.91	21.94	152.36	66.12	20
7	SM	2.8	0.00	0	30	30	1.89	0.97	15.76	0	20.9	22.4	0.79	0	330.15	10.860	267.69	14.4	8.79	109.61	0	0	267.4	535.09	25.01	214.03	99.88	22.8
8	SM	2	0.00	0	30	30	1.89	0.97	17.7	0	20.9	22.4	0.79	0	370.79	10.860	299.59	16.73	6.28	90.98	0	0	358.4	657.97	27.2	263.18	127.54	24.8
9	SM	1.62	0.00	0	30	30	1.89	0.97	19.27	0	20.9	22.4	0.79	0	403.68	10.860	325.41	18.48	5.08	81.3	0	0	439.7	765.09	28.98	306.03	152.09	26.42
10	SM	0.58	0.00	0	30	30	1.89	0.97	19.27	0	20.9	22.4	0.79	0	403.68	10.860	325	19.27	1.82	30.37	0	0	470.1	795.05	29.61	318.02	161.22	27

**Recommendation :**

a) Pile Diameter (mm)	1000
b) Pile cut off level (m)	2.0
c) Pile Shaft Length from Cut off Level (m)	27.0
d) Vertical Pile Capacity ( tonnes)	300.0
e) Uplift pile capacity (Tonnes)	150.0

\* For vertical Capacity of Pile weight of the pile has not been considered.



Project no : 2152	Lateral Load Capacity of pile			
	[As per IS 2911-2010 Part 1Section-2] Annex-C			
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			
Structure @ Chainage :	MJB @ 1+530			
Borehole no :	BH 2			
Type of pile :	Bored cast in situ	Bored cast in situ		
Diameter of the pile in "mm" :	1000	1200		
Cut off Level of the Pile in "m" :	2.000	2.300		
Length of the Pile below the cut off level in "m" :	27.0	27.0		
Type of Pile Head :	fixed	fixed		
Crossection of the Pile :	Circle	Circle		
Gade of the concrete (M):	35.0	35.0		
Type of Soil :	Granular	Granular		
Condition of Soil with w.r.t Ground water :	Submerged	Submerged		
No. of Blow (N)	18.00	18.00		
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07		
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05		
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	2.55E+03	2.55E+03		
Stiffness factor for Cohesionless soil (T) in m :	3.54	4.09		
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	6.420	6.120		
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	1.81	1.50		
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	20.58	20.88		
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R (As per Appendix C, Clause 5.5.2 Fig 2):	1.94	1.96		
Depth of Fixity L <sub>f</sub> in "m":	6.88	8.02		
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	13.30	14.14		
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile		
<b>Considering 1% of dia for Horizontal Deflection :</b>				
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>		
Horizontal Deflection on the top of the pile (x) " in mm" :	19.0	20.0		
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :	14.07	25.54		
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	<b>10.00</b>	<b>20.00</b>		
Equations :				
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$				
<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>				

**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile"as per IRC 78-2014**



Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	6+380	Location	VUP	Based on Bore Hole No	BH 3	Pile Cut-off level (m)	2.0
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	13.80	water Level considered (m)	0.00	Scour Level @ RL(m)	
Pile Diameter (mm)	1000	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	liquefaction depth below Ground level (m)	0.00	RL of the Borehole (m)	
Maximum effective overburden pressure= 20*Diameter of pile. Assuming the strata @ 20 m and below to be same.						Scour level below cut-off level(m) :	<b>0.000</b>				

Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion ,C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	γ (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance $P_{pu} = Ap * (cN_c + P_d N_q + 0.5 \gamma_r D N_{\gamma})$					Ultimate Shaft Friction $P_{su} = (\sum (K_s P_{dl} \tan \delta) A_{s1} + a.c.A_s)$					Total Ultimate Capacity, $P_u = P_{pu} + P_{su}$ (tonnes)	Weight of pile, $W_p$ (Tonnes)	Total Safe Capacity, $P_s$ (Tonnes) $P_s = \frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5 <sub>γ<sub>r</sub></sub> D.N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer 'P <sub>dl</sub> ' (t/m <sup>2</sup> )	A <sub>s1</sub> (m <sup>2</sup> )	(K <sub>s</sub> P <sub>dl</sub> Tanδ).A <sub>s1</sub>	Adhesion Factor, a	a.c.A <sub>s1</sub>						P <sub>su</sub>
1	SM-ML	4	0.00	0	29	29	1.82	0.98	3.92	0	18.1	19.3	0.79	0	70.86	9.000	62.69	1.96	12.6	20.46	0	0	0	62.69	4.39	25.07	4.39	4
2	SM	4	0.00	0	30	30	1.85	1.03	8.04	0	20.9	22.4	0.79	0	168.42	11.530	141.26	5.98	12.6	65.04	0	0	65.04	206.3	8.78	82.52	26.99	8
3	SM	4	0.00	0	30	30	1.85	1.03	12.16	0	20.9	22.4	0.79	0	254.73	11.530	209.01	10.1	12.6	109.86	0	0	174.9	383.91	13.17	153.56	62.14	12
4	SM	3	0.00	0	30	30	1.87	1.03	15.25	0	20.9	22.4	0.79	0	319.47	11.530	259.83	13.7	9.42	111.76	0	0	286.7	546.49	16.46	218.59	96.72	15
5	SM	2	0.00	0	30	30	1.87	1.03	17.31	0	20.9	22.4	0.79	0	362.62	11.530	293.7	16.28	6.28	88.54	0	0	375.2	668.9	18.65	267.56	123.7	17
6	SM	1	0.00	0	30	30	1.87	1.03	18.34	0	20.9	22.4	0.79	0	384.2	11.530	310.64	17.82	3.14	48.45	0	0	423.7	734.29	19.74	293.71	138.36	18
7	SM	1	0.00	0	30	30	1.87	1.03	19.37	0	20.9	22.4	0.79	0	405.77	11.530	327.58	18.85	3.14	51.25	0	0	474.9	802.48	20.83	320.99	153.8	19

**Recommendation :**

- a) Pile Diameter (mm)  
b) Pile cut off level (m)  
c) Pile Shaft Length from Cut off Level (m)  
d) Vertical Pile Capacity ( tonnes)  
e) Uplift pile capacity (Tonnes)

1000	
2.0	
18.0	19.0
280.0	300.0
120.0	140.0

\* For vertical Capacity of Pile weight of the pile has not been considered.

**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile"as per IRC 78-2014**



Name of Project	<b>Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.</b>			Structure @ Chainage	6+380	Location	VUP	Based on Bore Hole No	<b>BH 3</b>	Pile Cut-off level (m)	2.3
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	13.80	water Level considered (m)	0.00	Scour Level @ RL(m)	
Pile Diameter (mm)	1200	Earth Presure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	liquefaction depth below Ground level (m)	0.00	RL of the Borehole (m)	
Maximum effective overburden pressure= 20*Diameter of pile. Assuming the strata @ 20 m and below to be same.						Scour level below cut-off level(m) :		<b>0.000</b>			

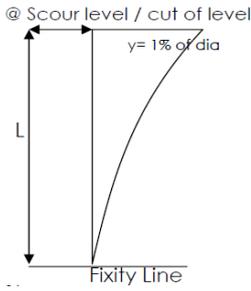
Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion ,C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	γ (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance $P_{pu} = Ap^* (cN_c + P_d N_q + 0.5 \gamma_v D N_{\gamma})$					Ultimate Shaft Friction $P_{su} = (\sum (K_s P_{d1} \tan \delta) A_{s1} + a.c.A_s)$					Total Ultimate Capacity, $P_u = P_{su} + P_{pu}$ (tonnes)	Weight of pile, $W_p$ (Tonnes)	Total Safe Capacity, $P_s$ (Tonnes) $P_s = \frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										$N_c$	$N_q$	$N_{\gamma}$	$A_p$ (m <sup>2</sup> )	$c.N_c$	$P_d N_q$	$0.5 \gamma_v D N_{\gamma}$	$P_{pu}$ (tonnes)	Effective overburden Pressure at c.g of the layer 'P <sub>d1</sub> ' (t/m <sup>2</sup> )	$A_{s1}$ (m <sup>2</sup> )	$(K_s P_{d1} \tan \delta) A_{s1}$	Adhesion Factor, a	a.c.A <sub>s</sub>						$P_{su}$
1	SM-ML	3.7	0.00	0	29	29	1.82	0.98	3.62	0	18.1	19.3	1.13	0	65.44	11.000	86.37	1.81	13.9	20.97	0	0	0	86.37	5.85	34.54	5.85	3.7
2	SM	4	0.00	0	30	30	1.85	1.03	7.74	0	20.9	22.4	1.13	0	162.14	13.840	198.85	5.68	15.1	74.12	0	0	74.12	272.97	12.17	109.18	32.92	7.7
3	SM	4	0.00	0	30	30	1.85	1.03	11.86	0	20.9	22.4	1.13	0	248.45	13.840	296.38	9.8	15.1	127.89	0	0	202	498.39	18.49	199.35	75.05	11.7
4	SM	3	0.00	0	30	30	1.87	1.03	14.95	0	20.9	22.4	1.13	0	313.18	13.840	369.53	13.4	11.3	131.13	0	0	333.1	702.67	23.23	281.06	116.5	14.7
5	SM	2.3	0.00	0	30	30	1.87	1.03	17.31	0	20.9	22.4	1.13	0	362.62	13.840	425.39	16.13	8.66	120.97	0	0	454.1	879.5	26.86	351.8	154.01	17
6	SM	1	0.00	0	30	30	1.87	1.03	18.34	0	20.9	22.4	1.13	0	384.2	13.840	449.78	17.82	3.76	58.02	0	0	512.1	961.91	28.44	384.76	171.83	18
7	SM	1	0.00	0	30	30	1.87	1.03	19.37	0	20.9	22.4	1.13	0	405.77	13.840	474.15	18.85	3.76	61.38	0	0	573.5	1047.66	30.02	419.06	190.6	19

**Recommendation :**

- a) Pile Diameter (mm)  
b) Pile cut off level (m)  
c) Pile Shaft Length from Cut off Level (m)  
d) Vertical Pile Capacity ( tonnes)  
e) Uplift pile capacity (Tonnes)

1200	
2.3	
18.0	19.0
370.0	400.0
160.0	170.0

\* For vertical Capacity of Pile weight of the pile has not been considered.

Project no : 2152	Lateral Load Capacity of pile		
	[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :	VUP @ 6+380		
Borehole no :	BH 3		
Type of pile :	Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :	1000	1200	
Cut off Level of the Pile in "m" :	2.000	2.300	
Length of the Pile below the cut off level in "m" :	18.0	18.0	
Type of Pile Head :	fixed	fixed	
Crossection of the Pile :	Circle	Circle	
Gade of the concrete (M):	35.0	35.0	
Type of Soil :	Granular	Granular	
Condition of Soil with w.r.t Ground water :	Submerged	Submerged	
No. of Blow (N)	14.00	14.00	
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	1.97E+03	1.97E+03	
Stiffness factor for Cohesionless soil (T) in m :	3.73	4.31	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	0.000	0.000	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	0.00	0.00	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	18.00	18.00	
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R [As per Appendix C, Clause 5.5.2 Fig 2]:	2.19	2.19	
Depth of Fixidity L <sub>f</sub> in "m":	8.17	9.44	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	8.17	9.44	
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>			
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>	
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :	31.96	51.55	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	<b>20.00</b>	<b>40.00</b>	
Equations :			
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$			
For Free Head (Y) = [QLxx <sup>3</sup> ]/3EI ; For Fixed head (Y)=[QLxx <sup>3</sup> ]/12EI			



**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile"as per IRC 78-2014**

Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	8+020	Location	FLYOVER	Based on Bore Hole No	BH 5	Pile Cut -off level (m)	2.0	
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	14.10	water Level considered (m)	0.00	Scour Level @ RL(m)		
Pile Diameter (mm)	1000	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	Liquefaction depth below Ground level (m)	0.00	RL of the Borehole (m)		
Maximum effective overburden pressure= 20*Diameter of pile. Assuming the strata @ 30 m and below to be same.							Scour level below cut-off level(m) :	0.000				

Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	r (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance $P_{pu} = Ap * (cN_c + P_d N_q + 0.5 \gamma_v D N_{\gamma})$					Ultimate Shaft Friction $P_{su} = (\sum (K_s P_{dl} \tan \delta)) A_s + a.c.A_s$					Total Ultimate Capacity, $P_u = P_{pu} + P_{su}$ (tonnes)	Weight of pile, $W_p$ (Tonnes)	Total Safe Capacity, $P_s$ $P_s = \frac{P_u}{2.5}$ (Tonnes)	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5 <sub>v</sub> .D.N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer P <sub>dl</sub> (t/m <sup>2</sup> )	A <sub>s</sub> (m <sup>2</sup> )	(K <sub>s</sub> P <sub>dl</sub> tanδ).A <sub>s</sub>	Adhesion Factor, a	a.c.A <sub>s</sub>						P <sub>su</sub>
1	SM-ML / SM	4	0.00	0	29	29	1.8	1.00	4	0	18.1	19.3	0.79	0	72.31	9.000	63.82	2	12.6	20.88	0	0	0	63.82	4.39	25.52	4.39	4
2	SM-ML / SM	4	0.00	0	30	30	1.8	1.01	8.04	0	20.9	22.4	0.79	0	168.42	11.310	141.08	6.02	12.6	65.48	0	0	65.48	206.56	8.78	82.62	27.11	8
3	Cl	2	0.00	14	0	0	1.83	1.05	10.14	9	0	0	0.79	126	0	0.000	98.91	9.09	6.28	0	0.3	26.37	91.85	190.76	10.97	76.3	36.68	10
4	SM-ML / SM	3	0.00	0	30	30	1.9	1.00	13.14	0	20.9	22.4	0.79	0	275.26	11.200	224.87	11.64	9.42	94.95	0	0	186.8	411.67	14.26	164.66	66.56	13
5	SM-ML / SM	2	0.00	0	30	30	1.9	1.00	15.14	0	20.9	22.4	0.79	0	317.16	11.200	257.76	14.14	6.28	76.9	0	0	263.7	521.46	16.45	208.58	90.28	15
6	SM-ML / SM	2	0.00	0	30	30	1.9	1.00	17.14	0	20.9	22.4	0.79	0	359.06	11.200	290.65	16.14	6.28	87.77	0	0	351.5	642.12	18.64	256.84	117.05	17
7	SM-ML / SM	1	0.00	0	30	30	1.9	1.00	18.14	0	20.9	22.4	0.79	0	380.01	11.200	307.09	17.64	3.14	47.96	0	0	399.4	706.52	19.73	282.6	131.57	18
8	SM-ML / SM	2	0.00	0	30	30	1.9	1.00	20.14	0	20.9	22.4	0.79	0	421.91	11.200	339.99	19.14	6.28	104.09	0	0	503.5	843.51	21.92	337.4	162.9	20

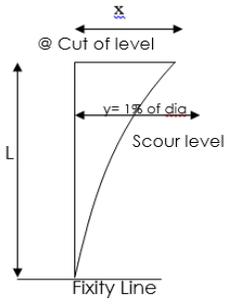
**Recommendation :**

- a) Pile Diameter (mm)
- b) Pile cut off level (m)
- c) Pile Shaft Length from Cut off Level (m)
- d) Vertical Pile Capacity ( tonnes)
- e) Uplift pile capacity (Tonnes)

1000
2.0
20.0
330.0
150.0

\* For vertical Capacity of Pile weight of the pile has not been considered.



Project no : 2152	Lateral Load Capacity of pile		
	[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :	Flyover @ 8+020		
Borehole no :	BH 5		
Type of pile :	Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :	1000	1200	
Cut off Level of the Pile in "m" :	2.000	2.300	
Length of the Pile below the cut off level in "m" :	20.0	20.0	
Type of Pile Head :	fixed	fixed	
Crossection of the Pile :	Circle	Circle	
Gade of the concrete (M):	35.0	35.0	
Type of Soil :	Granular	Granular	
Condition of Soil with w.r.t Ground water :	Submerged	Submerged	
No. of Blow (N)	12.00	12.00	
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m3 :	1.68E+03	1.68E+03	
Stiffness factor for Cohesionless soil (T) in m :	3.85	4.45	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	0.000	0.000	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	0.00	0.00	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	20.00	20.00	
Reading from the graph L <sub>F</sub> /T or L <sub>F</sub> /R [As per Appendix C, Clause 5.5.2 Fig 2]:	2.19	2.19	
Depth of Fixity L <sub>F</sub> in "m":	8.43	9.75	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>F</sub> ) in "m"	8.43	9.75	
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>			
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>	
Horizontal Deflection on the top of the pile (x) " in mm" :	10.0	12.0	
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :	29.06	46.84	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	<b>25.00</b>	<b>40.00</b>	
Equations :			
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$			
<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>			



**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile"as per IRC 78-2014**

Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	16+690	Location	VUP	Based on Bore Hole No	BH 6	Pile Cut -off level (m)	2.0
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	13.80	water Level considered (m)	0.00	Scour Level @ RL(m)	
Pile Diameter (mm)	1000	Earth Presure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	liquefaction depth below Ground level (m)	0.00	RL of the Borehole (m)	
<p>Maximum effective overburden pressure= 20*Diameter of pile.          Assuming the strata @ 20 m and below to be same.</p> <p align="center"><b>Scour level below cut-off level(m) :</b></p> <p align="center"><b>0.000</b></p>											

Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion , C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	γ (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance P <sub>pu</sub> = Ap* (cN <sub>c</sub> +P <sub>d</sub> N <sub>q</sub> +0.5.γ <sub>v</sub> .D.N <sub>γ</sub> )					Ultimate Shaft Friction P <sub>su</sub> = (Σ(K <sub>s</sub> P <sub>d</sub> tanδ).A <sub>si</sub> +a.c.A <sub>s</sub> )					Total Ultimate Capacity, P <sub>u</sub> =P <sub>pu</sub> + P <sub>su</sub> (tonnes)	Weight of pile, W <sub>p</sub> (Tonnes)	Total Safe Capacity, P <sub>s</sub> (Tonnes) P <sub>s</sub> = $\frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5.γ <sub>v</sub> .D.N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer 'P <sub>d</sub> ' (t/m <sup>2</sup> )	A <sub>si</sub> (m <sup>2</sup> )	(K <sub>s</sub> P <sub>d</sub> tanδ).A <sub>si</sub>	Adhesion Factor, a	a.c.A <sub>s</sub>						P <sub>su</sub>
1	Cl	2	0.00	6	0	0	1.84	1.03	2.06	9	0	0	0.79	54	0	0.000	42.39	1.03	6.28	0	0.3	11.3	0	42.39	2.19	16.95	2.19	2
2	SM-ML	2	0.00	0	30	30	1.86	0.99	4.04	0	20.9	22.4	0.79	0	84.63	11.080	75.13	3.05	6.28	16.58	0	0	16.58	91.71	4.38	36.68	9.02	4
3	SM	4	0.00	0	30	30	1.8	0.99	8	0	20.9	22.4	0.79	0	167.59	11.080	140.25	6.02	12.6	65.48	0	0	82.06	222.31	8.77	88.92	31.74	8
4	Cl	2	0.00	13	0	0	1.87	0.99	9.98	9	0	0	0.79	117	0	0.000	91.84	8.99	6.28	0	0.3	24.49	106.6	198.39	10.96	79.35	40.79	10
5	Cl	2	0.00	13	0	0	1.87	0.99	11.96	9	0	0	0.79	117	0	0.000	91.84	10.97	6.28	0	0.3	24.49	131	222.88	13.15	89.15	49.84	12
6	SM	2	0.00	0	30	30	1.87	0.99	13.94	0	20.9	22.4	0.79	0	292.02	11.080	237.93	12.95	6.28	70.43	0	0	201.5	439.4	15.34	175.76	71.75	14
7	SM	2	0.00	0	30	30	1.87	0.99	15.92	0	20.9	22.4	0.79	0	333.5	11.080	270.49	14.93	6.28	81.19	0	0	282.7	553.15	17.53	221.26	96.67	16
8	SM	2	0.00	0	30	30	1.87	0.99	17.9	0	20.9	22.4	0.79	0	374.98	11.080	303.05	16.91	6.28	91.96	0	0	374.6	677.67	19.72	271.06	124.61	18
9	SM	2	0.00	0	30	30	1.87	0.99	19.88	0	20.9	22.4	0.79	0	416.46	11.080	335.61	18.89	6.28	102.73	0	0	477.4	812.96	21.91	325.18	155.56	20

**Recommendation :**

- a) Pile Diameter (mm)
- b) Pile cut off level (m)
- c) Pile Shaft Length from Cut off Level (m)
- d) Vertical Pile Capacity ( tonnes)
- e) Uplift pile capacity (Tonnes)

1000	
2.0	
18.0	20.0
250.0	300.0
110.0	140.0

\* For vertical Capacity of Pile weight of the pile has not been considered.



**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile"as per IRC 78-2014**

Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	16+690	Location	VUP	Based on Bore Hole No	BH 6	Pile Cut -off level (m)	2.3
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resitance	2.5	Actual Water table (m)	13.80	water Level considered (m)	0.00	Scour Level @ RL(m)	
Pile Diameter (mm)	1200	Earth Presure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	liquefaction depth below Ground level (m)	0.00	RL of the Borehole (m)	
<p>Maximum effective overburden pressure= 20*Diameter of pile.          Assuming the strata @ 20 m and below to be same.</p> <p align="right"><b>Scour level below cut-off level(m) :</b> <span style="border: 1px solid black; padding: 2px;">0.000</span></p>											

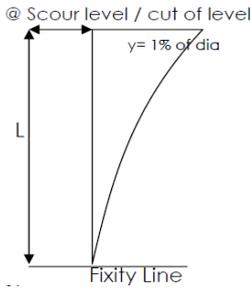
Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion . C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	r (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance P <sub>pu</sub> = Ap* (cN <sub>c</sub> +P <sub>d</sub> N <sub>q</sub> +0.5γ <sub>v</sub> .D.N <sub>γ</sub> )					Ultimate Shaft Friction P <sub>su</sub> = (Σ(K <sub>s</sub> P <sub>d</sub> tanδ).A <sub>si</sub> +a.c.A <sub>s</sub> )					Total Ultimate Capacity, P <sub>u</sub> =P <sub>pu</sub> + P <sub>su</sub> (tonnes)	Weight of pile, W <sub>p</sub> (Tonnes)	Total Safe Capacity, P <sub>s</sub> (Tonnes) P <sub>s</sub> = $\frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5γ <sub>v</sub> .D.N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer 'P <sub>d</sub> ' (t/m <sup>2</sup> )	A <sub>si</sub> (m <sup>2</sup> )	(K <sub>s</sub> P <sub>d</sub> tanδ).A <sub>si</sub>	Adhesion Factor, a	a.c.A <sub>s</sub>						P <sub>su</sub>
1	Cl	1.7	0.00	6	0	0	1.84	1.03	1.75	9	0	0	1.13	54	0	0.000	61.02	0.87	6.4	0	0.3	11.52	0	61.02	2.68	24.4	2.68	1.7
2	SM-ML	2	0.00	0	30	30	1.86	0.99	3.73	0	20.9	22.4	1.13	0	78.13	13.300	103.31	2.74	7.53	17.86	0	0	17.86	121.17	5.84	48.46	10.84	3.7
3	SM	4	0.00	0	30	30	1.8	0.99	7.69	0	20.9	22.4	1.13	0	161.09	13.300	197.06	5.71	15.1	74.52	0	0	92.38	289.44	12.16	115.77	38.02	7.7
4	Cl	2	0.00	13	0	0	1.87	0.99	9.67	9	0	0	1.13	117	0	0.000	132.21	8.68	7.53	0	0.3	29.36	121.7	253.95	15.32	101.58	49.4	9.7
5	Cl	2	0.00	13	0	0	1.87	0.99	11.65	9	0	0	1.13	117	0	0.000	132.21	10.66	7.53	0	0.3	29.36	151.1	283.31	18.48	113.32	60.78	11.7
6	SM	2.3	0.00	0	30	30	1.87	0.99	13.92	0	20.9	22.4	1.13	0	291.6	13.300	344.53	12.78	8.66	95.84	0	0	246.9	591.47	22.11	236.58	91.25	14
7	SM	2	0.00	0	30	30	1.87	0.99	15.9	0	20.9	22.4	1.13	0	333.08	13.300	391.4	14.91	7.53	97.23	0	0	344.2	735.57	25.27	294.22	121.63	16
8	SM	2	0.00	0	30	30	1.87	0.99	17.88	0	20.9	22.4	1.13	0	374.56	13.300	438.28	16.89	7.53	110.14	0	0	454.3	892.59	28.43	357.03	155.63	18
9	SM	2	0.00	0	30	30	1.87	0.99	19.86	0	20.9	22.4	1.13	0	416.04	13.300	485.15	18.87	7.53	123.05	0	0	577.4	1062.51	31.59	425	193.25	20

**Recommendation :**

- a) Pile Diameter (mm)  
b) Pile cut off level (m)  
c) Pile Shaft Length from Cut off Level (m)  
d) Vertical Pile Capacity ( tonnes)  
e) Uplift pile capacity (Tonnes)

1200	
2.3	
18.0	20.0
340.0	400.0
140.0	180.0

\* For vertical Capacity of Pile weight of the pile has not been considered.

Project no : 2152	Lateral Load Capacity of pile			
	[As per IS 2911-2010 Part 1Section-2] Annex-C			
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			
Structure @ Chainage :	VUP @ 16+690			
Borehole no :	BH 6			
Type of pile :	Bored cast in situ	Bored cast in situ		
Diameter of the pile in "mm" :	1000	1200		
Cut off Level of the Pile in "m" :	2.000	2.300		
Length of the Pile below the cut off level in "m" :	18.0	18.0		
Type of Pile Head :	fixed	fixed		
Crossection of the Pile :	Circle	Circle		
Gade of the concrete (M):	35.0	35.0		
Type of Soil :	Granular	Granular		
Condition of Soil with w.r.t Ground water :	Submerged	Submerged		
No. of Blow (N)	15.00	15.00		
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07		
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05		
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	2.12E+03	2.12E+03		
Stiffness factor for Cohesionless soil (T) in m :	3.67	4.25		
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	0.000	0.000		
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	0.00	0.00		
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	18.00	18.00		
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R [As per Appendix C, Clause 5.5.2 Fig 2]:	2.19	2.19		
Depth of Fixidity L <sub>f</sub> in "m":	8.04	9.31		
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	8.04	9.31		
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile		
<b>Considering 1% of dia for Horizontal Deflection :</b>				
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>		
Lateral capcity of pile ,Q (Tonnes) for 1% dia. deflection :	33.56	53.77		
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	<b>20.00</b>	<b>40.00</b>		
Equations :				
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$				
For Free Head (Y) = [QLxx <sup>3</sup> ]/3EI ; For Fixed head (Y)=[QLxx <sup>3</sup> ]/12EI				

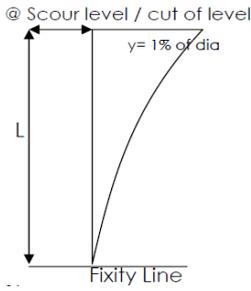
Project no: 2152	BEARING CAPACITY ANALYSIS FOR SHALLOW FOUNDATIONS		
	as per IS: 6403-1981		
Structure @ Chainage :	MNB @ 21+810	MNB @ 21+810	
Borehole no:	BH 7	BH 7	
Type of Foundation :	<b>Raft</b>	<b>Raft</b>	
Depth of Foundation below Bed level (D <sub>f</sub> ) :	<b>1.000</b>	<b>1.000</b>	
Width of the foundation (B) in "m":	<b>10.000</b>	<b>12.000</b>	
Length of the foundation (L) in "m" :	<b>20.000</b>	<b>20.000</b>	
Angle of Internal Friction ,Φ :	29	29	
Cohension , C (T/m <sup>2</sup> ) :	0	0	
Density of soil (γ) T/m <sup>3</sup> :	1.87	1.87	
Effective unit weight (γ') T/m <sup>3</sup> :	0.87	0.87	
Depth of water table (W.T) m from G.L :	11.3	11.3	
Design water table depth (W.T')m :	0	0	
Angle of Inclination factor :	0	0	
Depth factors (assumed that backfilling is not compacted properly)	1.00	1.00	
Surcharge at sub-base foundation level q= γ*D <sub>f</sub>	0.3	0.3	
Shape factors :	S <sub>c</sub>	1.1	1.12
	S <sub>q</sub>	1.1	1.12
	S <sub>γ</sub>	0.8	0.76
Inclination factors :	i <sub>c</sub>	1.00	1.00
	i <sub>q</sub>	1.00	1.00
	i <sub>γ</sub>	1.00	1.00
Depth factors :	dc = 1+0.2(D <sub>f</sub> /B)√(NΦ)	1.00	1.00
	dq = 1+0.1*(D <sub>f</sub> /B)√(NΦ) for >10°	1.00	1.00
	dγ = 1+0.1*(D <sub>f</sub> /B)√(NΦ) for >10°	1.00	1.00
<b>Shear failure criteria</b>			
Bearing capacity factor's for General Shear :	Φ	29	29
	N <sub>c</sub> = (Nq-1)/tanθ	27.83	27.83
	N <sub>q</sub> = Nγ/(2*tanθ)-1	16.43	16.43
	N <sub>γ</sub> = 2{[(exp(πtanθ))] tan <sup>2</sup> (45+θ/2)+1}tanθ	19.33	19.33
Bearing capacity factor's for Local Shear :	Φ'	20	20
	N' <sub>c</sub>	15.15	15.15
	N' <sub>q</sub>	6.63	6.63
	N' <sub>γ</sub>	5.67	5.67
Correction factor for W.T (W')	0.50	0.50	
Factor of safety	2.50	2.50	
General shear Net safe bearing pressure (T/m <sup>2</sup> ) : C*NC*Sc*ic*dc+q(Nq-1)*sq*iq*dq+0.50*B*γ*Nγ*sγ*iy*dγ*W'	26.78	30.28	
Local shear safe bearing pressure (T/m <sup>2</sup> ) : C*NC*Sc*ic*dc+q(Nq-1)*sq*iq*dq+0.50*B*γ*Nγ*sγ*iy*dγ*W'	8.00	9.03	
On interpolation Safe Bearing pressure (T/m <sup>2</sup> )	10.35	11.69	
* Considering bed protection work			


**Settlement criteria as per IS 8009(Part I),fig 12 :**

Structure @ Chainage :	MNB @ 21+810	MNB @ 21+810
Borehole no:	<b>BH 7</b>	<b>BH 7</b>
Depth of Foundation below Bed level (DF) :	<b>1.00</b>	<b>1.00</b>
Width of the foundation (B) in "m":	<b>10.00</b>	<b>12.00</b>
Corrected SPT (N) value =	<b>16</b>	<b>16</b>
settlement under footing with a load of 10 T/m <sup>2</sup> in dry cohesionless soil :	21	21
Settlement under footing with a load intensity of 10 T/m <sup>2</sup> after water table correction :	42	42
Settlement under footing with load intensity of 10 T/m <sup>2</sup> after Depth correction and rigidity correction	34	34
Net safe bearing pressure for 75 mm of settlements :	22	22





Project no : 2152	Lateral Load Capacity of pile			
	[As per IS 2911-2010 Part 1Section-2] Annex-C			
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			
Structure @ Chainage :	VUP @ 22+980			
Borehole no :	BH 8			
Type of pile :	Bored cast in situ	Bored cast in situ		
Diameter of the pile in "mm" :	1000	1200		
Cut off Level of the Pile in "m" :	2.000	2.300		
Length of the Pile below the cut off level in "m" :	18.0	18.0		
Type of Pile Head :	fixed	fixed		
Cross-section of the Pile :	Circle	Circle		
Grade of the concrete (M):	35.0	35.0		
Type of Soil :	Granular	Granular		
Condition of Soil with w.r.t Ground water :	Submerged	Submerged		
No. of Blow (N)	20.00	20.00		
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07		
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05		
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	2.84E+03	2.84E+03		
Stiffness factor for Cohesionless soil (T) in m :	3.46	4.01		
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	0.000	0.000		
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	0.00	0.00		
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	18.00	18.00		
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R [As per Appendix C, Clause 5.5.2 Fig 2]:	2.19	2.19		
Depth of Fixidity L <sub>f</sub> in "m":	7.58	8.78		
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	7.58	8.78		
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile		
<b>Considering 1% of dia for Horizontal Deflection :</b>				
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>		
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :	40.04	64.01		
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	<b>35.00</b>	<b>50.00</b>		
Equations :				
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$				
For Free Head (Y) = [QLxx <sup>3</sup> ]/3EI ; For Fixed head (Y)=[QLxx <sup>3</sup> ]/12EI				

**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile" as per IRC 78-2014**



Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	25+430	Location	VUP	Based on Bore Hole No	BH 9	Pile Cut-off level (m)	2.0
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	12.25	water Level considered (m)	0.00	Scour Level @ RL(m)	
Pile Diameter (mm)	1000	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	liquefaction depth below Ground level (m)	0.00	RL of the Borehole (m)	
Maximum effective overburden pressure= 20*Diameter of pile. Assuming the strata @ 20 m and below to be same.						Scour level below cut-off level(m) :	0.000				

Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	r (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance $P_{pu} = Ap * (cN_c + P_d N_q + 0.5 \gamma_r D N_{\gamma})$					Ultimate Shaft Friction $P_{su} = (\sum [K_s P_{di} \tan \delta] A_s) + a.c.A_s$					Total Ultimate Capacity, $P_u = P_{pu} + P_{su}$ (tonnes)	Weight of pile, $W_p$ (Tonnes)	Total Safe Capacity, $P_s$ (Tonnes) $P_s = \frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5.γ <sub>r</sub> .D.N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer "P <sub>di</sub> " (t/m <sup>2</sup> )	A <sub>si</sub> (m <sup>2</sup> )	(K <sub>s</sub> P <sub>di</sub> tan δ).A <sub>si</sub>	Adhesion Factor, a	a.c.A <sub>s</sub>						P <sub>su</sub>
1	Cl	3	0.00	5	0	0	1.82	1.01	3.03	9	0	0	0.79	45	0	0.000	35.32	1.51	9.42	0	0.3	14.13	0	35.32	3.29	14.12	3.29	3
2	SM-ML	2	0.00	0	30	30	1.84	0.99	5.01	0	20.9	22.4	0.79	0	104.95	11.080	73.8	4.02	6.28	21.86	0	0	21.86	95.66	5.48	38.26	11.6	5
3	SM-ML	3	0.00	0	30	30	1.84	0.99	7.98	0	20.9	22.4	0.79	0	167.17	11.080	73.58	6.49	9.42	52.94	0	0	74.8	148.38	8.77	59.35	29.71	8
4	SM-ML	2	0.00	0	30	30	1.82	0.95	9.88	0	20.9	22.4	0.79	0	206.97	10.640	57	8.93	6.28	48.56	0	0	123.4	180.36	10.96	72.14	45.5	10
5	CL	2.5	0.00	8	0	0	1.82	0.97	12.3	9	0	0	0.79	72	0	0.000	56.52	11.09	7.85	0	0.3	18.84	142.2	198.72	13.7	79.48	53.51	12.5
6	SM	2.5	0.00	0	30	30	1.82	0.95	14.67	0	20.9	22.4	0.79	0	307.32	10.640	249.59	13.48	7.85	91.64	0	0	233.8	483.43	16.44	193.37	81.91	15
7	SM	3	0.00	0	30	30	1.82	0.95	17.52	0	20.9	22.4	0.79	0	367.02	10.640	296.46	16.09	9.42	131.26	0	0	365.1	661.56	19.73	264.62	121.95	18
8	SM	1	0.00	0	30	30	1.82	0.95	18.47	0	20.9	22.4	0.79	0	386.92	10.640	312.08	17.99	3.14	48.92	0	0	414	726.1	20.82	290.44	136.74	19

**Recommendation :**

- a) Pile Diameter (mm)  
b) Pile cut off level (m)  
c) Pile Shaft Length from Cut off Level (m)  
d) Vertical Pile Capacity (tonnes)  
e) Uplift pile capacity (Tonnes)

3000	
2.0	
18.0	19.0
250.0	270.0
110.0	120.0

\* For vertical Capacity of Pile weight of the pile has not been considered.

**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile" as per IRC 78-2014**



Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	25+430	Location	VUP	Based on Bore Hole No	BH 9	Pile Cut-off level (m)	2.3	
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	12.25	water Level considered (m)	0.00	Scour Level @ RL(m)		
Pile Diameter (mm)	1200	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	liquefaction depth below Ground level (m)	0.00	RL of the Borehole (m)		
Maximum effective overburden pressure= 20*Diameter of pile. Assuming the strata @ 20 m and below to be same.							Scour level below cut-off level(m) :	0.000				

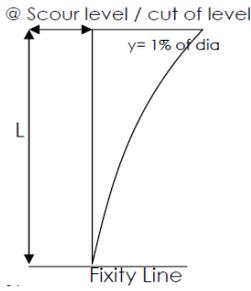
Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	r (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance $P_{pu} = Ap * (cN_c + P_d N_q + 0.5 \gamma_r D N_{\gamma})$					Ultimate Shaft Friction $P_{su} = (\sum (K_s P_{di} \tan \delta) A_{si} + a.c.A_s)$					Total Ultimate Capacity, $P_u = P_{pu} + P_{su}$ (tonnes)	Weight of pile, $W_p$ (Tonnes)	Total Safe Capacity, $P_s$ (Tonnes) $P_s = \frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5.γ <sub>r</sub> .D.N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer "P <sub>di</sub> " (t/m <sup>2</sup> )	A <sub>si</sub> (m <sup>2</sup> )	(K <sub>s</sub> P <sub>di</sub> tan δ). A <sub>si</sub>	Adhesion Factor, a	a.c.A <sub>s</sub>						P <sub>su</sub>
1	CI	2.7	0.00	5	0	0	1.82	1.01	2.72	9	0	0	1.13	45	0	0.000	50.85	1.36	10.2	0	0.3	15.25	0	50.85	4.27	20.34	4.27	2.7
2	SM-ML	2	0.00	0	30	30	1.84	0.99	4.7	0	20.9	22.4	1.13	0	98.45	13.300	100.07	3.71	7.53	24.19	0	0	24.19	124.26	7.43	49.7	14.2	4.7
3	SM-ML	3	0.00	0	30	30	1.84	0.99	7.67	0	20.9	22.4	1.13	0	160.67	13.300	100.56	6.18	11.3	60.47	0	0	84.66	185.22	12.17	74.08	35.87	7.7
4	SM-ML	2	0.00	0	30	30	1.82	0.95	9.57	0	20.9	22.4	1.13	0	200.48	12.760	81.36	8.62	7.53	56.21	0	0	140.9	222.23	15.33	88.89	54.77	9.7
5	CL	2.5	0.00	8	0	0	1.82	0.97	11.99	9	0	0	1.13	72	0	0.000	81.36	10.78	9.42	0	0.3	22.6	163.5	244.83	19.28	97.93	65.05	12.2
6	SM	2.8	0.00	0	30	30	1.82	0.95	14.65	0	20.9	22.4	1.13	0	306.9	12.760	361.21	13.32	10.6	121.69	0	0	285.2	646.37	23.7	258.54	103.54	15
7	SM	3	0.00	0	30	30	1.82	0.95	17.5	0	20.9	22.4	1.13	0	366.6	12.760	428.67	16.07	11.3	157.26	0	0	442.4	871.09	28.44	348.43	152.31	18
8	SM	1	0.00	0	30	30	1.82	0.95	18.45	0	20.9	22.4	1.13	0	386.5	12.760	451.16	17.97	3.76	58.51	0	0	500.9	952.09	30.02	380.83	170.28	19

**Recommendation :**

- a) Pile Diameter (mm)  
b) Pile cut off level (m)  
c) Pile Shaft Length from Cut off Level (m)  
d) Vertical Pile Capacity (tonnes)  
e) Uplift pile capacity (Tonnes)

1200	
2.3	
18.0	19.0
330.0	360.0
140.0	160.0

\* For vertical Capacity of Pile weight of the pile has not been considered.

Project no : 2152	Lateral Load Capacity of pile			
	[As per IS 2911-2010 Part 1Section-2] Annex-C			
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			
Structure @ Chainage :	VUP @ 25+430			
Borehole no :	BH 9			
Type of pile :	Bored cast in situ	Bored cast in situ		
Diameter of the pile in "mm" :	1000	1200		
Cut off Level of the Pile in "m" :	2.000	2.300		
Length of the Pile below the cut off level in "m" :	18.0	18.0		
Type of Pile Head :	fixed	fixed		
Cross-section of the Pile :	Circle	Circle		
Grade of the concrete (M):	35.0	35.0		
Type of Soil :	Granular	Granular		
Condition of Soil with w.r.t Ground water :	Submerged	Submerged		
No. of Blow (N)	14.00	14.00		
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07		
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05		
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	1.97E+03	1.97E+03		
Stiffness factor for Cohesionless soil (T) in m :	3.73	4.31		
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	0.000	0.000		
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	0.00	0.00		
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	18.00	18.00		
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R [As per Appendix C, Clause 5.5.2 Fig 2]:	2.19	2.19		
Depth of Fixidity L <sub>f</sub> in "m":	8.17	9.44		
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	8.17	9.44		
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile		
<b>Considering 1% of dia for Horizontal Deflection :</b>				
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>		
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :	31.96	51.55		
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	<b>25.00</b>	<b>40.00</b>		
Equations :				
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$				
For Free Head (Y) = [QLxx <sup>3</sup> ]/3EI ; For Fixed head (Y)=[QLxx <sup>3</sup> ]/12EI				

Project no: 2152	BEARING CAPACITY ANALYSIS FOR SHALLOW FOUNDATIONS		
	as per IS: 6403-1981		
Structure @ Chainage :	MNB @ 29+260	MNB @ 29+260	
Borehole no:	BH 11	BH 11	
Type of Foundation :	<b>Raft</b>	<b>Raft</b>	
Depth of Foundation below Grond level (D <sub>f</sub> ) :	<b>1.000</b>	<b>1.000</b>	
Width of the foundation (B) in "m":	<b>10.000</b>	<b>12.000</b>	
Length of the foundation (L) in "m" :	<b>20.000</b>	<b>20.000</b>	
Angle of Internal Friction ,Φ :	28	28	
Cohension , C (T/m <sup>2</sup> ) :	0	0	
Density of soil (γ) T/m <sup>3</sup> :	1.8	1.8	
Effective unit weight (γ') T/m <sup>3</sup> :	0.8	0.8	
Depth of water table (W.T) m from G.L :	5.5	5.5	
Design water table depth (W.T')m :	0	0	
Angle of Inclination factor :	0	0	
Depth factors (assumed that backfilling is not compacted properly)	1.00	1.00	
Surcharge at sub-base foundation level q= γ'D <sub>f</sub>	1.5	1.5	
Shape factors :	S <sub>c</sub>	1.1	1.12
	S <sub>q</sub>	1.1	1.12
	S <sub>γ</sub>	0.8	0.76
Inclination factors :	i <sub>c</sub>	1.00	1.00
	i <sub>q</sub>	1.00	1.00
	i <sub>γ</sub>	1.00	1.00
Depth factors :	dc = 1+0.2(D <sub>f</sub> /B)√(NΦ)	1.00	1.00
	dq = 1+0.1*(D <sub>f</sub> /B)√(NΦ) for >10°	1.00	1.00
	dγ = 1+0.1*(D <sub>f</sub> /B)√(NΦ) for >10°	1.00	1.00
<b>Shear failure criteria</b>			
Bearing capacity factor's for General Shear :	Φ	28	28
	N <sub>c</sub> = (N <sub>q</sub> -1)/tanθ	25.78	25.78
	N <sub>q</sub> = N <sub>γ</sub> /(2*tanθ)-1	14.71	14.71
	N <sub>γ</sub> = 2*{[(exp(π*tanθ)*] tan2(45+θ/2)+1]*tanθ}	16.71	16.71
Bearing capacity factor's for Local Shear :	Φ'	20	20
	N' <sub>c</sub>	14.42	14.42
	N' <sub>q</sub>	6.14	6.14
	N' <sub>γ</sub>	5.09	5.09
Correction factor for W.T (W')	0.50	0.50	
Factor of safety	2.50	2.50	
safe bearing pressure (T/m <sup>2</sup> ) : C*NC*Sc*ic*dc+q(Nq-1)*sq*iq*dq+0.50*B*γ*Nγ*sγ*ir*dγ*W'	9.91	10.88	
* Considering Bed protection work			


**Settlement criteria as per IS 8009(Part I),fig 12 :**

Structure @ Chainage :	MNB @ 29+260	MNB @ 29+260
Borehole no:	BH 11	BH 11
Depth of Foundation below Grond level (DF) :	1.00	1.00
Width of the foundation (B) in "m":	10.00	12.00
Corrected SPT (N) value =	11	11
settlement under footing with a load of 10 T/m <sup>2</sup> in dry cohesionless soil :	33	33
Settlement under footing with a load intensity of 10 T/m <sup>2</sup> after water table correction :	66	66
Settlement under footing with load intensity of 10 T/m <sup>2</sup> after Depth correction and rigidity correction	53	53
Net safe bearing pressure for 75 mm of settlements :	14	14



**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile" as per IRC 78-2014**

Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	32+170	Location	FLYOVER	Based on Bore Hole No	BH 12	Pile Cut-off level (m)	2.0
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	13.20	water Level considered (m)	0.00	Scour Level @ RL(m)	
Pile Diameter (mm)	1000	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	Liquefaction depth below Ground level (m)	0.00	RL of the Borehole (m)	
Maximum effective overburden pressure= 20*Diameter of pile. Assuming the strata @ 30 m and below to be same.						Scour level below cut-off level(m) :	0.000				

Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	γ (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>sp</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance $P_{pu} = Ap^* (cN_c + P_d N_q + 0.5 \gamma_v D N_{\gamma})$					Ultimate Shaft Friction $P_{su} = \sum (K_s P_{dl} \tan \delta) A_{sj} + a.c.A_s$					Total Ultimate Capacity, $P_u = P_{pu} + P_{su}$ (tonnes)	Weight of pile, $W_p$ (Tonnes)	Total Safe Capacity, $P_s$ (Tonnes) $P_s = \frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5.γ <sub>v</sub> .D.N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer P <sub>dl</sub> (t/m <sup>2</sup> )	A <sub>sj</sub> (m <sup>2</sup> )	[K <sub>s</sub> P <sub>dl</sub> Tan δ] A <sub>sj</sub>	Adhesion Factor, a	a.c.A <sub>s</sub>						P <sub>su</sub>
1	SM-ML / SM	1.7	0.00	0	29	29	1.82	1.01	1.71	0	18.1	19.3	0.79	0	30.91	9.000	31.32	0.85	5.33	3.76	0	0	0	31.32	1.86	12.52	1.86	1.7
2	Cl	3	0.00	8	0	0	1.85	1.01	4.74	9	0	0	0.79	72	0	0.000	56.52	3.22	9.42	0	0	0	0	56.52	5.15	22.6	5.15	4.7
3	Cl	2	0.00	14	0	0	1.88	1.02	6.78	9	0	0	0.79	126	0	0.000	98.91	5.76	6.28	0	0.3	26.37	26.37	125.28	7.34	50.11	14.72	6.7
4	Cl	2	0.00	14	0	0	1.88	1.02	8.82	9	0	0	0.79	126	0	0.000	98.91	7.8	6.28	0	0.3	26.37	52.74	151.65	9.53	60.66	24.29	8.7
5	SM-ML / SM	2	0.00	0	30	30	1.88	0.96	10.74	0	20.9	22.4	0.79	0	224.99	10.750	185.05	9.78	6.28	53.18	0	0	105.9	290.97	11.72	116.38	41.37	10.7
6	SM-ML / SM	2	0.00	0	30	30	1.88	0.95	12.64	0	20.9	22.4	0.79	0	264.79	10.640	216.21	11.69	6.28	63.57	0	0	169.5	385.7	13.91	154.28	61.36	12.7
7	CH	2	0.00	14	0	0	1.88	0.97	14.58	9	0	0	0.79	126	0	0.000	98.91	13.61	6.28	0	0.3	26.37	195.9	294.77	16.1	117.9	70.94	14.7
8	CH	2	0.00	14	0	0	1.88	0.97	16.52	9	0	0	0.79	126	0	0.000	98.91	15.55	6.28	0	0.3	26.37	222.2	321.14	18.29	128.45	80.51	16.7
9	CH	2.3	0.00	11	0	0	1.88	0.97	18.75	9	0	0	0.79	99	0	0.000	77.71	17.63	7.22	0	0.3	23.82	246.1	323.76	20.81	129.5	89.7	19
10	CH	1	0.00	11	0	0	1.88	0.97	19.72	9	0	0	0.79	99	0	0.000	77	19.23	3.14	0	0.3	10.36	256.4	333.41	21.9	133.36	93.69	20
11	CH	2	0.00	11	0	0	1.88	0.97	19.72	9	0	0	0.79	99	0	0.000	77	19.72	6.28	0	0.3	20.72	277.1	354.13	24.09	141.65	101.68	22
12	CH	2	0.00	11	0	0	1.88	0.97	19.72	9	0	0	0.79	99	0	0.000	77	19.72	6.28	0	0.3	20.72	297.9	374.85	26.28	149.94	109.67	24
13	CH	2	0.00	15	0	0	1.88	0.97	19.72	9	0	0	0.79	135	0	0.000	105	19.72	6.28	0	0.3	28.26	326.1	431.11	28.47	172.44	119.78	26
14	CH	2	0.00	15	0	0	1.88	0.97	19.72	9	0	0	0.79	135	0	0.000	105	19.72	6.28	0	0.3	28.26	354.4	459.37	30.66	183.74	129.88	28

**Recommendation :**

- a) Pile Diameter (mm)
- b) Pile cut off level (m)
- c) Pile Shaft Length from Cut off Level (m)
- d) Vertical Pile Capacity ( tonnes)
- e) Uplift pile capacity (Tonnes)

1000		
2.0		
24.0	26.0	28.0
140.0	160.0	170.0
100.0	110.0	120.0

\* For vertical Capacity of Pile weight of the pile has not been considered.



**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile" as per IRC 78-2014**

Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	32+170	Location	FLYOVER	Based on Bore Hole No	BH 12	Pile Cut-off level (m)	2.3
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	13.20	water Level considered (m)	0.00	Scour Level @ RL(m)	
Pile Diameter (mm)	1200	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	Liquefaction depth below Ground level (m)	0.00	RL of the Borehole (m)	
Maximum effective overburden pressure= 20*Diameter of pile. Assuming the strata @ 30 m and below to be same.						Scour level below cut-off level(m) :	0.000				

Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	γ (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>sp</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance $P_{pu} = Ap^* (cN_c + P_d N_q + 0.5 \gamma_v D N_{\gamma})$					Ultimate Shaft Friction $P_{su} = \sum (K_s P_{dl} \tan \delta) A_{sj} + a.c.A_s$					Total Ultimate Capacity, $P_u = P_{pu} + P_{su}$ (tonnes)	Weight of pile, $W_p$ (Tonnes)	Total Safe Capacity, $P_s$ (Tonnes) $P_s = \frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5.γ <sub>v</sub> .D.N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer P <sub>dl</sub> (t/m <sup>2</sup> )	A <sub>sj</sub> (m <sup>2</sup> )	[K <sub>s</sub> P <sub>dl</sub> Tan δ] A <sub>sj</sub>	Adhesion Factor, a	a.c.A <sub>s</sub>						P <sub>su</sub>
1	SM-ML / SM	1.7	0.00	0	29	29	1.82	1.01	1.71	0	18.1	19.3	1.13	0	30.91	11.000	47.35	0.85	6.4	4.52	0	0	0	47.35	2.68	18.94	2.68	1.7
2	Cl	3	0.00	8	0	0	1.85	1.01	4.74	9	0	0	1.13	72	0	0.000	81.36	3.22	11.3	0	0	0	0	81.36	7.42	32.54	7.42	4.7
3	Cl	2	0.00	14	0	0	1.88	1.02	6.78	9	0	0	1.13	126	0	0.000	142.38	5.76	7.53	0	0.3	31.62	31.62	174	10.58	69.6	19.43	6.7
4	Cl	2	0.00	14	0	0	1.88	1.02	8.82	9	0	0	1.13	126	0	0.000	142.38	7.8	7.53	0	0.3	31.62	63.24	205.62	13.74	82.24	31.44	8.7
5	SM-ML / SM	2	0.00	0	30	30	1.88	0.96	10.74	0	20.9	22.4	1.13	0	224.99	12.900	268.81	9.78	7.53	63.77	0	0	127	395.82	16.9	158.32	52.46	10.7
6	SM-ML / SM	2	0.00	0	30	30	1.88	0.95	12.64	0	20.9	22.4	1.13	0	264.79	12.760	313.63	11.69	7.53	76.23	0	0	203.2	516.87	20.06	206.74	76.96	12.7
7	CH	2	0.00	14	0	0	1.88	0.97	14.58	9	0	0	1.13	126	0	0.000	142.38	13.61	7.53	0	0.3	31.62	234.9	377.24	23.22	150.89	88.98	14.7
8	CH	2	0.00	14	0	0	1.88	0.97	16.52	9	0	0	1.13	126	0	0.000	142.38	15.55	7.53	0	0.3	31.62	266.5	408.86	26.38	163.54	100.99	16.7
9	CH	2.3	0.00	11	0	0	1.88	0.97	18.75	9	0	0	1.13	99	0	0.000	111.87	17.63	8.66	0	0.3	28.57	295.1	406.92	30.01	162.76	112.62	19
10	CH	1	0.00	11	0	0	1.88	0.97	19.72	9	0	0	1.13	99	0	0.000	111	19.23	3.76	0	0.3	12.4	307.5	418.45	31.59	167.38	117.67	20
11	CH	2	0.00	11	0	0	1.88	0.97	21.66	9	0	0	1.13	99	0	0.000	111	20.69	7.53	0	0.3	24.84	332.3	443.29	34.75	177.31	127.79	22
12	CH	2	0.00	11	0	0	1.88	0.97	23.6	9	0	0	1.13	99	0	0.000	111	22.63	7.53	0	0.3	24.84	357.1	468.13	37.91	187.25	137.9	24
13	CH	2	0.00	15	0	0	1.88	0.97	23.6	9	0	0	1.13	135	0	0.000	152	23.6	7.53	0	0.3	33.88	391	543.01	41.07	217.2	150.55	26
14	CH	2	0.00	15	0	0	1.88	0.97	23.6	9	0	0	1.13	135	0	0.000	152	23.6	7.53	0	0.3	33.88	424.9	576.89	44.23	230.75	163.19	28

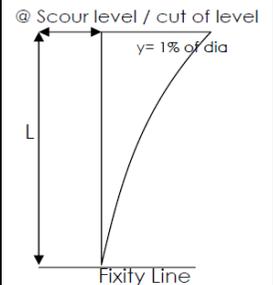
**Recommendation :**

- a) Pile Diameter (mm)
- b) Pile cut off level (m)
- c) Pile Shaft Length from Cut off Level (m)
- d) Vertical Pile Capacity ( tonnes)
- e) Uplift pile capacity (Tonnes)

1200		
2.3		
24.0	26.0	28.0
180.0	200.0	220.0
130.0	140.0	150.0

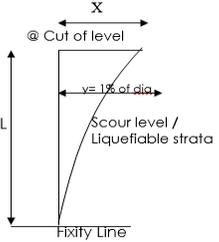
\* For vertical Capacity of Pile weight of the pile has not been considered.

Project no : 2152		Lateral Load Capacity of pile		
		[As per IS 2911-2010 Part 1 Section-2] Annex-C		
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			
Structure @ Chainage :	Flyover @ 32+170			
Borehole no :	BH 12			
Type of pile :	Bored cast in situ	Bored cast in situ		
Diameter of the pile in "mm" :	1000	1200		
Cut off Level of the Pile in "m" :	2.000	2.300		
Length of the Pile below the cut off level in "m" :	24.0	24.0		
Type of Pile Head :	fixed	fixed		
Cross-section of the Pile :	Circle	Circle		
Grade of the concrete (M):	35.0	35.0		
Type of Soil :	Granular	Granular		
Condition of Soil with w.r.t Ground water :	Submerged	Submerged		
No. of Blow (N)	21.00	21.00		
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07		
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05		
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	2.98E+03	2.98E+03		
Stiffness factor for Cohesionless soil (T) in m :	3.43	3.97		
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	0.000	0.000		
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	0.00	0.00		
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	24.00	24.00		
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R {As per Appendix C, Clause 5.5.2 Fig 2):	2.19	2.19		
Depth of Fixidity L <sub>f</sub> in "m":	7.51	8.69		
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	7.51	8.69		
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile		
<b>Considering 1% of dia for Horizontal Deflection :</b>				
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>		
Lateral capacity of pile , Q (Tonnes) for 1% dia. deflection :	41.10	65.97		
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	<b>30.00</b>	<b>50.00</b>		
Equations :				
	$T = (EI/n_h)^{1/5}$ ; $R = (EI/K_1)^{1/4}$			
	<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>			







Project no : 2152	Lateral Load Capacity of pile		
	[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :	MJB @ 33+420		
Borehole no :	BH 13		
Type of pile :	Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :	1000	1200	
Cut off Level of the Pile in "m" :	2.000	2.300	
Length of the Pile below the cut off level in "m" :	31.0	31.0	
Type of Pile Head :	fixed	fixed	
Crossection of the Pile :	Circle	Circle	
Gade of the concrete (M):	35.0	35.0	
Type of Soil :	Granular	Granular	
Condition of Soil with w.r.t Ground water :	Submerged	Submerged	
No. of Blow (N)	18.00	18.00	
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	2.55E+03	2.55E+03	
Stiffness factor for Cohesionless soil (T) in m :	3.54	4.09	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	13.000	12.700	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	3.67	3.11	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	18.00	18.30	
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R (As per Appendix C, Clause 5.5.2 Fig 2):	1.86	1.88	
Depth of Fixity L <sub>f</sub> in "m":	6.60	7.71	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	19.60	20.41	
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>			
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>	
Horizontal Deflection on the top of the pile (x) " in mm" :	37.9	37.5	
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :	8.77	15.94	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	5.00	10.00	
Equations :			
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$			
<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>			





Project no : 2152		Lateral Load Capacity of pile		
		[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :		Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :		MJB @ 33+490		
Borehole no :		BH 14		
Type of pile :		Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :		1000	1200	
Cut off Level of the Pile in "m" :		2.000	2.300	
Length of the Pile below the cut off level in "m" :		30.0	30.0	
Type of Pile Head :		fixed	fixed	
Crossection of the Pile :		Circle	Circle	
Gade of the concrete (M):		35.0	35.0	
Type of Soil :		Granular	Granular	
Condition of Soil with w.r.t Ground water :		Submerged	Submerged	
No. of Blow (N)		20.00	20.00	
Moment of Inertia , I in "cm <sup>4</sup> " :		4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :		2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :		2.84E+03	2.84E+03	
Stiffness factor for Cohesionless soil (T) in m :		3.46	4.01	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":		9.510	9.210	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :		2.75	2.30	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :		20.49	20.79	
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R [As per Appendix C, Clause 5.5.2 Fig 2]:		1.90	1.92	
Depth of Fixity L <sub>f</sub> in "m":		6.57	7.69	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"		16.08	16.90	
Type of Pile Behaviour :		Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>				
Permissible Horizontal Deflection pile (Y) " in mm":		10.00	12.00	
Horizontal Deflection on the top of the pile (x) " in mm":		27.5	27.7	
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :		11.51	20.75	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>		10.00	18.00	
Equations :				
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$				
<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>				





Project no : 2152		Lateral Load Capacity of pile		
		[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :		Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :		MJB @ 35+860		
Borehole no :		BH 15		
Type of pile :		Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :		1000	1200	
Cut off Level of the Pile in "m" :		2.000	2.300	
Length of the Pile below the cut off level in "m" :		28.0	28.0	
Type of Pile Head :		fixed	fixed	
Crossection of the Pile :		Circle	Circle	
Gade of the concrete (M):		35.0	35.0	
Type of Soil :		Granular	Granular	
Condition of Soil with w.r.t Ground water :		Submerged	Submerged	
No. of Blow (N)		15.00	15.00	
Moment of Inertia , I in "cm <sup>4</sup> " :		4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :		2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :		2.12E+03	2.12E+03	
Stiffness factor for Cohesionless soil (T) in m :		3.67	4.25	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":		7.000	6.700	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :		1.91	1.58	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :		21.00	21.30	
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R (As per Appendix C, Clause 5.5.2 Fig 2):		1.94	1.96	
Depth of Fixity L <sub>f</sub> in "m":		7.12	8.32	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"		14.12	15.02	
Type of Pile Behaviour :		Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>				
Permissible Horizontal Deflection pile (Y) " in mm":		<b>10.00</b>	<b>12.00</b>	
Horizontal Deflection on the top of the pile (x) " in mm":		19.7	20.7	
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :		12.22	22.05	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>		<b>10.00</b>	<b>18.00</b>	
Equations :				
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$				
<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>				



**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile"as per IRC 78-2014**

Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	38+010	Location	MNB	Based on Bore Hole No	BH 16	Pile Cut -off level (m)	2.0	
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	2.70	water Level considered (m)	0.00	Scour Level @ RL(m)	262.707	
File Diameter (mm)	1000	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	Liquefaction depth below Ground level (m)	9.00	RL of the Borehole (m)	263.430	
Maximum effective overburden pressure= 20*Diameter of pile. R.L's and scour level provided by the client.Assuming the strata @ 20 m and below to be same.												
							Liquefaction depth below cut-off level(m) :	7.000				

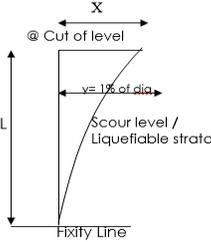
Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	r (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors						Ultimate Base Resistance $P_{pu} = Ap^* (cN_c + P_d N_q + 0.5 \gamma_r D N_{\gamma})$						Ultimate Shaft Friction $P_{su} = [\sum (K_s P_{dl} \tan \delta) \cdot A_s + a \cdot c \cdot A_s]$						Total Ultimate Capacity, $P_u = P_{pu} + P_{su}$ (tonnes)	Weight of pile, W <sub>p</sub> (Tonnes)	Total Safe Capacity, P <sub>s</sub> (Tonnes) $P_s = \frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5·γ <sub>r</sub> ·D·N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer P <sub>dl</sub> (t/m <sup>2</sup> )	A <sub>s</sub> (m <sup>2</sup> )	(K <sub>s</sub> P <sub>dl</sub> tanδ)·A <sub>s</sub>	Adhesion Factor, α	a.c.A <sub>s</sub>	P <sub>su</sub>									
1	SM-ML / SM	2	0.00	0	26	26	1.75	0.93	0	0	11.6	12.5	0.79	0	0	5.000	0	0	6.28	0	0	0	0	0	2.19	0	2.19	2				
2	SM	2	0.00	0	28	28	1.77	0.93	0	0	15.6	16.7	0.79	0	0	7.770	0	0	6.28	0	0	0	0	0	4.38	0	4.38	4				
3	Cl-CH	3	0.00	2	0	0	1.8	0.93	0	9	0	0	0.79	18	0	0.000	0	0	9.42	0	0.3	5.65	0	0	7.67	0	7.67	7				
4	Cl-CH	4	0.00	7	0	0	1.86	0.93	3.72	9	0	0	0.79	63	0	0.000	49.45	1.86	12.6	0	0.3	26.37	26.37	75.82	12.06	30.32	19.44	11				
5	Cl-CH	2	0.00	7	0	0	1.86	0.93	5.58	9	0	0	0.79	63	0	0.000	49.45	4.65	6.28	0	0.3	13.18	39.55	89	14.25	35.6	25.32	13				
6	Cl-CH	3	0.00	9	0	0	1.86	0.93	8.37	9	0	0	0.79	81	0	0.000	63.58	6.97	9.42	0	0.3	25.43	64.98	128.56	17.54	51.42	35.73	16				
7	Cl-CH	2	0.00	9	0	0	1.86	0.93	10.23	9	0	0	0.79	81	0	0.000	63.58	9.3	6.28	0	0.3	16.95	81.93	145.51	19.73	58.2	42.67	18				
8	Cl-CH	2	0.00	9	0	0	1.86	0.93	12.09	9	0	0	0.79	81	0	0.000	63.58	11.16	6.28	0	0.3	16.95	98.88	162.46	21.92	64.98	49.6	20				
9	Cl-CH	2	0.00	9	0	0	1.86	0.93	13.95	9	0	0	0.79	81	0	0.000	63.58	13.02	6.28	0	0.3	16.95	115.8	179.41	24.11	71.76	56.54	22				
10	Cl-CH	2	0.00	9	0	0	1.86	0.93	15.81	9	0	0	0.79	81	0	0.000	63	14.88	6.28	0	0.3	16.95	132.8	195.78	26.3	78.31	63.47	24				

**Recommendation :**

- a) Pile Diameter (mm) 1000
- b) Pile cut off level (m) 2.0
- c) Pile Shaft Length from Cut off Level (m) 24.0
- d) Vertical Pile Capacity ( tonnes) 70.0
- e) Uplift pile capacity (Tonnes) 60.0

\* For vertical Capacity of Pile weight of the pile has not been considered.



Project no : 2152		Lateral Load Capacity of pile		
		[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :		Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :		MNB @ 38+010		
Borehole no :		BH 16		
Type of pile :		Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :		1000	1200	
Cut off Level of the Pile in "m" :		2.000	2.300	
Length of the Pile below the cut off level in "m" :		24.0	24.0	
Type of Pile Head :		fixed	fixed	
Crossection of the Pile :		Circle	Circle	
Gade of the concrete (M):		35.0	35.0	
Type of Soil :		Granular	Granular	
Condition of Soil with w.r.t Ground water :		Submerged	Submerged	
No. of Blow (N)		16.00	16.00	
Moment of Inertia , I in "cm <sup>4</sup> " :		4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :		2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :		2.26E+03	2.26E+03	
Stiffness factor for Cohesionless soil (T) in m :		3.62	4.19	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":		7.000	6.700	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :		1.93	1.60	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :		17.00	17.30	
Reading from the graph L <sub>F</sub> /T or L <sub>F</sub> /R (As per Appendix C, Clause 5.5.2 Fig 2):		1.94	1.96	
Depth of Fixity L <sub>F</sub> in "m":		7.02	8.19	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>F</sub> ) in "m"		14.02	14.89	
Type of Pile Behaviour :		Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>				
Permissible Horizontal Deflection pile (Y) " in mm":		10.00	12.00	
Horizontal Deflection on the top of the pile (x) " in mm":		20.0	20.9	
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :		12.62	22.83	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>		10.00	18.00	
Equations :				
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$				
<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>				





**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile" as per IRC 78-2014**

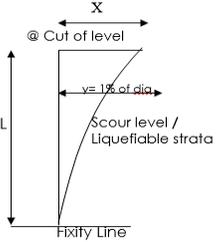
Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	39+510	Location	MJB	Based on Bore Hole No	BH 17	Pile Cut-off level (m)	2.3	
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	2.70	water Level considered (m)	0.00	Scour Level @ RL(m)		
Pile Diameter (mm)	1200	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	Liquefaction depth below Ground level (m)	12.00	RL of the Borehole (m)		
Maximum effective overburden pressure= 20*Diameter of pile. R.L's and scour level provided by the client.Assuming the strata @ 30 m and below to be same.												
							Liquefaction depth below cut-off level(m) :	9.700				

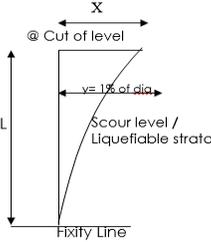
Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	γ (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>sp</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance P <sub>pu</sub> = Ap* (cN <sub>c</sub> +P <sub>d</sub> N <sub>q</sub> +0.5γ <sub>v</sub> D <sub>v</sub> N <sub>γ</sub> )					Ultimate Shaft Friction P <sub>su</sub> = [Σ(K <sub>s</sub> P <sub>d</sub> tanδ) <sub>s</sub> + a.c.A <sub>s</sub> ]					Total Ultimate Capacity, P <sub>u</sub> =P <sub>pu</sub> + P <sub>su</sub> (tonnes)	Weight of pile, W <sub>p</sub> (Tonnes)	Total Safe Capacity, P <sub>s</sub> (Tonnes)	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5γ <sub>v</sub> D <sub>v</sub> N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer P <sub>ai</sub> ' (t/m <sup>2</sup> )	A <sub>si</sub> (m <sup>2</sup> )	[K <sub>s</sub> P <sub>d</sub> tanδ) <sub>s</sub>	Adhesion Factor, α	a.c.A <sub>s</sub>						P <sub>su</sub>
1	SM-ML / SM	1.7	0.00	0	28	28	1.75	0.93	0	0	15.6	16.7	1.13	0	0	9.000	0	0	6.4	0	0	0	0	0	2.68	0	2.68	1.7
2	SM-ML / SM	3	0.00	0	28	28	1.75	0.93	0	0	15.6	16.7	1.13	0	0	9.320	0	0	11.3	0	0	0	0	0	7.42	0	7.42	4.7
3	SM-ML / SM	3	0.00	0	28	28	1.76	0.89	0	0	15.6	16.7	1.13	0	0	8.920	0	0	11.3	0	0	0	0	0	12.16	0	12.16	7.7
4	SM-ML / SM	2	0.00	0	29	29	1.76	0.89	0	0	18.1	19.3	1.13	0	0	10.320	0	0	7.53	0	0	0	0	0	15.32	0	15.32	9.7
5	SM-ML / SM	2	0.00	0	29	29	1.76	0.90	1.8	0	18.1	19.3	1.13	0	32.54	10.440	48.56	0.9	7.53	5.63	0	0	5.63	54.19	18.48	21.67	20.05	11.7
6	SM-ML / SM	2	0.00	0	29	29	1.76	0.90	3.6	0	18.1	19.3	1.13	0	65.08	10.440	85.33	2.7	7.53	16.9	0	0	22.53	107.86	21.64	43.14	27.94	13.7
7	CH	2	0.00	8	0	0	1.8	0.91	5.42	9	0	0	1.13	72	0	0.000	81.36	4.51	7.53	0	0.3	18.07	40.6	121.96	24.8	48.78	36.16	15.7
8	CH	2.3	0.00	8	0	0	1.8	0.91	7.51	9	0	0	1.13	72	0	0.000	81.36	6.46	8.66	0	0.3	20.78	61.38	142.74	28.43	57.09	45.61	18
9	CH	2	0.00	12	0	0	1.8	0.91	9.33	9	0	0	1.13	108	0	0.000	122.04	8.42	7.53	0	0.3	27.1	88.48	210.52	31.59	84.2	56.36	20
10	CH	2	0.00	12	0	0	1.8	0.91	11.15	9	0	0	1.13	108	0	0.000	122	10.24	7.53	0	0.3	27.1	115.6	237.58	34.75	95.03	67.11	22
11	CH	2	0.00	12	0	0	1.86	0.91	12.97	9	0	0	1.13	108	0	0.000	122	12.06	7.53	0	0.3	27.1	142.7	264.68	37.91	105.87	77.86	24
12	CH	2	0.00	12	0	0	1.86	0.91	14.79	9	0	0	1.13	108	0	0.000	122	13.88	7.53	0	0.3	27.1	169.8	291.78	41.07	116.71	88.6	26
13	CH	2	0.00	17	0	0	1.86	0.91	16.61	9	0	0	1.13	153	0	0.000	172	15.7	7.53	0	0.3	38.4	208.2	380.18	44.23	152.07	102.52	28
14	CH	2	0.00	17	0	0	1.86	0.91	18.43	9	0	0	1.13	153	0	0.000	172	17.52	7.53	0	0.3	38.4	246.6	418.58	47.39	167.43	116.43	30

**Recommendation :**

a) Pile Diameter (mm)	1200	
b) Pile cut off level (m)	2.3	
c) Pile Shaft Length from Cut off Level (m)	28.0	30.0
d) Vertical Pile Capacity ( tonnes)	150.0	160.0
e) Uplift pile capacity (Tonnes)	110.0	110.0

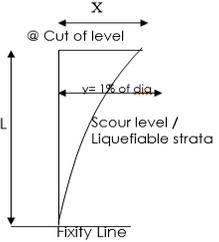
\* For vertical Capacity of Pile weight of the pile has not been considered.

Project no : 2152	Lateral Load Capacity of pile		
	[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :	MJB @ 39+690		
Borehole no :	BH 18		
Type of pile :	Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :	1000	1200	
Cut off Level of the Pile in "m" :	2.000	2.300	
Length of the Pile below the cut off level in "m" :	29.0	29.0	
Type of Pile Head :	fixed	fixed	
Crossection of the Pile :	Circle	Circle	
Gade of the concrete (M):	35.0	35.0	
Type of Soil :	Granular	Granular	
Condition of Soil with w.r.t Ground water :	Submerged	Submerged	
No. of Blow (N)	16.00	16.00	
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	2.26E+03	2.26E+03	
Stiffness factor for Cohesionless soil (T) in m :	3.62	4.19	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	4.000	3.700	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	1.10	0.88	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	25.00	25.30	
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R (As per Appendix C, Clause 5.5.2 Fig 2):	1.99	2.01	
Depth of Fixity L <sub>f</sub> in "m":	7.20	8.43	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	11.20	12.13	
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>			
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>	
Horizontal Deflection on the top of the pile (x) " in mm" :	14.1	15.4	
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :	17.48	31.19	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	15.00	30.00	
Equations :			
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$			
<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>			

Project no : 2152		Lateral Load Capacity of pile		
		[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :		Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :		MJB @ 39+510		
Borehole no :		BH 17		
Type of pile :		Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :		1000	1200	
Cut off Level of the Pile in "m" :		2.000	2.300	
Length of the Pile below the cut off level in "m" :		28.0	28.0	
Type of Pile Head :		fixed	fixed	
Crossection of the Pile :		Circle	Circle	
Gade of the concrete (M):		35.0	35.0	
Type of Soil :		Granular	Granular	
Condition of Soil with w.r.t Ground water :		Submerged	Submerged	
No. of Blow (N)		16.00	16.00	
Moment of Inertia , I in "cm <sup>4</sup> " :		4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :		2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :		2.26E+03	2.26E+03	
Stiffness factor for Cohesionless soil (T) in m :		3.62	4.19	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":		10.000	9.700	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :		2.76	2.32	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :		18.00	18.30	
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R (As per Appendix C, Clause 5.5.2 Fig 2):		1.90	1.92	
Depth of Fixity L <sub>f</sub> in "m":		6.87	8.04	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"		16.87	17.74	
Type of Pile Behaviour :		Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>				
Permissible Horizontal Deflection pile (Y) " in mm":		10.00	12.00	
Horizontal Deflection on the top of the pile (x) " in mm":		27.6	27.9	
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :		10.01	18.07	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>		9.00	15.00	
Equations :				
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$				
<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>				





Project no : 2152	Lateral Load Capacity of pile		
	[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :	MJB @ 39+690		
Borehole no :	BH 18		
Type of pile :	Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :	1000	1200	
Cut off Level of the Pile in "m" :	2.000	2.300	
Length of the Pile below the cut off level in "m" :	29.0	29.0	
Type of Pile Head :	fixed	fixed	
Crossection of the Pile :	Circle	Circle	
Gade of the concrete (M):	35.0	35.0	
Type of Soil :	Granular	Granular	
Condition of Soil with w.r.t Ground water :	Submerged	Submerged	
No. of Blow (N)	16.00	16.00	
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	2.26E+03	2.26E+03	
Stiffness factor for Cohesionless soil (T) in m :	3.62	4.19	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	4.000	3.700	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	1.10	0.88	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	25.00	25.30	
Reading from the graph L <sub>F</sub> /T or L <sub>F</sub> /R (As per Appendix C, Clause 5.5.2 Fig 2):	1.99	2.01	
Depth of Fixity L <sub>F</sub> in "m":	7.20	8.43	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>F</sub> ) in "m"	11.20	12.13	
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>			
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>	
Horizontal Deflection on the top of the pile (x) " in mm" :	14.1	15.4	
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :	17.48	31.19	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	<b>15.00</b>	<b>30.00</b>	
Equations :			
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$			
<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>			



**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile" as per IRC 78-2014**

Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	40+940	Location	VUP	Based on Bore Hole No	BH 19	Pile Cut-off level (m)	2.0	
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	11.80	water Level considered (m)	0.00	Scour Level @ RL(m)		
Pile Diameter (mm)	1000	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	Liquefaction depth below Ground level (m)	0.00	RL of the Borehole (m)		
Maximum effective overburden pressure= 20*Diameter of pile. Assuming the strata @ 20 m and below to be same.							Scour level below cut-off level(m) :	0.000				

Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	γ (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance P <sub>pu</sub> = Ap* (cN <sub>c</sub> +P <sub>d</sub> N <sub>q</sub> +0.5γ <sub>v</sub> D.N <sub>y</sub> )					Ultimate Shaft Friction P <sub>su</sub> = (Σ(K <sub>s</sub> P <sub>d</sub> tanδ).A <sub>s</sub> +a.c.A <sub>s</sub> )					Total Ultimate Capacity, P <sub>u</sub> =P <sub>pu</sub> + P <sub>su</sub> (tonnes)	Weight of pile, W <sub>p</sub> (Tonnes)	Total Safe Capacity, P <sub>s</sub> (Tonnes) P <sub>s</sub> = $\frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>y</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5γ <sub>v</sub> D.N <sub>y</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer "P <sub>d</sub> " (t/m <sup>2</sup> )	A <sub>s</sub> (m <sup>2</sup> )	(K <sub>s</sub> P <sub>d</sub> tanδ).A <sub>s</sub>	Adhesion Factor, a	a.c.A <sub>s</sub>						P <sub>su</sub>
1	Cl	3	0.00	4	0	0	1.78	1.02	3.06	9	0	0	0.79	36	0	0.000	28.26	1.53	9.42	0	0.3	11.3	0	28.26	3.29	11.3	3.29	3
2	Cl	3	0.00	5	0	0	1.82	1.03	6.15	9	0	0	0.79	45	0	0.000	45.92	4.6	9.42	0	0.3	14.13	14.13	60.05	6.58	24.02	10.53	6
3	SM-ML/SM	3	0.00	0	31	31	1.91	1.02	9.21	0	23.9	26	0.79	0	220.35	13.250	82.27	7.68	9.42	65.2	0	0	79.33	161.6	9.87	64.64	32.08	9
4	SM-ML/SM	2	0.00	0	31	31	1.91	1.02	11.25	0	23.9	26	0.79	0	269.16	13.250	57	10.23	6.28	57.9	0	0	137.2	194.23	12.06	77.69	50.48	11
5	SM-ML/SM	2.5	0.00	0	31	31	1.91	1.02	13.8	0	23.9	26	0.79	0	330.17	13.250	269.58	12.52	7.85	88.58	0	0	225.8	495.39	14.8	198.15	78.02	13.5
6	SM-ML/SM	2	0.00	0	31	31	1.91	1.02	15.84	0	23.9	26	0.79	0	378.97	13.250	307.89	14.82	6.28	83.88	0	0	309.7	617.58	16.99	247.03	103.7	15.5
7	CH	2.5	0.00	13	0	0	1.91	1.05	18.46	9	0	0	0.79	117	0	0.000	91.84	17.15	7.85	0	0.3	30.61	340.3	432.14	19.73	172.85	115.01	18
8	CH	2	0.00	13	0	0	1.91	1.05	20.56	9	0	0	0.79	117	0	0.000	91.84	19.51	6.28	0	0.3	24.49	364.8	456.63	21.92	182.65	124.06	20
9	CH	1	0.00	13	0	0	1.91	1.04	20.56	9	0	0	0.79	117	0	0.000	91.84	20.56	3.14	0	0.3	12.24	377	468.87	23.01	187.54	128.57	21

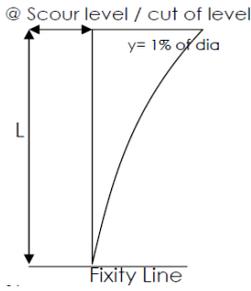
**Recommendation :**

- a) Pile Diameter (mm)  
b) Pile cut off level (m)  
c) Pile Shaft Length from Cut off Level (m)  
d) Vertical Pile Capacity (tonnes)  
e) Uplift pile capacity (Tonnes)

1000	
2.0	
18.0	21.0
160.0	180.0
100.0	120.0

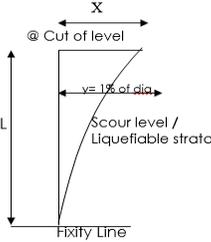
\* For vertical Capacity of Pile weight of the pile has not been considered.



Project no : 2152	Lateral Load Capacity of pile			
	[As per IS 2911-2010 Part 1Section-2] Annex-C			
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			
Structure @ Chainage :	VUP @40+940			
Borehole no :	BH 19			
Type of pile :	Bored cast in situ	Bored cast in situ		
Diameter of the pile in "mm" :	1000	1200		
Cut off Level of the Pile in "m" :	2.000	2.300		
Length of the Pile below the cut off level in "m" :	18.0	18.0		
Type of Pile Head :	fixed	fixed		
Cross-section of the Pile :	Circle	Circle		
Grade of the concrete (M):	35.0	35.0		
Type of Soil :	Granular	Granular		
Condition of Soil with w.r.t Ground water :	Submerged	Submerged		
No. of Blow (N)	8.00	8.00		
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07		
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05		
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	1.00E+03	1.00E+03		
Stiffness factor for Cohesion soil (T) in m :	4.27	4.94		
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	0.000	0.000		
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	0.00	0.00		
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	18.00	18.00		
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R (As per Appendix C, Clause 5.5.2 Fig 2):	2.19	2.19		
Depth of Fixidity L <sub>f</sub> in "m":	9.35	10.82		
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	9.35	10.82		
Type of Pile Behaviour :	Long Flexible Pile	Rigid & Elastic pile		
<b>Considering 1% of dia for Horizontal Deflection :</b>				
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>		
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :	21.30	34.24		
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	<b>15.00</b>	<b>25.00</b>		
Equations :				
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$				
For Free Head (Y) = [QLxx <sup>3</sup> ]/3EI ; For Fixed head (Y)=[QLxx <sup>3</sup> ]/12EI				

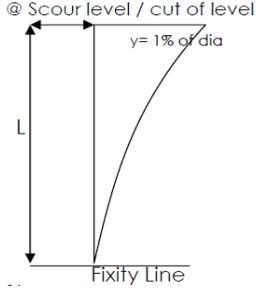




Project no : 2152		Lateral Load Capacity of pile		
		[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :		Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :		MJB @ 42+550		
Borehole no :		BH 20		
Type of pile :		Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :		1000	1200	
Cut off Level of the Pile in "m" :		2.000	2.300	
Length of the Pile below the cut off level in "m" :		29.0	29.0	
Type of Pile Head :		fixed	fixed	
Crossection of the Pile :		Circle	Circle	
Gade of the concrete (M):		35.0	35.0	
Type of Soil :		Granular	Granular	
Condition of Soil with w.r.t Ground water :		Submerged	Submerged	
No. of Blow (N)		18.00	18.00	
Moment of Inertia , I in "cm <sup>4</sup> " :		4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :		2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :		2.55E+03	2.55E+03	
Stiffness factor for Cohesionless soil (T) in m :		3.54	4.09	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":		8.000	7.700	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :		2.26	1.88	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :		21.00	21.30	
Reading from the graph L <sub>F</sub> /T or L <sub>F</sub> /R [As per Appendix C, Clause 5.5.2 Fig 2]:		1.92	1.94	
Depth of Fixidity L <sub>F</sub> in "m":		6.80	7.94	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>F</sub> ) in "m"		14.80	15.64	
Type of Pile Behaviour :		Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>				
Permissible Horizontal Deflection pile (Y) " in mm" :		10.00	12.00	
Horizontal Deflection on the top of the pile (x) " in mm" :		22.8	23.5	
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :		12.24	22.16	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>		10.00	20.00	
Equations :				
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$				
<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>				





Project no : 2152	Lateral Load Capacity of pile		
	[As per IS 2911-2010 Part 1 Section-2] Annex-C		
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :	Flyover @ 43+910		
Borehole no :	BH 21		
Type of pile :	Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :	1000	1200	
Cut off Level of the Pile in "m" :	2.000	2.300	
Length of the Pile below the cut off level in "m" :	21.0	21.0	
Type of Pile Head :	fixed	fixed	
Crossection of the Pile :	Circle	Circle	
Gade of the concrete (M):	35.0	35.0	
Type of Soil :	Granular	Granular	
Condition of Soil with w.r.t Ground water :	Submerged	Submerged	
No. of Blow (N)	9.00	9.00	
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	1.20E+03	1.20E+03	
Stiffness factor for Cohesionless soil (T) in m :	4.11	4.76	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	0.000	0.000	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	0.00	0.00	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	21.00	21.00	
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R [As per Appendix C, Clause 5.5.2 Fig 2]:	2.19	2.19	
Depth of Fixidity L <sub>f</sub> in "m":	9.00	10.42	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	9.00	10.42	
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>			
Permissible Horizontal Deflection pile (Y) " in mm":	<b>10.00</b>	<b>12.00</b>	
Lateral capcity of pile ,Q (Tonnes) for 1% dia. deflection :	23.89	38.27	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	20.00	30.00	
Equations :			
$T = (EI/n_h)^{1/5}$ ; $R = (EI/K_1)^{1/4}$			
For Free Head (Y) = [QLxx <sup>3</sup> ]/3EI ; For Fixed head (Y) = [QLxx <sup>3</sup> ]/12EI			



**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile"as per IRC 78-2014**

Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.				Structure @ Chainage	47+950	Location	MJB	Based on Bore Hole No	BH 22	Pile Cut -off level (m)	2.0
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	2.70	water Level considered (m)	0.00	Scour Level @ RL(m)		
Pile Diameter (mm)	1000	Earth Pressure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	Liquefaction depth below Ground level (m)	15.00	RL of the Borehole (m)		
<p>Maximum effective overburden pressure= 20*Diameter of pile.          Considering No Scour.Assuming the strata @ 20 m and below to be same.</p> <p align="right">Liquefaction depth below cut-off level(m) : <b>13.000</b></p>												

Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	γ (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance P <sub>pu</sub> = A <sub>p</sub> * (cN <sub>c</sub> +P <sub>d</sub> N <sub>b</sub> +0.5γ <sub>v</sub> D <sub>b</sub> N <sub>f</sub> )					Ultimate Shaft Friction P <sub>su</sub> = [Σ(K <sub>s</sub> P <sub>d</sub> tanδ) <sub>s</sub> +α.c.A <sub>s</sub> ]					Total Ultimate Capacity, P <sub>u</sub> =P <sub>pu</sub> + P <sub>su</sub> (tonnes)	Weight of pile, W <sub>p</sub> (Tonnes)	Total Safe Capacity, P <sub>s</sub> (Tonnes) P <sub>s</sub> = $\frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>f</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>b</sub>	0.5γ <sub>v</sub> D <sub>b</sub> N <sub>f</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer P <sub>ai</sub> ' (t/m <sup>2</sup> )	A <sub>si</sub> (m <sup>2</sup> )	(K <sub>s</sub> P <sub>d</sub> tanδ) <sub>s</sub>	Adhesion Factor, α	α.c.A <sub>s</sub>						P <sub>su</sub>
1	SM-ML / SM	3	0.00	0	30	30	1.86	0.98	0	0	20.9	22.4	0.79	0	0	10.000	0	0	9.42	0	0	0	0	0	3.29	0	3.29	3
2	SM	1	0.00	0	29	29	1.85	0.94	0	0	18.1	19.3	0.79	0	0	9.080	0	0	3.14	0	0	0	0	0	4.38	0	4.38	4
3	Cl-CH	3	0.00	8	0	0	1.87	0.99	0	9	0	0	0.79	72	0	0.000	0	0	9.42	0	0.3	22.6	0	0	7.67	0	7.67	7
4	SM-ML / SM	4	0.00	0	29	29	1.87	0.97	0	0	18.1	19.3	0.79	0	0	9.370	0	0	12.6	0	0	0	0	0	12.06	0	12.06	11
5	SM-ML / SM	2	0.00	0	29	29	1.87	0.97	0	0	18.1	19.3	0.79	0	0	9.370	0	0	6.28	0	0	0	0	0	14.25	0	14.25	13
6	SM-ML / SM	3	0.00	0	30	30	1.87	0.97	2.91	0	20.9	22.4	0.79	0	60.96	10.860	56.37	1.45	9.42	11.82	0	0	11.82	68.19	17.54	27.27	20.84	16
7	SM-ML / SM	2	0.00	0	30	30	1.87	0.97	4.85	0	20.9	22.4	0.79	0	101.6	10.860	88.28	3.88	6.28	21.1	0	0	32.92	121.2	19.73	48.48	28.94	18
8	SM-ML / SM	2	0.00	0	30	0	1.87	0.97	6.79	0	20.9	22.4	0.79	0	142.24	10.860	120.18	5.82	6.28	0	0	0	32.92	153.1	21.92	61.24	31.13	20
9	SM-ML / SM	2	0.00	0	30	30	1.87	0.97	8.73	0	20.9	22.4	0.79	0	182.88	10.860	152.08	7.76	6.28	42.2	0	0	75.12	227.2	24.11	90.88	45.14	22
10	SM-ML / SM	2	0.00	0	30	30	1.87	0.97	10.67	0	20.9	22.4	0.79	0	223.52	10.860	183	9.7	6.28	52.75	0	0	127.9	310.87	26.3	124.34	62.1	24
11	SM-ML / SM	2	0.00	0	30	30	1.87	0.97	12.61	0	20.9	22.4	0.79	0	264.16	10.860	215	11.64	6.28	63.3	0	0	191.2	406.17	28.49	162.46	82.01	26
12	SM-ML / SM	2	0.00	0	30	30	1.87	0.97	14.55	0	20.9	22.4	0.79	0	304.8	10.860	247	13.58	6.28	73.85	0	0	265	512.02	30.68	204.8	104.88	28
13	SM-ML / SM	2	0.00	0	30	30	1.87	0.97	16.49	0	20.9	22.4	0.79	0	345.44	10.860	279	15.52	6.28	84.4	0	0	349.4	628.42	32.87	251.36	130.7	30

**Recommendation :**

- a) Pile Diameter (mm) 1000  
 b) Pile cut off level (m) 2.0  
 c) Pile Shaft Length from Cut off Level (m) 30.0  
 d) Vertical Pile Capacity ( tonnes) 240.0  
 e) Uplift pile capacity (Tonnes) 120.0

\* For vertical Capacity of Pile weight of the pile has not been considered.



**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile"as per IRC 78-2014**

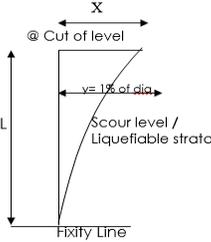
Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	47+950	Location	MJB	Based on Bore Hole No	BH 22	Pile Cut -off level (m)	2.3
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resistance	2.5	Actual Water table (m)	2.70	water Level considered (m)	0.00	Scour Level @ RL(m)	
Pile Diameter (mm)	1200	Earth Presure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	Liquefaction depth below Ground level (m)	15.00	RL of the Borehole (m)	
Maximum effective overburden pressure= 20*Diameter of pile. Considering No Scour.Assuming the strata @ 20 m and below to be same.											
							Liquefaction depth below cut-off level(m) :	12.700			

Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W.T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	γ (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective overburden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance P <sub>pu</sub> = Ap*(cN <sub>c</sub> +P <sub>d</sub> N <sub>q</sub> +0.5γ <sub>v</sub> D.N <sub>γ</sub> )					Ultimate Shaft Friction P <sub>su</sub> = [Σ(K <sub>s</sub> P <sub>d</sub> tanδ).A <sub>s</sub> +α.c.A <sub>s</sub> ]					Total Ultimate Capacity, P <sub>u</sub> =P <sub>pu</sub> + P <sub>su</sub> (tonnes)	Weight of pile, W <sub>p</sub> (Tonnes)	Total Safe Capacity, P <sub>s</sub> (Tonnes) $P_s = \frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										N <sub>c</sub>	N <sub>q</sub>	N <sub>γ</sub>	A <sub>p</sub> (m <sup>2</sup> )	c.N <sub>c</sub>	P <sub>d</sub> N <sub>q</sub>	0.5γ <sub>v</sub> D.N <sub>γ</sub>	P <sub>pu</sub> (tonnes)	Effective overburden Pressure at c.g of the layer P <sub>ai</sub> (t/m <sup>2</sup> )	A <sub>si</sub> (m <sup>2</sup> )	(K <sub>s</sub> P <sub>d</sub> Tanδ).A <sub>si</sub>	Adhesion Factor, α	α.c.A <sub>si</sub>						P <sub>su</sub>
1	SM-ML / SM	2.7	0.00	0	30	30	1.86	0.98	0	0	20.9	22.4	1.13	0	0	13.000	0	0	10.2	0	0	0	0	0	4.27	0	4.27	2.7
2	SM	1	0.00	0	29	29	1.85	0.94	0	0	18.1	19.3	1.13	0	0	10.900	0	0	3.76	0	0	0	0	0	5.85	0	5.85	3.7
3	Cl-CH	3	0.00	8	0	0	1.87	0.99	0	0	0	0	1.13	72	0	0.000	0	0	11.3	0	0.3	27.12	0	0	10.59	0	10.59	6.7
4	SM-ML / SM	4	0.00	0	29	29	1.87	0.97	0	0	18.1	19.3	1.13	0	0	11.250	0	0	15.1	0	0	0	0	0	16.91	0	16.91	10.7
5	SM-ML / SM	2	0.00	0	29	29	1.87	0.97	0	0	18.1	19.3	1.13	0	0	11.250	0	0	7.53	0	0	0	0	0	20.07	0	20.07	12.7
6	SM-ML / SM	3	0.00	0	30	30	1.87	0.97	2.91	0	20.9	22.4	1.13	0	60.96	13.030	83.6	1.45	11.3	14.18	0	0	14.18	97.78	24.81	39.11	28.78	15.7
7	SM-ML / SM	2	0.00	0	30	30	1.87	0.97	4.85	0	20.9	22.4	1.13	0	101.6	13.030	129.53	3.88	7.53	25.3	0	0	39.48	169.01	27.97	67.6	39.02	17.7
8	SM-ML / SM	2.3	0.00	0	30	0	1.87	0.97	7.08	0	20.9	22.4	1.13	0	148.31	13.030	182.31	5.96	8.66	0	0	0	39.48	221.79	31.6	88.71	42.65	20
9	SM-ML / SM	2	0.00	0	30	30	1.87	0.97	9.02	0	20.9	22.4	1.13	0	188.95	13.030	228.23	8.05	7.53	52.49	0	0	91.97	320.2	34.76	128.08	60.51	22
10	SM-ML / SM	2	0.00	0	30	30	1.87	0.97	10.96	0	20.9	22.4	1.13	0	229.59	13.030	274	9.99	7.53	65.14	0	0	157.1	431.11	37.92	172.44	81.91	24
11	SM-ML / SM	2	0.00	0	30	30	1.87	0.97	12.9	0	20.9	22.4	1.13	0	270.24	13.030	320	11.93	7.53	77.79	0	0	234.9	554.9	41.08	221.96	106.85	26
12	SM-ML / SM	2	0.00	0	30	30	1.87	0.97	14.84	0	20.9	22.4	1.13	0	310.88	13.030	366	13.87	7.53	90.44	0	0	325.3	691.34	44.24	276.53	135.33	28
13	SM-ML / SM	2	0.00	0	30	30	1.87	0.97	16.78	0	20.9	22.4	1.13	0	351.52	13.030	411	15.81	7.53	103.09	0	0	428.4	839.43	47.4	335.77	167.36	30

**Recommendation :**

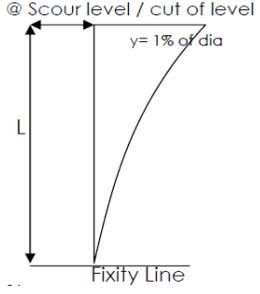
- a) Pile Diameter (mm) 1200
- b) Pile cut off level (m) 2.3
- c) Pile Shaft Length from Cut off Level (m) 30.0
- d) Vertical Pile Capacity ( tonnes) 320.0
- e) Uplift pile capacity (Tonnes) 160.0

\* For vertical Capacity of Pile weight of the pile has not been considered.

Project no : 2152	Lateral Load Capacity of pile		
	[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :	MJB @ 47+950		
Borehole no :	BH 22		
Type of pile :	Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :	1000	1200	
Cut off Level of the Pile in "m" :	2.000	2.300	
Length of the Pile below the cut off level in "m" :	30.0	30.0	
Type of Pile Head :	fixed	fixed	
Crossection of the Pile :	Circle	Circle	
Gade of the concrete (M):	35.0	35.0	
Type of Soil :	Granular	Granular	
Condition of Soil with w.r.t Ground water :	Submerged	Submerged	
No. of Blow (N)	24.00	24.00	
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	3.41E+03	3.41E+03	
Stiffness factor for Cohesionless soil (T) in m :	3.34	3.86	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	13.000	12.700	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	3.89	3.29	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	17.00	17.30	
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R (As per Appendix C, Clause 5.5.2 Fig 2):	1.86	1.88	
Depth of Fixity L <sub>f</sub> in "m":	6.20	7.25	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	19.20	19.95	
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>			
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>	
Horizontal Deflection on the top of the pile (x) " in mm" :	40.7	40.0	
Lateral capacity of pile ,Q (Tonnes) for 1% dia. deflection :	10.02	18.21	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	<b>9.00</b>	<b>17.00</b>	
Equations :			
$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$			
<b>For Free Head (Y) = [QLxx<sup>3</sup>]/3EI ; For Fixed head (Y) = [QLxx<sup>3</sup>]/12EI</b>			





Project no : 2152	Lateral Load Capacity of pile		
	[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :	Flyover @ 49+900		
Borehole no :	BH 23		
Type of pile :	Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :	1000	1200	
Cut off Level of the Pile in "m" :	2.000	2.300	
Length of the Pile below the cut off level in "m" :	20.0	20.0	
Type of Pile Head :	fixed	fixed	
Crossection of the Pile :	Circle	Circle	
Gade of the concrete (M):	35.0	35.0	
Type of Soil :	Granular	Granular	
Condition of Soil with w.r.t Ground water :	Submerged	Submerged	
No. of Blow (N)	12.00	12.00	
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	1.68E+03	1.68E+03	
Stiffness factor for Cohesionless soil (T) in m :	3.85	4.45	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	0.000	0.000	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	0.00	0.00	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	20.00	20.00	
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R [As per Appendix C, Clause 5.5.2 Fig 2]:	2.19	2.19	
Depth of Fixidity L <sub>f</sub> in "m":	8.43	9.75	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	8.43	9.75	
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>			
Permissible Horizontal Deflection pile (Y) " in mm":	10.00	12.00	
Lateral capcity of pile ,Q (Tonnes) for 1% dia. deflection :	29.06	46.84	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	20.00	35.00	
Equations :	$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$		
	$\text{For Free Head (Y)} = [QLxx^3]/3EI; \text{ For Fixed head (Y)} = [QLxx^3]/12EI$		

Annexure II  
Liquefaction Analysis

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.0	Efficiency in SPT Boring (for $C_E$ factor) "%":	60		
Structure @ Chainage	Flyover @ 0+800	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 1	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	4.50						
Water Table Depth considered (m)	0.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at site, $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM-ML	10	17.90	7.90	94	0.99	32.22	32.22	14.22	0.35	1.70	1.06	18.02	5.00	1.20	26.62	0.33	0.39	1.12	Non Liquefiable
3.3	SM-ML	5	17.90	7.90	43	0.97	59.07	59.07	26.07	0.34	1.30	1.06	6.90	5.00	1.20	13.28	0.14	0.17	0.50	Liquefiable
4.8	SM-ML	8	17.90	7.90	32	0.96	85.92	82.92	37.92	0.34	1.10	1.06	9.31	4.83	1.17	15.73	0.17	0.20	0.59	Liquefiable
6.3	SM-ML	11	17.40	7.40	37	0.95	112.02	94.02	49.02	0.34	1.03	1.06	12.03	5.00	1.20	19.43	0.21	0.25	0.73	Liquefiable
7.80	SM	13	17.40	7.40	29	0.94	138.12	105.12	60.12	0.34	0.98	1.06	13.44	4.64	1.15	20.04	0.22	0.26	0.76	Liquefiable
9.30	SM	17	17.40	7.40	24	0.93	164.22	116.22	71.22	0.33	0.93	1.06	16.72	4.18	1.11	22.69	0.25	0.30	0.90	Liquefiable
10.80	SM	21	17.40	7.40	30	0.89	190.32	127.32	82.32	0.32	0.89	1.06	19.73	4.71	1.15	27.48	0.35	0.42	1.32	Non Liquefiable
12.30	SM	23	17.40	7.40	27	0.85	216.42	138.42	93.42	0.31	0.85	1.06	20.72	4.48	1.13	27.90	0.37	0.44	1.43	Non Liquefiable
13.80	SM	28	17.40	7.40	19	0.81	242.52	149.52	104.52	0.29	0.82	1.06	24.27	3.43	1.07	29.47	0.43	0.52	1.78	Non Liquefiable
15.30	CI	17	17.40	7.40	89	0.77	268.62	160.62	115.62	0.28	0.79	1.06	14.22	5.00	1.20	22.06	0.24	0.29	1.04	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



Project : Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.00	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ Chainage	MJB @ 1+530	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 2	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	2.70						
Water Table Depth considered (m)	0.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{Field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_{cd}$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60CS</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM	5	17.40	7.40	29	0.99	31.32	31.32	13.32	0.36	1.70	1.06	9.01	4.64	1.15	14.96	0.16	0.19	0.53	Liquefiable
3.3	SM	6	17.40	7.40	33	0.97	57.42	51.42	24.42	0.36	1.39	1.06	8.87	4.88	1.18	15.34	0.16	0.20	0.55	Liquefiable
4.8	SM-ML	10	17.40	7.40	69	0.96	83.52	62.52	35.52	0.35	1.26	1.06	13.41	5.00	1.20	21.09	0.23	0.27	0.77	Liquefiable
6.3	SM	13	18.30	8.30	33	0.95	110.97	74.97	47.97	0.34	1.15	1.06	15.91	4.88	1.18	23.65	0.27	0.32	0.93	Liquefiable
7.80	SM	15	18.30	8.30	46	0.94	138.42	87.42	60.42	0.34	1.07	1.06	17.01	5.00	1.20	25.41	0.30	0.36	1.07	Non Liquefiable
9.30	SM	23	18.60	8.60	31	0.93	166.32	100.32	73.32	0.33	1.00	1.06	24.34	4.77	1.16	33.07	NA	NA	>1	Non Liquefiable
10.80	SM	33	18.60	8.60	39	0.89	194.22	113.22	86.22	0.31	0.94	1.06	32.87	5.00	1.20	44.45	NA	NA	>1	Non Liquefiable
12.30	SM	27	18.60	8.60	36	0.85	222.12	126.12	99.12	0.30	0.89	1.06	25.48	5.00	1.20	35.58	NA	NA	>1	Non Liquefiable
13.80	SM	17	18.90	8.90	98	0.81	250.47	139.47	112.47	0.28	0.85	1.06	15.26	5.00	1.20	23.31	0.26	0.31	1.12	Non Liquefiable
15.30	CL-CI	21	18.90	8.90	99	0.77	278.82	152.82	125.82	0.26	0.81	1.06	18.01	5.00	1.20	26.61	0.33	0.39	1.48	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.00	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ chainage	VUP @ 6+380	DesignPGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 3	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	13.80						
Water Table Depth considered (m)	9.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content ( % )	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM-ML	12	18.20	8.20	95	0.99	32.76	32.76	32.76	0.15	1.70	1.06	21.62	5.00	1.20	30.95	NA	NA	>1	Non Liquefiable
3.3	SM-ML	9	18.20	8.20	86	0.97	60.06	60.06	60.06	0.15	1.29	1.06	12.31	5.00	1.20	19.77	0.21	0.25	1.67	Non Liquefiable
4.8	SM-ML	27	18.20	8.20	92	0.96	87.36	87.36	87.36	0.15	1.07	1.06	30.62	5.00	1.20	41.74	NA	NA	>1	Non Liquefiable
6.3	SM	13	18.50	8.50	14	0.95	115.11	115.11	115.11	0.15	0.93	1.06	12.84	2.20	1.04	15.59	0.17	0.20	1.33	Non Liquefiable
7.8	SM	15	18.50	8.50	29	0.94	142.86	142.86	142.86	0.15	0.84	1.06	13.30	4.64	1.15	19.88	0.21	0.26	1.74	Non Liquefiable
9.3	SM	19	18.70	8.70	29	0.93	170.91	170.91	167.67	0.15	0.76	1.06	15.41	4.64	1.15	22.29	0.25	0.29	2.00	Non Liquefiable
10.8	SM	24	18.70	8.70	22	0.89	198.96	198.96	180.72	0.15	0.71	1.06	18.04	3.93	1.09	23.64	0.27	0.32	2.10	Non Liquefiable
12.3	SM	31	18.70	8.70	28	0.85	227.01	227.01	193.77	0.15	0.63	1.06	20.83	4.56	1.14	28.27	0.38	0.45	2.93	Non Liquefiable
13.8	SM	27	18.70	8.70	28	0.81	255.06	255.06	206.82	0.15	0.59	1.06	16.79	4.56	1.14	23.67	0.27	0.32	2.06	Non Liquefiable
15.3	SM	35	18.70	8.70	42	0.77	283.11	268.11	219.87	0.15	0.57	1.06	21.03	5.00	1.20	30.24	NA	NA	>1	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ Chainage :	FLYOVER @ 8+020	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 5	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	14.10						
Water Table Depth considered (m)	10.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM-ML	7	18.00	8.00	65	0.99	32.80	32.80	32.80	0.15	1.70	1.06	12.61	5.00	1.20	20.14	0.22	0.26	1.68	Non Liquefiable
3.3	SM-ML	10	18.00	8.00	71	0.97	59.80	59.80	59.80	0.15	1.29	1.06	13.71	5.00	1.20	21.45	0.23	0.28	1.84	Non Liquefiable
4.8	SM-ML	12	18.00	8.00	74	0.96	86.80	86.80	86.80	0.15	1.07	1.06	13.65	5.00	1.20	21.38	0.23	0.28	1.85	Non Liquefiable
6.3	SM	13	18.30	8.30	64	0.95	114.25	114.25	114.25	0.15	0.94	1.06	12.89	5.00	1.20	20.47	0.22	0.26	1.78	Non Liquefiable
7.80	SM	16	18.30	8.30	26	0.94	141.70	141.70	141.70	0.15	0.84	1.06	14.25	4.39	1.12	20.38	0.22	0.26	1.79	Non Liquefiable
9.30	CI	42	19.00	9.00	91	0.93	170.20	170.20	170.20	0.14	0.77	1.06	34.13	5.00	1.20	45.95	NA	NA	>1	Non Liquefiable
10.80	CI	32	19.00	9.00	88	0.89	198.70	198.70	190.70	0.14	0.71	1.06	24.06	5.00	1.20	33.88	NA	NA	>1	Non Liquefiable
12.30	SM-ML	24	19.00	9.00	95	0.85	227.20	227.20	204.20	0.15	0.63	1.06	16.12	5.00	1.20	24.34	0.28	0.33	2.27	Non Liquefiable
13.80	SM-ML	47	19.00	9.00	25	0.81	255.70	255.70	217.70	0.15	0.59	1.06	29.17	4.29	1.12	36.82	NA	NA	>1	Non Liquefiable
15.30	SM-ML	57	19.00	9.00	38	0.77	284.20	272.20	231.20	0.15	0.56	1.06	33.89	5.00	1.20	45.67	NA	NA	>1	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018



## Computation Sheet

**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7	Efficiency in SPT Boring (for $C_E$ factor) "%":	60		
Structure @ Chainage :	VUP @ 16+690	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 6	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	13.30						
Water Table Depth considered (m)	9.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	CI	11	18.40	8.40	86	0.99	33.12	33.12	33.12	0.15	1.70	1.06	19.82	5.00	1.20	28.79	0.40	0.48	3.10	Non Liquefiable
3.3	CI	19	18.40	8.40	93	0.97	60.72	60.72	60.72	0.15	1.28	1.06	25.85	5.00	1.20	36.02	NA	NA	>1	Non Liquefiable
4.8	CI	15	18.40	8.40	95	0.96	88.32	88.32	88.32	0.15	1.06	1.06	16.92	5.00	1.20	25.30	0.30	0.36	2.37	Non Liquefiable
6.3	SM-ML	24	18.60	8.60	32	0.95	116.22	116.22	116.22	0.15	0.93	1.06	23.60	4.83	1.17	32.46	NA	NA	>1	Non Liquefiable
7.80	SM	15	18.60	8.60	31	0.94	144.12	144.12	144.12	0.15	0.83	1.06	13.24	4.77	1.16	20.17	0.22	0.26	1.77	Non Liquefiable
9.30	SM	25	18.60	8.60	35	0.93	172.02	172.02	169.02	0.15	0.76	1.06	20.20	5.00	1.20	29.25	0.42	0.50	3.43	Non Liquefiable
10.80	CI	29	18.60	8.60	97	0.89	199.92	199.92	181.92	0.15	0.71	1.06	21.74	5.00	1.20	31.09	NA	NA	>1	Non Liquefiable
12.30	CI	32	18.60	8.60	97	0.85	227.82	227.82	194.82	0.15	0.63	1.06	21.45	5.00	1.20	30.75	NA	NA	>1	Non Liquefiable
13.80	CI	34	18.60	8.60	96	0.81	255.72	250.72	207.72	0.15	0.59	1.06	21.39	5.00	1.20	30.67	NA	NA	>1	Non Liquefiable
15.30	SM	38	18.60	8.60	20	0.77	283.62	263.62	220.62	0.15	0.57	1.06	23.10	3.61	1.08	28.55	0.39	0.47	3.03	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.0	Efficiency in SPT Boring (for $C_E$ factor) "%":	60		
Structure @ Chainage	MNB @ 21+810	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 7	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	11.30						
Water Table Depth considered (m)	7.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{Field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content ( % )	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at site, $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM-ML	6	17.90	7.90	82	0.99	32.22	32.22	32.22	0.15	1.70	1.06	10.81	5.00	1.20	17.97	0.19	0.23	1.48	Non Liquefiable
3.3	SM-ML	10	17.90	7.90	70	0.97	59.07	59.07	59.07	0.15	1.30	1.06	13.79	5.00	1.20	21.55	0.24	0.28	1.85	Non Liquefiable
4.8	SM-ML	28	17.90	7.90	64	0.96	85.92	85.92	85.92	0.15	1.08	1.06	32.02	5.00	1.20	43.42	NA	NA	>1	Non Liquefiable
6.3	SM-ML	31	18.70	8.70	58	0.95	113.97	113.97	113.97	0.15	0.94	1.06	30.78	5.00	1.20	41.94	NA	NA	>1	Non Liquefiable
7.80	SM	18	18.70	8.70	48	0.94	142.02	142.02	134.02	0.16	0.84	1.06	16.01	5.00	1.20	24.21	0.28	0.33	2.13	Non Liquefiable
9.30	SM-ML	13	18.70	8.70	87	0.93	170.07	170.07	147.07	0.17	0.77	1.06	10.57	5.00	1.20	17.68	0.19	0.22	1.34	Non Liquefiable
10.80	SM-ML	11	18.20	8.20	83	0.89	197.37	197.37	159.37	0.17	0.71	1.06	8.30	5.00	1.20	14.96	0.16	0.19	1.11	Non Liquefiable
12.30	SM-ML	18	18.20	8.20	91	0.85	224.67	214.67	171.67	0.17	0.66	1.06	12.54	5.00	1.20	20.05	0.22	0.26	1.49	Non Liquefiable
13.80	SM-ML	19	18.20	8.20	98	0.81	251.97	226.97	183.97	0.17	0.63	1.06	12.77	5.00	1.20	20.32	0.22	0.26	1.52	Non Liquefiable
15.30	SM-ML	24	18.20	8.20	82	0.77	279.27	239.27	196.27	0.17	0.61	1.06	15.58	5.00	1.20	23.69	0.27	0.32	1.88	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.00	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ Chainage	VUP @ 22+890	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 8	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	14.20						
Water Table Depth considered (m)	10.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{Field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_{cd}$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	CI	18	19.00	9.00	84	0.99	34.20	34.20	34.20	0.15	1.70	1.06	32.44	5.00	1.20	43.92	NA	NA	>1	Non Liquefiable
3.3	CI	27	19.00	9.00	89	0.97	62.70	62.70	62.70	0.15	1.26	1.06	36.14	5.00	1.20	48.37	NA	NA	>1	Non Liquefiable
4.8	CI	19	19.00	9.00	93	0.96	91.20	91.20	91.20	0.15	1.05	1.06	21.09	5.00	1.20	30.31	NA	NA	>1	Non Liquefiable
6.3	SM	32	19.00	9.00	30	0.95	119.70	119.70	119.70	0.15	0.91	1.06	31.00	4.71	1.15	40.49	NA	NA	>1	Non Liquefiable
7.80	SM	30	19.00	9.00	20	0.94	148.20	148.20	148.20	0.15	0.82	1.06	26.12	3.61	1.08	31.81	NA	NA	>1	Non Liquefiable
9.30	SM	28	18.80	8.80	27	0.93	176.40	176.40	176.40	0.14	0.75	1.06	22.35	4.48	1.13	29.74	0.45	0.54	3.72	Non Liquefiable
10.80	SM	29	18.80	8.80	30	0.89	204.60	204.60	196.60	0.14	0.68	1.06	20.83	4.71	1.15	28.76	0.40	0.48	3.31	Non Liquefiable
12.30	SM	32	18.80	8.80	20	0.85	232.80	232.80	209.80	0.15	0.62	1.06	21.15	3.61	1.08	26.45	0.32	0.39	2.64	Non Liquefiable
13.80	SM	34	18.80	8.80	27	0.81	261.00	261.00	223.00	0.15	0.58	1.06	20.81	4.48	1.13	28.00	0.37	0.44	3.00	Non Liquefiable
15.30	SM	51	18.80	8.80	26	0.77	289.20	278.20	236.20	0.15	0.55	1.06	29.87	4.39	1.12	37.92	NA	NA	>1	Non Liquefiable

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Project : Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.00	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ chainage	VUP @ 25+430	DesignPGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 9	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	12.25						
Water Table Depth considered (m)	8.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{Field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content ( % )	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	CI	8	18.50	8.50	95	0.99	33.30	33.30	33.30	0.15	1.70	1.06	14.42	5.00	1.20	22.30	0.25	0.29	1.91	Non Liquefiable
3.3	CI	17	18.50	8.50	99	0.97	61.05	61.05	61.05	0.15	1.28	1.06	23.06	5.00	1.20	32.68	NA	NA	>1	Non Liquefiable
4.8	CI	11	18.50	8.50	97	0.96	88.80	88.80	88.80	0.15	1.06	1.06	12.37	5.00	1.20	19.85	0.21	0.25	1.69	Non Liquefiable
6.3	SM-ML	21	18.60	8.60	87	0.95	116.70	116.70	116.70	0.15	0.93	1.06	20.61	5.00	1.20	29.73	0.45	0.54	3.61	Non Liquefiable
7.8	SM-ML	25	18.60	8.60	89	0.94	144.60	144.60	144.60	0.15	0.83	1.06	22.04	5.00	1.20	31.44	NA	NA	>1	Non Liquefiable
9.3	SM-ML	8	18.60	8.60	75	0.93	172.50	172.50	159.50	0.16	0.76	1.06	6.46	5.00	1.20	12.75	0.14	0.16	1.06	Non Liquefiable
10.8	SM-ML	12	18.60	8.60	96	0.89	200.40	200.40	172.40	0.16	0.69	1.06	8.73	5.00	1.20	15.48	0.16	0.20	1.22	Non Liquefiable
12.3	CL	18	18.60	8.60	87	0.85	228.30	227.80	185.30	0.16	0.63	1.06	12.07	5.00	1.20	19.48	0.21	0.25	1.53	Non Liquefiable
13.8	CL	19	19.40	9.40	98	0.81	257.40	241.90	199.40	0.16	0.61	1.06	12.24	5.00	1.20	19.69	0.21	0.25	1.56	Non Liquefiable
15.3	SM-ML	22	19.40	9.40	96	0.77	286.50	256.00	213.50	0.16	0.59	1.06	13.64	5.00	1.20	21.37	0.23	0.28	>1	Non Liquefiable

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**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ Chainage :	MNB @ 29+260	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 11	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	5.50						
Water Table Depth considered (m)	3.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	CH	6	18.00	8.00	80	0.99	32.80	32.80	32.80	0.15	1.70	1.06	10.81	5.00	1.20	17.97	0.19	0.23	1.48	Non Liquefiable
3.3	SM-ML	9	18.00	8.00	86	0.97	59.80	59.80	56.80	0.16	1.29	1.06	12.34	5.00	1.20	19.80	0.21	0.25	1.59	Non Liquefiable
4.8	SM-ML	11	18.00	8.00	77	0.96	86.80	86.80	68.80	0.19	1.07	1.06	12.52	5.00	1.20	20.02	0.22	0.26	1.36	Non Liquefiable
6.3	SM-ML	13	18.30	8.30	84	0.95	114.25	106.04	81.25	0.21	0.97	1.06	13.38	5.00	1.20	21.06	0.23	0.27	1.31	Non Liquefiable
7.80	SM-ML	18	18.30	8.30	83	0.94	141.70	118.49	93.70	0.22	0.92	1.06	17.53	5.00	1.20	26.03	0.31	0.37	1.69	Non Liquefiable
9.30	SM-ML	12	18.20	8.20	72	0.93	169.00	130.79	106.00	0.23	0.87	1.06	11.12	5.00	1.20	18.35	0.20	0.23	1.01	Non Liquefiable
10.80	SM-ML	13	18.20	8.20	93	0.89	196.30	143.09	118.30	0.23	0.84	1.06	11.52	5.00	1.20	18.82	0.20	0.24	1.05	Non Liquefiable
12.30	SM-ML	14	18.20	8.20	93	0.85	223.60	155.39	130.60	0.23	0.80	1.06	11.90	5.00	1.20	19.29	0.21	0.25	1.09	Non Liquefiable
13.80	SM-ML	17	18.20	8.20	94	0.81	250.90	167.69	142.90	0.22	0.77	1.06	13.92	5.00	1.20	21.70	0.24	0.28	1.29	Non Liquefiable
15.30	SM-ML	13	18.20	8.20	97	0.77	278.20	179.99	155.20	0.21	0.75	1.06	10.27	5.00	1.20	17.33	0.18	0.22	1.03	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018



## Computation Sheet

**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7	Efficiency in SPT Boring (for $C_E$ factor) "%"	60		
Structure @ Chainage :	FLYOVER @ 32+170	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 12	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	13.20						
Water Table Depth considered (m)	9.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM-ML	18	18.20	8.20	76	0.99	32.76	32.76	32.76	0.15	1.70	1.06	32.44	5.00	1.20	43.92	NA	NA	>1	Non Liquefiable
3.3	SM	9	18.20	8.20	27	0.97	60.06	60.06	60.06	0.15	1.29	1.06	12.31	4.48	1.13	18.39	0.20	0.23	1.54	Non Liquefiable
4.8	CI	19	18.20	8.20	64	0.96	87.36	87.36	87.36	0.15	1.07	1.06	21.55	5.00	1.20	30.86	NA	NA	>1	Non Liquefiable
6.3	CI	23	18.50	8.50	98	0.95	115.11	115.11	115.11	0.15	0.93	1.06	22.72	5.00	1.20	32.27	NA	NA	>1	Non Liquefiable
7.80	CI	28	18.50	8.50	96	0.94	142.86	142.86	142.86	0.15	0.84	1.06	24.83	5.00	1.20	34.80	NA	NA	>1	Non Liquefiable
9.30	CI	29	18.80	8.80	98	0.93	171.06	171.06	167.70	0.15	0.76	1.06	23.50	5.00	1.20	33.20	NA	NA	>1	Non Liquefiable
10.80	CI	22	18.80	8.80	81	0.89	199.26	199.26	180.90	0.15	0.71	1.06	16.52	5.00	1.20	24.82	0.29	0.34	2.26	Non Liquefiable
12.30	SM	25	18.80	8.80	44	0.85	227.46	227.46	194.10	0.15	0.63	1.06	16.78	5.00	1.20	25.13	NA	NA	>1	Non Liquefiable
13.80	SM	30	18.80	8.80	34	0.81	255.66	249.66	207.30	0.15	0.60	1.06	18.93	4.93	1.19	27.42	0.35	0.42	2.70	Non Liquefiable
15.30	CH	29	18.80	8.80	89	0.77	283.86	262.86	220.50	0.15	0.57	1.06	17.66	5.00	1.20	26.20	0.32	0.38	2.47	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.0	Efficiency in SPT Boring (for $C_E$ factor) "%":	60		
Structure @ Chainage	MJB @ 33+420	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 13	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	2.10						
Water Table Depth considered (m)	0.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{Field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at site, $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM	2	17.30	7.30	3	0.99	31.14	31.14	13.14	0.36	1.70	1.06	3.60	0.00	1.00	3.60	0.06	0.07	0.20	Liquefiable
3.3	CI-CH	3	17.30	7.30	91	0.97	57.09	45.09	24.09	0.36	1.49	1.06	4.74	5.00	1.20	10.68	0.12	0.14	0.39	Liquefiable
4.8	CI-CH	4	17.30	7.30	93	0.96	83.04	56.04	35.04	0.36	1.34	1.06	5.66	5.00	1.20	11.80	0.13	0.15	0.43	Liquefiable
6.3	CI-CH	2	17.40	7.40	90	0.95	109.14	67.14	46.14	0.35	1.22	1.06	2.59	5.00	1.20	8.10	0.10	0.12	0.33	Liquefiable
7.80	CI-CH	2	17.40	7.40	95	0.94	135.24	78.24	57.24	0.35	1.13	1.06	2.40	5.00	1.20	7.88	0.09	0.11	0.33	Liquefiable
9.30	SM	3	17.40	7.40	16	0.93	161.34	89.34	68.34	0.34	1.06	1.06	3.36	2.77	1.05	6.31	0.08	0.10	0.29	Liquefiable
10.80	SM	5	17.40	7.40	9	0.89	187.44	100.44	79.44	0.33	1.00	1.06	5.29	0.56	1.02	5.94	0.08	0.09	0.29	Liquefiable
12.30	SM	7	17.40	7.40	7	0.85	213.54	111.54	90.54	0.31	0.95	1.06	7.03	0.12	1.01	7.21	0.09	0.11	0.34	Liquefiable
13.80	SM	18	17.40	7.40	17	0.81	239.64	122.64	101.64	0.30	0.90	1.06	17.23	3.01	1.06	21.28	0.23	0.28	0.93	Liquefiable
15.30	CL-CI	34	17.40	7.40	83	0.77	265.74	133.74	112.74	0.28	0.86	1.06	31.16	5.00	1.20	42.40	NA	NA	>1	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



Project : Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.00	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ Chainage	MJB @ 33+490	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 14	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	3.20						
Water Table Depth considered (m)	0.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{Field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_{cd}$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60CS</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM	5	17.50	7.50	26	0.99	31.50	31.50	13.50	0.36	1.70	1.06	9.01	4.39	1.12	14.50	0.16	0.18	0.52	Liquefiable
3.3	SM	8	17.50	7.50	15	0.97	57.75	56.75	24.75	0.35	1.33	1.06	11.26	2.50	1.05	14.30	0.15	0.18	0.51	Liquefiable
4.8	CH	11	17.50	7.50	98	0.96	84.00	68.00	36.00	0.35	1.21	1.06	14.14	5.00	1.20	21.97	0.24	0.29	0.82	Liquefiable
6.3	CH	18	18.40	8.40	96	0.95	111.60	80.60	48.60	0.34	1.11	1.06	21.25	5.00	1.20	30.50	NA	NA	>1	Non Liquefiable
7.80	CH	13	18.40	8.40	96	0.94	139.20	93.20	61.20	0.33	1.04	1.06	14.27	5.00	1.20	22.13	0.24	0.29	0.87	Liquefiable
9.30	CH	17	18.60	8.60	98	0.93	167.10	106.10	74.10	0.33	0.97	1.06	17.49	5.00	1.20	25.99	0.31	0.37	1.15	Non Liquefiable
10.80	SM	22	18.60	8.60	11	0.89	195.00	119.00	87.00	0.31	0.92	1.06	21.38	1.21	1.03	23.15	0.26	0.31	1.00	Non Liquefiable
12.30	SM	27	18.60	8.60	20	0.85	222.90	131.90	99.90	0.29	0.87	1.06	24.92	3.61	1.08	30.51	NA	NA	>1	Non Liquefiable
13.80	SM	24	18.60	8.60	18	0.81	250.80	144.80	112.80	0.28	0.83	1.06	21.14	3.23	1.07	25.78	0.31	0.37	1.32	Non Liquefiable
15.30	SM	38	18.60	8.60	12	0.77	278.70	157.70	125.70	0.26	0.80	1.06	32.08	1.55	1.03	34.64	NA	NA	>1	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



Project : Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.00	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ chainage	MJB @ 35+860	DesignPGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 15	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	5.30						
Water Table Depth considered (m)	1.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{Field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content ( % )	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM	7	18.30	8.30	21	0.99	32.94	32.94	24.94	0.20	1.70	1.06	12.61	3.78	1.09	17.48	0.19	0.22	1.09	Non Liquefiable
3.3	SM	9	18.30	8.30	12	0.97	60.39	60.39	37.39	0.25	1.29	1.06	12.28	1.55	1.03	14.22	0.15	0.18	0.74	Liquefiable
4.8	SM	19	18.30	8.30	15	0.96	87.84	87.84	49.84	0.26	1.07	1.06	21.49	2.50	1.05	25.02	0.29	0.35	1.32	Non Liquefiable
6.3	SM	22	18.50	8.50	99	0.95	115.59	105.49	62.59	0.27	0.97	1.06	22.71	5.00	1.20	32.25	NA	NA	>1	Non Liquefiable
7.8	CI-CH	12	18.50	8.50	98	0.94	143.34	118.24	75.34	0.28	0.92	1.06	11.70	5.00	1.20	19.04	0.20	0.24	0.87	Liquefiable
9.3	CI-CH	29	18.60	8.60	94	0.93	171.24	131.14	88.24	0.28	0.87	1.06	26.84	5.00	1.20	37.21	NA	NA	>1	Non Liquefiable
10.8	CI-CH	16	18.60	8.60	98	0.89	199.14	144.04	101.14	0.27	0.83	1.06	14.13	5.00	1.20	21.96	0.24	0.29	1.06	Non Liquefiable
12.3	CI-CH	21	18.60	8.60	98	0.85	227.04	156.94	114.04	0.26	0.80	1.06	17.77	5.00	1.20	26.32	0.32	0.38	1.46	Non Liquefiable
13.8	SM	29	18.60	8.60	41	0.81	254.94	169.84	126.94	0.25	0.77	1.06	23.59	5.00	1.20	33.31	NA	NA	>1	Non Liquefiable
15.3	SM-ML	16	18.60	8.60	86	0.77	282.84	182.74	139.84	0.24	0.74	1.06	12.55	5.00	1.20	20.06	0.22	0.26	>1	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



Project : Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ Chainage	MNB @ 38+010	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 16	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	8.75						
Water Table Depth considered (m)	4.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{Field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content ( % )	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at site, $kN/m^2$	Effective overburden ( $s_o$ ) at considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM-ML	10	18.30	8.30	50	0.99	32.94	32.94	32.94	0.15	1.70	1.06	18.02	5.00	1.20	26.62	0.33	0.39	2.55	Non Liquefiable
3.3	SM-ML	4	18.30	8.30	60	0.97	60.39	60.39	60.39	0.15	1.29	1.06	5.46	5.00	1.20	11.55	0.13	0.15	1.00	Liquefiable
4.8	SM-ML	8	18.30	8.30	81	0.96	87.84	87.84	79.84	0.17	1.07	1.06	9.05	5.00	1.20	15.86	0.17	0.20	1.22	Non Liquefiable
6.3	SM-ML	4	18.30	8.30	91	0.95	115.29	100.29	92.29	0.19	1.00	1.06	4.23	5.00	1.20	10.08	0.11	0.14	0.73	Liquefiable
7.80	CI-CH	7	18.30	8.30	96	0.94	142.74	112.74	104.74	0.20	0.94	1.06	6.99	5.00	1.20	13.39	0.14	0.17	0.86	Liquefiable
9.30	CI-CH	13	18.60	8.60	97	0.93	170.64	164.53	117.64	0.21	0.78	1.06	10.74	5.00	1.20	17.89	0.19	0.23	1.09	Non Liquefiable
10.80	CI-CH	18	18.60	8.60	98	0.89	198.54	177.43	130.54	0.21	0.75	1.06	14.32	5.00	1.20	22.19	0.24	0.29	1.39	Non Liquefiable
12.30	CI-CH	15	18.60	8.60	98	0.85	226.44	190.33	143.44	0.21	0.72	1.06	11.53	5.00	1.20	18.83	0.20	0.24	1.15	Non Liquefiable
13.80	CI-CH	14	18.60	8.60	96	0.81	254.34	203.23	156.34	0.20	0.68	1.06	10.10	5.00	1.20	17.12	0.18	0.22	1.06	Non Liquefiable
15.30	CI-CH	17	19.80	9.80	98	0.77	284.04	217.93	171.04	0.20	0.65	1.06	11.73	5.00	1.20	19.08	0.20	0.24	1.23	Non Liquefiable

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## Computation Sheet



**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ Chainage :	MJB @ 39+510	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 17	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	4.50						
Water Table Depth considered (m)	0.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM-ML	5	17.50	7.50	99	0.99	32.30	32.30	14.30	0.35	1.70	1.06	9.01	5.00	1.20	15.81	0.17	0.20	0.58	Liquefiable
3.3	SM-ML	9	17.50	7.50	99	0.97	58.55	58.55	25.55	0.35	1.31	1.06	12.47	5.00	1.20	19.96	0.21	0.26	0.74	Liquefiable
4.8	SM-ML	7	17.50	7.50	90	0.96	84.80	81.80	36.80	0.35	1.11	1.06	8.20	5.00	1.20	14.84	0.16	0.19	0.55	Liquefiable
6.3	SM-ML	9	17.50	7.50	96	0.95	111.05	93.05	48.05	0.34	1.04	1.06	9.89	5.00	1.20	16.87	0.18	0.21	0.62	Liquefiable
7.80	SM-ML	11	17.50	7.50	99	0.94	137.30	104.30	59.30	0.34	0.98	1.06	11.42	5.00	1.20	18.70	0.20	0.24	0.70	Liquefiable
9.30	SM-ML	10	17.60	7.60	98	0.93	163.70	115.70	70.70	0.33	0.93	1.06	9.85	5.00	1.20	16.83	0.18	0.21	0.64	Liquefiable
10.80	SM-ML	14	17.60	7.60	95	0.89	190.10	127.10	82.10	0.32	0.89	1.06	13.16	5.00	1.20	20.80	0.23	0.27	0.84	Liquefiable
12.30	SM-ML	17	17.60	7.60	95	0.85	216.50	138.50	93.50	0.31	0.85	1.06	15.31	5.00	1.20	23.37	0.26	0.31	1.03	Non Liquefiable
13.80	SM	29	17.60	7.60	38	0.81	242.90	149.90	104.90	0.29	0.82	1.06	25.11	5.00	1.20	35.13	NA	NA	>1	Non Liquefiable
15.30	SM	33	17.60	7.60	46	0.77	269.30	161.30	116.30	0.28	0.79	1.06	27.54	5.00	1.20	38.05	NA	NA	>1	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018



## Computation Sheet

**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7	Efficiency in SPT Boring (for $C_E$ factor) "%":	60		
Structure @ Chainage :	MJB @ 39+690	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 18	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	4.50						
Water Table Depth considered (m)	0.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	CI	6	18.20	8.20	93	0.99	32.76	32.76	14.76	0.34	1.70	1.06	10.81	5.00	1.20	17.97	0.19	0.23	0.67	Liquefiable
3.3	CI	10	18.20	8.20	97	0.97	60.06	60.06	27.06	0.34	1.29	1.06	13.68	5.00	1.20	21.41	0.23	0.28	0.83	Liquefiable
4.8	CI	13	18.20	8.20	92	0.96	87.36	84.36	39.36	0.33	1.09	1.06	15.00	5.00	1.20	23.00	0.26	0.31	0.92	Liquefiable
6.3	SM-ML	15	18.20	8.20	75	0.95	114.66	96.66	51.66	0.33	1.02	1.06	16.17	5.00	1.20	24.41	0.28	0.33	1.02	Non Liquefiable
7.80	SM-ML	23	18.20	8.20	72	0.94	141.96	108.96	63.96	0.33	0.96	1.06	23.36	5.00	1.20	33.03	NA	NA	>1	Non Liquefiable
9.30	SM	27	18.30	8.30	46	0.93	169.41	121.41	76.41	0.32	0.91	1.06	25.97	5.00	1.20	36.17	NA	NA	>1	Non Liquefiable
10.80	SM	24	18.30	8.30	31	0.89	196.86	133.86	88.86	0.31	0.86	1.06	21.99	4.77	1.16	30.33	NA	NA	>1	Non Liquefiable
12.30	SM	31	18.30	8.30	26	0.85	224.31	146.31	101.31	0.29	0.83	1.06	27.17	4.39	1.12	34.88	NA	NA	>1	Non Liquefiable
13.80	SM	24	20.30	10.30	26	0.81	254.76	161.76	116.76	0.27	0.79	1.06	20.00	4.39	1.12	26.84	0.33	0.40	1.45	Non Liquefiable
15.30	SM-ML	17	20.30	10.30	55	0.77	285.21	177.21	132.21	0.26	0.75	1.06	13.54	5.00	1.20	21.24	0.23	0.28	1.07	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.0	Efficiency in SPT Boring (for $C_E$ factor) "%":	60		
Structure @ Chainage	VUP @ 40+940	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 19	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	11.80						
Water Table Depth considered (m)	7.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{Field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at site, $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	CI	7	17.80	7.80	86	0.99	32.04	32.04	32.04	0.15	1.70	1.06	12.61	5.00	1.20	20.14	0.22	0.26	1.68	Non Liquefiable
3.3	CI	7	17.80	7.80	91	0.97	58.74	58.74	58.74	0.15	1.30	1.06	9.68	5.00	1.20	16.62	0.18	0.21	1.39	Non Liquefiable
4.8	CI	9	17.80	7.80	89	0.96	85.44	85.44	85.44	0.15	1.08	1.06	10.32	5.00	1.20	17.39	0.19	0.22	1.47	Non Liquefiable
6.3	CI	11	18.20	8.20	92	0.95	112.74	112.74	112.74	0.15	0.94	1.06	10.98	5.00	1.20	18.18	0.19	0.23	1.56	Non Liquefiable
7.80	CI	24	18.20	8.20	89	0.94	140.04	140.04	132.04	0.16	0.85	1.06	21.50	5.00	1.20	30.80	NA	NA	>1	Non Liquefiable
9.30	SM-ML	40	19.10	9.10	60	0.93	168.69	168.69	145.69	0.17	0.77	1.06	32.65	5.00	1.20	44.17	NA	NA	>1	Non Liquefiable
10.80	SM	37	19.10	9.10	42	0.89	197.34	197.34	159.34	0.17	0.71	1.06	27.92	5.00	1.20	38.50	NA	NA	>1	Non Liquefiable
12.30	SM	31	19.10	9.10	36	0.85	225.99	220.99	172.99	0.17	0.65	1.06	21.20	5.00	1.20	30.44	NA	NA	>1	Non Liquefiable
13.80	SM	35	19.10	9.10	18	0.81	254.64	234.64	186.64	0.17	0.62	1.06	23.01	3.23	1.07	27.78	0.36	0.43	2.52	Non Liquefiable
15.30	SM	36	19.10	9.10	35	0.77	283.29	248.29	200.29	0.17	0.60	1.06	22.80	5.00	1.20	32.35	NA	NA	>1	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.00	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ Chainage	MJB @ 42+550	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 20	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	3.35						
Water Table Depth considered (m)	0.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{Field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_{cd}$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60CS</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM	7	18.10	8.10	17	0.99	32.58	32.58	14.58	0.34	1.70	1.06	12.61	3.01	1.06	16.38	0.17	0.21	0.60	Liquefiable
3.3	SM	10	18.10	8.10	24	0.97	59.73	59.73	26.73	0.34	1.29	1.06	13.72	4.18	1.11	19.37	0.21	0.25	0.73	Liquefiable
4.8	SM	12	18.10	8.10	12	0.96	86.88	72.38	38.88	0.34	1.18	1.06	14.95	1.55	1.03	16.98	0.18	0.22	0.64	Liquefiable
6.3	SM-ML	12	18.40	8.40	92	0.95	114.48	84.98	51.48	0.33	1.08	1.06	13.80	5.00	1.20	21.56	0.24	0.28	0.85	Liquefiable
7.80	SM-ML	14	18.40	8.40	87	0.94	142.08	97.58	64.08	0.33	1.01	1.06	15.02	5.00	1.20	23.03	0.26	0.31	0.94	Liquefiable
9.30	SM-ML	23	18.40	8.40	66	0.93	169.68	110.18	76.68	0.32	0.95	1.06	23.23	5.00	1.20	32.87	NA	NA	>1	Non Liquefiable
10.80	SM-ML	21	18.60	8.60	78	0.89	197.58	123.08	89.58	0.30	0.90	1.06	20.06	5.00	1.20	29.08	0.41	0.49	1.62	Non Liquefiable
12.30	SM	27	18.60	8.60	32	0.85	225.48	135.98	102.48	0.29	0.86	1.06	24.54	4.83	1.17	33.57	NA	NA	>1	Non Liquefiable
13.80	SM	25	18.60	8.60	27	0.81	253.38	148.88	115.38	0.28	0.82	1.06	21.72	4.48	1.13	29.03	0.41	0.49	1.78	Non Liquefiable
15.30	SM	32	18.60	8.60	16	0.77	281.28	161.78	128.28	0.26	0.79	1.06	26.67	2.77	1.05	30.88	NA	NA	>1	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



Project : Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.00	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ chainage	FLYOVER @ 43+910	DesignPGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 21	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	10.25						
Water Table Depth considered (m)	6.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM-ML	6	18.10	8.10	82	0.99	32.58	32.58	32.58	0.15	1.70	1.06	10.81	5.00	1.20	17.97	0.19	0.23	1.48	Non Liquefiable
3.3	SM-ML	7	18.10	8.10	84	0.97	59.73	59.73	59.73	0.15	1.29	1.06	9.60	5.00	1.20	16.52	0.18	0.21	1.38	Non Liquefiable
4.8	SM-ML	7	18.10	8.10	96	0.96	86.88	86.88	86.88	0.15	1.07	1.06	7.96	5.00	1.20	14.55	0.16	0.19	1.24	Non Liquefiable
6.3	CI	10	18.30	8.30	95	0.95	114.33	114.33	111.09	0.15	0.94	1.06	9.91	5.00	1.20	16.90	0.18	0.21	1.40	Non Liquefiable
7.8	CI	11	18.30	8.30	93	0.94	141.78	141.78	123.54	0.17	0.84	1.06	9.79	5.00	1.20	16.75	0.18	0.21	1.26	Non Liquefiable
9.3	SM-ML	21	18.30	8.30	91	0.93	169.23	169.23	135.99	0.18	0.77	1.06	17.11	5.00	1.20	25.53	0.30	0.36	2.01	Non Liquefiable
10.8	SM	20	18.60	8.60	45	0.89	197.13	191.35	148.89	0.18	0.72	1.06	15.33	5.00	1.20	23.39	0.26	0.31	1.72	Non Liquefiable
12.3	SM	29	18.60	8.60	33	0.85	225.03	204.25	161.79	0.18	0.68	1.06	20.86	4.88	1.18	29.48	0.44	0.52	2.83	Non Liquefiable
13.8	SM-ML	25	18.60	8.60	51	0.81	252.93	217.15	174.69	0.18	0.65	1.06	17.29	5.00	1.20	25.75	0.31	0.37	2.02	Non Liquefiable
15.3	CI	20	18.60	8.60	84	0.77	280.83	230.05	187.59	0.18	0.63	1.06	13.32	5.00	1.20	20.99	0.23	0.27	>1	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



Project : Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ Chainage	MJB @ 47+950	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 22	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	3.80						
Water Table Depth considered (m)	0.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{Field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content ( % )	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at site, $kN/m^2$	Effective overburden ( $s_o$ ) at considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM-ML	15	18.30	8.30	65	0.99	32.94	32.94	14.94	0.34	1.70	1.06	27.03	5.00	1.20	37.44	NA	NA	>1	Non Liquefiable
3.3	SM	24	18.30	8.30	20	0.97	60.39	60.39	27.39	0.34	1.29	1.06	32.74	3.61	1.08	38.95	NA	NA	>1	Non Liquefiable
4.8	SM-ML	10	18.30	8.30	84	0.96	87.84	87.84	39.84	0.33	1.07	1.06	11.31	5.00	1.20	18.57	0.20	0.24	0.71	Liquefiable
6.3	CI-CH	13	18.30	8.30	97	0.95	115.29	115.29	52.29	0.33	0.93	1.06	12.83	5.00	1.20	20.40	0.22	0.26	0.80	Liquefiable
7.80	CI-CH	16	18.30	8.30	92	0.94	142.74	142.74	64.74	0.32	0.84	1.06	14.20	5.00	1.20	22.03	0.24	0.29	0.89	Liquefiable
9.30	SM-ML	20	18.60	8.60	93	0.93	170.64	170.64	77.64	0.32	0.77	1.06	16.23	5.00	1.20	24.47	0.28	0.34	1.06	Non Liquefiable
10.80	SM-ML	19	18.60	8.60	95	0.89	198.54	183.54	90.54	0.30	0.74	1.06	14.87	5.00	1.20	22.84	0.25	0.30	1.00	Non Liquefiable
12.30	SM-ML	16	18.60	8.60	96	0.85	226.44	196.44	103.44	0.29	0.71	1.06	12.10	5.00	1.20	19.52	0.21	0.25	0.87	Liquefiable
13.80	SM-ML	18	18.60	8.60	98	0.81	254.34	209.34	116.34	0.27	0.67	1.06	12.75	5.00	1.20	20.29	0.22	0.26	0.95	Liquefiable
15.30	SM-ML	27	19.80	9.80	95	0.77	284.04	224.04	131.04	0.26	0.64	1.06	18.30	5.00	1.20	26.96	0.34	0.40	1.55	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7	Efficiency in SPT Boring (for $C_E$ factor) %	60		
Structure @ Chainage :	FLYOVER @ 49+900	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 23	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	9.80						
Water Table Depth considered (m)	5.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM-ML	11	17.50	7.50	99	0.99	32.30	32.30	32.30	0.15	1.70	1.06	19.82	5.00	1.20	28.79	0.40	0.48	3.10	Non Liquefiable
3.3	CI	6	17.50	7.50	99	0.97	58.55	58.55	58.55	0.15	1.31	1.06	8.31	5.00	1.20	14.97	0.16	0.19	1.25	Non Liquefiable
4.8	CI	10	17.50	7.50	90	0.96	84.80	84.80	84.80	0.15	1.09	1.06	11.51	5.00	1.20	18.81	0.20	0.24	1.60	Non Liquefiable
6.3	SM	12	17.50	7.50	96	0.95	111.05	111.05	98.05	0.17	0.95	1.06	12.07	5.00	1.20	19.48	0.21	0.25	1.48	Non Liquefiable
7.80	SM	18	17.50	7.50	99	0.94	137.30	137.30	109.30	0.18	0.85	1.06	16.28	5.00	1.20	24.54	0.28	0.34	1.83	Non Liquefiable
9.30	SM	21	17.60	7.60	98	0.93	163.70	163.70	120.70	0.20	0.78	1.06	17.40	5.00	1.20	25.88	0.31	0.37	1.89	Non Liquefiable
10.80	SM	20	17.60	7.60	95	0.89	190.10	180.10	132.10	0.20	0.75	1.06	15.80	5.00	1.20	23.96	0.27	0.33	1.64	Non Liquefiable
12.30	SM	31	17.60	7.60	95	0.85	216.50	191.50	143.50	0.20	0.72	1.06	23.75	5.00	1.20	33.49	NA	NA	>1	Non Liquefiable
13.80	SM	28	17.60	7.60	38	0.81	242.90	202.90	154.90	0.20	0.68	1.06	20.22	5.00	1.20	29.27	0.42	0.51	2.56	Non Liquefiable
15.30	SM	32	17.60	7.60	46	0.77	269.30	214.30	166.30	0.19	0.66	1.06	22.32	5.00	1.20	31.79	NA	NA	>1	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018



## Computation Sheet

**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7	Efficiency in SPT Boring (for $C_E$ factor) "%":	60		
Structure @ Chainage :	MJB @ 39+690	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 18	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	4.50						
Water Table Depth considered (m)	0.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	CI	6	18.20	8.20	93	0.99	32.76	32.76	14.76	0.34	1.70	1.06	10.81	5.00	1.20	17.97	0.19	0.23	0.67	Liquefiable
3.3	CI	10	18.20	8.20	97	0.97	60.06	60.06	27.06	0.34	1.29	1.06	13.68	5.00	1.20	21.41	0.23	0.28	0.83	Liquefiable
4.8	CI	13	18.20	8.20	92	0.96	87.36	84.36	39.36	0.33	1.09	1.06	15.00	5.00	1.20	23.00	0.26	0.31	0.92	Liquefiable
6.3	SM-ML	15	18.20	8.20	75	0.95	114.66	96.66	51.66	0.33	1.02	1.06	16.17	5.00	1.20	24.41	0.28	0.33	1.02	Non Liquefiable
7.80	SM-ML	23	18.20	8.20	72	0.94	141.96	108.96	63.96	0.33	0.96	1.06	23.36	5.00	1.20	33.03	NA	NA	>1	Non Liquefiable
9.30	SM	27	18.30	8.30	46	0.93	169.41	121.41	76.41	0.32	0.91	1.06	25.97	5.00	1.20	36.17	NA	NA	>1	Non Liquefiable
10.80	SM	24	18.30	8.30	31	0.89	196.86	133.86	88.86	0.31	0.86	1.06	21.99	4.77	1.16	30.33	NA	NA	>1	Non Liquefiable
12.30	SM	31	18.30	8.30	26	0.85	224.31	146.31	101.31	0.29	0.83	1.06	27.17	4.39	1.12	34.88	NA	NA	>1	Non Liquefiable
13.80	SM	24	20.30	10.30	26	0.81	254.76	161.76	116.76	0.27	0.79	1.06	20.00	4.39	1.12	26.84	0.33	0.40	1.45	Non Liquefiable
15.30	SM-ML	17	20.30	10.30	55	0.77	285.21	177.21	132.21	0.26	0.75	1.06	13.54	5.00	1.20	21.24	0.23	0.28	1.07	Non Liquefiable

# Borelogs and Figures

# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

Flyover @ CH 0+800

Date of start : 20/03/2021

BH :1

Depth : 30.00m

Depth of Water table : 4.50 m

Date of finish : 22/03/2021

Project No. 2152



Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc			
				Observed	Corrected	Gravel	Sand	Silt/Clay	r (wet)	r (dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)				
				*—	*—																
	0.00			0	20	40	60	80	100	0	20	40	60	80	100						
	1.80	SPT	Sandy Silt with Gravel (SM-ML)	10	13	1	5	94	1.79	1.50	18.94	Non	Plastic	2.65	DST	0.14	25				
	2.50	UDS																			
	3.30	SPT		5	5	0	57	43				Non	Plastic								
	4.80	SPT	Silty Sand with Gravel (SM)	8	8	0	68	32	1.74	1.43	21.32	Non	Plastic		DST		25				
	5.50	UDS																			
	6.30	SPT			11	11	0	63	37				Non	Plastic							
	7.80	SPT			13	12	0	71	29				Non	Plastic							
	9.30	SPT			17	15	0	76	24				Non	Plastic							
	10.80	SPT			21	17	1	69	30				Non	Plastic							
	12.30	SPT			23	17	0	73	27				Non	Plastic							
	13.80	SPT			28	19	0	81	19				Non	Plastic							
	15.30	SPT		Silty Clay of Medium Plasticity (CI)	12	12	1	10	89												
	16.80	SPT				10	10	0	5	95				41				23			
	18.30	SPT	Sandy Silt with Gravel (SM-ML)	18	14	0	2	98				Non	Plastic								
	19.80	SPT			21	15	2	7	91				Non	Plastic							
	21.30	SPT	Silty Sand with Gravel (SM)	26	17	1	78	21				Non	Plastic								
	22.80	SPT			33	19	1	60	39				Non	Plastic							
	24.30	SPT	Sandy Silt with Gravel (SM-ML)	46	23	0	46	54				Non	Plastic								
	25.80	SPT			51	25	0	51	49				Non	Plastic							
	27.30	SPT	Silty Sand with Gravel (SM)	57	26	0	79	21				Non	Plastic								
	28.80	SPT			61	27	1	87	12				Non	Plastic							
	30.30	SPT			71	30	0	86	14				Non	Plastic							

# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

MJB @ CH 1+530  
BH : 2  
Depth : 30.00m  
Depth of Water table : 2.70 m

Date of start : 21/03/2021

Date of finish : 23/03/2021



Project No. 2152

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc				
				Observed	Corrected	Gravel	Sand	Silt/Clay	r (wet)	r (dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)					
				✱	✱																	
	0.00																					
	1.00																					
	1.80	SPT	Silty Sand with Gravel (SM)	2.00	✱ 5	✱ 6	0	71	29	2.50	2.09	19.86	Non Plastic	2.62	DST	0.12	28					
	2.50	UDS		3.00	✱ 6	✱ 7	0	67	33				Non Plastic									
	3.30	SPT		4.00	✱ 10	✱ 11	0	40	60	5.50	4.56	20.58	Non Plastic									
	4.80	SPT	Sandy Silt with Gravel (SM-ML)	5.00	✱ 13	✱ 14	0	67	33				Non Plastic	2.62	DST	0.12	29					
	5.50	UDS		6.00	✱ 15	✱ 15	0	54	46	8.50	7.10	19.79	Non Plastic									
	6.30	SPT		7.00	✱ 23	✱ 18	0	69	31				Non Plastic									
	7.80	SPT	Silty Sand with Gravel (SM)	8.00	✱ 33	✱ 23	0	61	39				Non Plastic	2.71	UU	1.18	4					
	8.50	UDS		9.00	✱ 27	✱ 20	0	64	36				Non Plastic									
	9.30	SPT		10.00	✱ 17	✱ 14	0	2	98	14.50	12.16	19.25	Non Plastic									
	10.80	SPT	Silty Clay of Low to Medium Plasticity (CL-CI)	11.00	✱ 21	✱ 21	0	1	99				Non Plastic	2.71	UU	1.18	4					
	12.30	SPT		12.00	✱ 24	✱ 24	2	7	91				38 21									
	13.80	SPT		13.00	✱ 22	✱ 22	0	1	99				44 27									
	14.50	SPT	Silty Sand with Gravel (SM)	14.00	✱ 27	✱ 27	0	5	95				Non Plastic	2.71	UU	1.18	4					
	15.30	SPT		15.00	✱ 33	✱ 20	1	82	17				Non Plastic									
	16.80	SPT		16.00	✱ 38	✱ 21	1	68	31				Non Plastic									
	18.30	SPT	Silty Sand with Gravel (SM)	17.00	✱ 43	✱ 23	1	74	25				Non Plastic	2.71	UU	1.18	4					
	19.80	SPT		18.00	✱ 53	✱ 26	1	68	31				Non Plastic									
	21.30	SPT		19.00	✱ 48	✱ 24	1	75	24				Non Plastic									
	22.80	SPT	Silty Sand with Gravel (SM)	20.00	✱ 58	✱ 27	1	80	19				Non Plastic	2.71	UU	1.18	4					
	24.30	SPT		21.00	✱ 67	✱ 29	0	69	31				Non Plastic									
	25.80	SPT		22.00									Non Plastic									
	27.30	SPT		23.00								Non Plastic										
	28.80	SPT		24.00								Non Plastic										
	30.30	SPT		25.00								Non Plastic										

# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

VUP @ CH 6+380

BH :3

Depth : 20.00m

Depth of Water table : 13.80 m

Date of start : 24/03/2021

Date of finish : 25/03/2021



Project No. 2152

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc
				Observed *—	Corrected *—	Gravel	Sand	Silt/Clay	r(wet)	r(dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)	
	0.00																	
	1.80	SPT	Sandy Silt with Gravel (SM-ML)	12	16	0	5	95				Non Plastic						
	2.50	UDS								1.82	1.67	9.19				DST	0.14	29
	3.30	SPT			9	10	0	14	86				Non Plastic					
	4.80	SPT			13	13	0	8	92				Non Plastic					
	5.50	UDS							1.85	1.68	10.34			2.61	DST	0.14	30	
	6.30	SPT	Silty Sand with Gravel (SM)	15	14	0	86	14				Non Plastic						
	7.80	SPT			19	16	0	71	29				Non Plastic					
	8.50	UDS								1.87	1.66	12.86			2.65	DST		32
	9.30	SPT			24	19	0	71	29				Non Plastic					
	10.80	SPT			31	24	1	77	22				Non Plastic					
	12.30	SPT			27	19	0	72	28				Non Plastic					
	13.80	SPT			35	24	0	72	28				Non Plastic					
	15.30	SPT			52	25	1	57	42				Non Plastic					
	16.80	SPT		47	23	0	72	28				Non Plastic						
	18.30	SPT		57	26	0	69	31				Non Plastic						
	20.30	SPT		61	26	0	75	25				Non Plastic						



# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

VUP @ CH 16+690

BH :6

Depth : 20.00m

Depth of Water table : 13.30 m

Date of start : 28/03/2021

Date of finish : 30/03/2021



**Project No. 2152**

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc
				Observed	Corrected	Gravel	Sand	Silt/Clay	r (wet)	r (dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)	
				*	*													
	0.00																	
	1.80	SPT	Silty Clay of Medium Plasticity (CI)	11	11	0	14	86				47	23	2.74	UU	0.61	9	
	2.50	UDS							1.84	1.63	12.86							
	3.30	SPT		19	19	0	7	93										
	4.80	SPT	Sandy Silt with Gravel (SM-ML)	15	15	0	5	95				Non Plastic		2.61	DST	0.14	30	
	5.50	UDS							1.86	1.62	14.51							
	6.30	SPT	Silty Sand with Gravel (SM)	24	23	0	68	32				Non Plastic						
	7.80	SPT		15	13	0	69	31				Non Plastic						
	9.30	SPT		25	20	0	65	35				Non Plastic						
	10.80	SPT	Silty Clay of Medium Plasticity (CI)	29	29	0	3	97				43	22					
	12.30	SPT																
	13.80	SPT		32	32	0	3	97										
	15.30	SPT	Silty Sand with Gravel (SM)	34	34	0	4	96				44	23					
	16.80	SPT																
	18.30	SPT		38	20	1	79	20				Non Plastic						
	20.30	SPT		44	22	1	75	24				Non Plastic						
	17.00	SPT																
	18.00	SPT																
	19.00	SPT																
	20.00	SPT																
	20.30	SPT				0	72	28				Non Plastic						

# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

MNB @ CH 21+810  
BH :7  
Depth : 20.00m  
Depth of Water table : 11.30 m

Date of start : 31/03/2021

Date of finish : 01/04/2021



Project No. 2152

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc
				Observed	Corrected	Gravel	Sand	Silt/Clay	r(wet)	r(dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)	
				—*	—*													
	0.00																	
	1.80	SPT	Sandy Silt with Gravel (SM-ML)	6	8	1	17	82				Non Plastic						
	2.50	UDS								1.79	1.58	13.21		DST	0.14	28		
	3.30	SPT			10	11	0	30	70				Non Plastic					
	4.80	SPT			28	29	0	36	64				Non Plastic					
	5.50	UDS								1.87	1.63	14.78		DST	0.12	31		
	6.30	SPT		31	29	0	42	58				Non Plastic						
	7.80	SPT	Silty Sand with Gravel (SM)	18	15	0	52	48				Non Plastic						
	8.50	UDS							1.82	1.56	16.82		DST	0.12	29			
	9.30	SPT		13	10	2	11	87				Non Plastic						
	10.80	SPT	Sandy Silt with Gravel (SM-ML)	11	8	9	8	83				Non Plastic						
	12.30	SPT			18	13	2	7	91				Non Plastic					
	13.80	SPT			19	13	0	2	98				Non Plastic					
	15.30	SPT			24	16	0	18	82				Non Plastic					
	16.80	SPT			27	16	0	5	95				Non Plastic					
	18.30	SPT			33	18	0	5	95				Non Plastic					
	20.30	SPT			53	25	0	4	96				Non Plastic					

# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

VUP @ CH 22+980  
BH :8  
Depth : 20.00m  
Depth of Water table : 14.20 m

Date of start : 31/03/2021

Date of finish : 01/04/2021



**Project No. 2152**

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc	
				Observed	Corrected	Gravel	Sand	Silt/Clay	r(wet)	r(dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)		
				*	*														
	0.00																		
	1.80	SPT	Silty Clay of Medium Plasticity (CI)	18	18	1	15	84				40	25	2.71	UU	1.09	9		
	2.50	UDS							1.90	1.71	11.42								
	3.30	SPT		27	27	0	11	89											
	4.80	SPT	Silty Sand with Gravel (SM)	19	19	0	7	93				36	24	2.65	DST	31			
	5.50	UDS							1.90	1.69	12.33								
	6.30	SPT		32	30	0	70	30				Non	Plastic						
	7.80	SPT		30	26	0	80	20				Non	Plastic						
	8.50	UDS							1.88	1.62	15.86								
	9.30	SPT		28	23	0	73	27				Non	Plastic						
	10.80	SPT		29	22	0	70	30				Non	Plastic						
	12.30	SPT		32	23	0	80	20				Non	Plastic						
	13.80	SPT		34	23	0	73	27				Non	Plastic						
	15.30	SPT		51	24	1	73	26				Non	Plastic						
	16.80	SPT	49	23	0	79	21				Non	Plastic							
	18.30	SPT	38	19	0	67	33				Non	Plastic							
	20.30	SPT	33	17	1	75	24				Non	Plastic							

# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

VUP @ CH 25+430

BH :9

Depth : 20.00m

Depth of Water table : 12.25 m

Date of start : 02/04/2021

Date of finish : 03/04/2021



Project No. 2152

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc
				Observed	Corrected	Gravel	Sand	Silt/Clay	r(wet)	r(dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)	
				—*	—*													
	0.00			0	0													
	1.80	SPT	Silty Clay of Medium Plasticity (CI)	8	8	0	5	95				46	22	2.71	UU	0.53	11	
	2.50	UDS							1.82	1.61	12.89							
	3.30	SPT		17	17	0	1	99										
	4.80	SPT	Sandy Silt with Gravel (SM-ML)	11	11	0	3	97				42	21	2.62	DST	0.14	30	
	5.50	UDS							1.84	1.61	14.55							
	6.30	SPT		21	20	5	8	87				Non	Plastic					
	7.80	SPT		25	22	1	10	89				Non	Plastic					
	8.50	UDS							1.82	1.55	17.43							
	9.30	SPT		8	6	0	25	75				Non	Plastic					
	10.80	SPT	Silty Clay of Low Plasticity (CL)	12	9	0	4	96				Non	Plastic					
	12.30	SPT										33	18					
	13.80	SPT		18	18	0	13	87										
	15.30	SPT	Sandy Silt with Gravel (SM-ML)	19	19	0	2	98				Non	Plastic					
	16.80	SPT																
	18.30	SPT		22	15	0	4	96				Non	Plastic					
	19.00	SPT		23	15	2	8	90				Non	Plastic					
	20.30	SPT																
	20.00	SPT																
				33	18	1	46	53				Non	Plastic					
				53	24	0	49	51				Non	Plastic					

# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

MNB @ CH 29+260  
BH : 11  
Depth : 20.00m  
Depth of Water table : 5.50 m

Date of start : 04/04/2021

Date of finish : 05/04/2021



Project No. 2152

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc	
				Observed	Corrected	Gravel	Sand	Silt/Clay	r(wet)	r(dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)		
				★	★														
	0.00																		
	1.80	SPT	Silty Clay of High Plasticity (CH)	6	6	2	18	80				54	36						
	2.50	UDS							1.80	1.55	15.93			2.61	DST	0.14	28		
	3.30	SPT		9	10	0	14	86				Non	Plastic						
	4.80	SPT		11	11	1	22	77				Non	Plastic						
	5.50	UDS							1.83	1.51	21.55				DST	0.1	29		
	6.30	SPT		13	12	2	14	84				Non	Plastic						
	7.80	SPT		18	16	1	16	83				Non	Plastic						
	8.50	UDS							1.82	1.52	19.76				DST	0.1	29		
	9.30	SPT		12	11	0	28	72				Non	Plastic						
	10.80	SPT	Sandy Silt with Gravel (SM-ML)	13	11	0	7	93				Non	Plastic						
	12.30	SPT		14	13	1	6	93				Non	Plastic						
	13.80	SPT		17	14	0	6	94				Non	Plastic						
	15.30	SPT		13	10	0	3	97				Non	Plastic						
	16.80	SPT	Silty Clay of Medium Plasticity (CI)	17	17	0	1	99				42	23						
	18.30	SPT		21	15	0	7	93				Non	Plastic						
	20.30	SPT	Sandy Silt with Gravel (SM-ML)	31	19	0	7	93				Non	Plastic						

# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

Flyover @ CH 32+170  
BH : 12  
Depth : 30.00m  
Depth of Water table : 13.20 m

Date of start : 06/04/2021

Date of finish : 07/04/2021



Project No. 2152

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc		
				Observed	Corrected	Gravel	Sand	Silt/Clay	r (wet)	r (dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)			
				*	*															
	0.00																			
	1.80	SPT	Sandy Silt with Gravel (SM)	18	24	0	24	76												
	2.50	UDS							1.82	1.64	10.32	Non	Plastic	2.65	DST	0.81	9	29		
	3.30	SPT	Silty Sand with Gravel (SM)	9	10	0	73	27				Non	Plastic							
	4.80	SPT	Silty Clay of Medium Plasticity (Cl)	19	19	4	32	64	1.85	1.65	11.45	32	19	2.71	UU	1.43	9			
	5.50	UDS																		
	6.30	SPT			23	23	0	2	98											
	7.80	SPT			28	28	0	4	96	1.88	1.63	14.76	44							20
	8.50	UDS																		
	9.30	SPT			29	29	0	2	98											
	10.80	SPT		22	22	2	17	81				39	21	2.65	DST	0.81	9	30		
	12.30	SPT	Silty Sand with Gravel (SM)	25	18	0	56	44				Non	Plastic							
	13.80	SPT		30	18	0	66	34	1.88	1.55	20.91	Non	Plastic							
	14.50	UDS																		
	15.30	SPT		29	29	0	11	89												
	16.80	SPT		26	26	0	1	99												
	18.30	SPT		27	27	0	2	98				76	33	2.65	DST	0.81	9	30		
	19.80	SPT		30	30	0	3	97												
	21.30	SPT	Silty Clay of High Plasticity (CH)	28	28	0	2	98												
	22.80	SPT			22	22	0	1	99											
	24.30	SPT			24	24	0	1	99				63							32
	25.80	SPT			25	25	1	3	96											
	27.30	SPT			31	31	0	2	98											
	28.80	SPT			34	34	1	17	82				53	28						
	30.30	SPT		35	35	1	10	89												



# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

MJB @ CH 33+490  
BH : 14  
Depth : 30.00m  
Depth of Water table : 3.20 m

Date of start : 09/04/2021

Date of finish : 10/04/2021



Project No. 2152

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc	
				Observed	Corrected	Gravel	Sand	Silt/Clay	r (wet)	r (dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)		
				✱	✱														
	0.00			0 20 40 60 80 100	0 20 40 60 80 100														
	1.00																		
	1.80	SPT	Silty Sand with Gravel (SM)	2.00	✱ 5	✱ 6	0	74	26	1.75	1.49	17.51	Non	Plastic	DST	27			
	2.50	UDS		3.00	✱ 8	✱ 9	0	85	15				Non	Plastic					
	3.30	SPT		4.00	✱ 11	✱ 11	0	2	98	1.84	1.53	20.36	58	27					
	4.80	SPT	Silty Clay of High Plasticity (CH)	5.00	✱ 11	✱ 11	0	2	98						UU	0.74	2		
	5.50	UDS		6.00	✱ 18	✱ 18	1	3	96										
	6.30	SPT		7.00	✱ 13	✱ 13	0	4	96	1.86	1.55	20.09	54	25					
	7.80	SPT		8.00	✱ 13	✱ 13	0	4	96										
	8.50	UDS		9.00	✱ 17	✱ 17	0	2	98										
	9.30	SPT		10.00	✱ 17	✱ 17	0	2	98						UU	0.86	3		
	10.80	SPT	11.00	✱ 22	✱ 17	1	88	11				Non	Plastic						
	12.30	SPT	12.00	✱ 27	✱ 19	0	80	20				Non	Plastic						
	13.80	SPT	13.00	✱ 27	✱ 19	0	80	20				Non	Plastic						
	15.30	SPT	14.00	✱ 24	✱ 18	0	82	18				Non	Plastic						
	16.80	SPT	Silty Sand with Gravel (SM)	15.00	✱ 38	✱ 23	0	88	12				Non	Plastic					
	18.30	SPT		16.00	✱ 31	✱ 20	0	90	10				Non	Plastic					
	19.80	SPT		17.00	✱ 31	✱ 20	0	90	10				Non	Plastic					
	21.30	SPT	Silty Clay of High Plasticity (CI)	18.00	✱ 28	✱ 28	0	2	98						UU	0.86	3		
	22.80	SPT		19.00	✱ 28	✱ 28	0	2	98										
	24.30	SPT		20.00	✱ 32	✱ 32	1	5	94				55	23					
	25.80	SPT	Silty Sand with Gravel (SM)	21.00	✱ 41	✱ 41	0	4	96						UU	0.86	3		
	27.30	SPT		22.00	✱ 41	✱ 41	0	4	96										
	28.80	SPT		23.00	✱ 39	✱ 39	1	2	97				51	22					
	30.30	SPT		24.00	✱ 48	✱ 24	0	83	17				Non	Plastic					
		SPT		25.00	✱ 48	✱ 24	0	83	17				Non	Plastic					
		SPT	Silty Sand with Gravel (SM)	26.00	✱ 52	✱ 25	0	86	14				Non	Plastic					
		SPT		27.00	✱ 52	✱ 25	0	86	14				Non	Plastic					
		SPT		28.00	✱ 55	✱ 26	0	79	21				Non	Plastic					
		SPT	Silty Sand with Gravel (SM)	29.00	✱ 55	✱ 26	0	79	21				Non	Plastic					
		SPT		30.00	✱ 62	✱ 28	0	84	16				Non	Plastic					
		SPT		30.00	✱ 67	✱ 29	0	75	25				Non	Plastic					



# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

MNB @ CH 38+010  
BH : 16  
Depth : 20.00m  
Depth of Water table : 8.75 m

Date of start : 12/04/2021

Date of finish : 13/04/2021



**Project No. 2152**

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc
				Observed	Corrected	Gravel	Sand	Silt/Clay	r(wet)	r(dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)	
				*	*													
	0.00																	
	1.80	SPT	Sandy Silt with Gravel (SM-ML)	10	13	0	50	50				Non	Plastic					
	2.50	UDS								1.75	1.51	15.86			DST	0.13	26	
	3.30	SPT			4	4	1	39	60				Non	Plastic				
	4.80	SPT	Silty Sand with Gravel (SM)	8	8	1	18	81				Non	Plastic					
	5.50	UDS								1.77	1.51	17.21			DST		28	
	6.30	SPT			4	4	1	8	91				52	23				
	7.80	SPT	Silty Clay of Medium to High Plasticity (CI-CH)	7	7	0	4	96										
	8.50	UDS								1.80	1.48	21.64			UU	0.23	4	
	9.30	SPT			13	13	0	3	97				66	28				
	10.80	SPT			18	18	0	2	98									
	12.30	SPT			15	15	0	2	98				56	27				
	13.80	SPT			14	14	1	3	96									
	15.30	SPT			17	17	0	2	98				55	25				
	16.80	SPT			22	22	0	4	96									
	18.30	SPT			19	19	0	6	94									
	20.30	SPT			26	26	0	2	98				54	25				





# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

VUP @ CH 40+940

BH : 19

Depth : 20.00m

Depth of Water table : 11.80 m

Date of start : 14/04/2021

Date of finish : 15/04/2021



**Project No. 2152**

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc	
				Observed	Corrected	Gravel	Sand	Silt/Clay	r(wet)	r(dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)		
				★	★														
	0.00																		
	1.80	SPT	Silty Clay of Medium Plasticity (CI)	★ 7	★ 7	0	14	86				39	21	2.75	UU	0.41	9		
	2.50	UDS								1.78	1.61	10.45							
	3.30	SPT		★ 7	★ 7	0	9	91											
	4.80	SPT		★ 9	★ 9	0	11	89				44	23						
	5.50	UDS								1.82	1.62	12.68							
	6.30	SPT	★ 11	★ 11	0	8	92												
	7.80	SPT	Sandy Silt with Gravel (SM-ML)	★ 24	★ 24	0	11	89				45	21	2.61	DST	0.13	31		
	8.50	UDS								1.91	1.66	15.36							
	9.30	SPT		★ 40	★ 33	0	40	60				Non	Plastic						
	10.80	SPT		★ 37	★ 28	0	58	42				Non	Plastic						
	12.30	SPT		★ 31	★ 19	0	64	36				Non	Plastic						
	13.80	SPT	Silty Sand with Gravel (SM)	★ 35	★ 20	0	82	18				Non	Plastic						
	15.30	SPT		★ 36	★ 20	0	65	35				Non	Plastic						
	16.80	SPT		★ 42	★ 22	0	75	25				Non	Plastic						
	18.30	SPT	Silty Clay of High Plasticity (CH)	★ 35	★ 35	0	3	97				62	27						
	20.30	SPT		★ 31	★ 31	0	3	97											



# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

Flyover @ CH 43+910

BH : 21

Depth : 30.00m

Depth of Water table : 10.25 m

Date of start : 16/04/2021

Date of finish : 17/04/2021



Project No. 2152

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc		
				Observed	Corrected	Gravel	Sand	Silt/Clay	r(wet)	r(dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)			
				✱	✱															
	0.00																			
	1.00																			
	1.80	SPT	Sandy Silt with Gravel (SM-ML)	2.00	✱ 6	✱ 8	1	17	82				Non	Plastic						
	2.50	UDS																		
	3.30	SPT			3.00	✱ 7	✱ 8	1	15	84				Non	Plastic					DST
	4.00			4.00																
	4.80	SPT	Silty Clay of Medium Plasticity (CI)	5.00	✱ 7	✱ 7	0	4	96				Non	Plastic						
	5.50	UDS																		
	6.30	SPT			6.00	✱ 10	✱ 10	0	5	95			46	22						DST
	7.00			7.00																
	7.80	SPT	Sandy Silt with Gravel (SM-ML)	8.00	✱ 11	✱ 11	1	6	93											
	8.50	UDS																		
	9.30	SPT			9.00	✱ 21	✱ 17	0	9	91				Non	Plastic					DST
	10.00			10.00																
	10.80	SPT	Silty Sand with Gravel (SM)	11.00	✱ 20	✱ 15	1	54	45				Non	Plastic						
	12.30	SPT			12.00	✱ 29	✱ 18	0	67	33				Non	Plastic					
	13.80	SPT			13.00															
	13.80	SPT	Sandy Silt with Gravel (SM-ML)	14.00	✱ 25	✱ 16	0	49	51				Non	Plastic						
	15.30	SPT	Silty Clay of Medium Plasticity (CI)	15.00	✱ 20	✱ 20	5	11	84				46	23						
	16.80	SPT			16.00															
	17.00				17.00	✱ 19	✱ 19	3	75	22										
	18.30	SPT	Silty Sand with Gravel (SM)	18.00	✱ 28	✱ 17	0	61	39				Non	Plastic						
	19.80	SPT			19.00															
	21.30	SPT			20.00	✱ 32	✱ 18	3	72	25				Non	Plastic					
	22.80	SPT			21.00	✱ 33	✱ 18	2	58	40				Non	Plastic					
	24.30	SPT			22.00															
	25.80	SPT			23.00	✱ 41	✱ 20	1	73	26				Non	Plastic					
	27.30	SPT			24.00	✱ 40	✱ 20	0	69	31				Non	Plastic					
	28.80	SPT		25.00																
	29.00			26.00	✱ 55	✱ 24	0	84	16				Non	Plastic						
	29.00			27.00	✱ 52	✱ 23	1	86	13				Non	Plastic						
	29.00			28.00																
	29.00			29.00	✱ 65	✱ 26	3	79	18				Non	Plastic						
	30.30	SPT		30.00	✱ 72	✱ 28	1	82	17				Non	Plastic						

# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

MJB @ CH 47+950  
BH : 22  
Depth : 30.00m  
Depth of Water table : 3.80 m

Date of start : 19/04/2021

Date of finish : 20/04/2021



Project No. 2152

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc
				Observed	Corrected	Gravel	Sand	Silt/Clay	r(wet)	r(dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)	
				✱	✱													
	0.00			0	0	0	0	0										
	1.00																	
	1.80	SPT	Sandy Silt with Gravel (SM-ML)	15	20	0	35	65	1.86	1.60	16.41	Non Plastic						
	2.50	UDS																
	3.00	SPT	Silty Sand with Gravel (SM)	24	28	0	80	20				Non Plastic		DST	0.13	30		
	4.00																	
	4.80	SPT	Sandy Silt with Gravel (SM-ML)	10	10	0	16	84	1.85	1.53	20.59	Non Plastic						
	5.50	UDS																
	6.30	SPT	Silty Clay of Medium to High Plasticity (CI-CH)	13	13	0	3	97				56	27					
	7.00																	
	7.80	SPT		16	15	0	8	92	1.87	1.58	18.45							
	8.50	UDS																
	9.30	SPT		20	17	0	7	93				Non Plastic						
	10.00																	
	10.80	SPT	Sandy Silt with Gravel (SM-ML)	19	16	1	4	95				Non Plastic						
	12.30	SPT		16	14	0	4	96				Non Plastic						
	13.80	SPT		18	15	0	2	98				Non Plastic						
	15.30	SPT		27	18	0	5	95				Non Plastic						
	16.00																	
	16.80	SPT		39	23	1	67	32				Non Plastic						
	18.30	SPT		43	24	0	69	31				Non Plastic						
	19.80	SPT		49	26	1	84	15				Non Plastic						
	21.30	SPT	Silty Sand with Gravel (SM)	42	23	1	85	14				Non Plastic						
	22.80	SPT		55	27	1	81	18				Non Plastic						
	24.30	SPT		63	30	0	78	22				Non Plastic						
	25.80	SPT		53	26	0	74	26				Non Plastic						
	27.30	SPT		61	28	1	80	19				Non Plastic						
	28.80	SPT		73	32	1	88	11				Non Plastic						
	30.30	SPT		76	32	2	88	10				Non Plastic						

# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

Flyover @ CH 49+900  
BH : 23  
Depth : 30.00m  
Depth of Water table : 9.80 m

Date of start : 20/04/2021

Date of finish : 21/04/2021

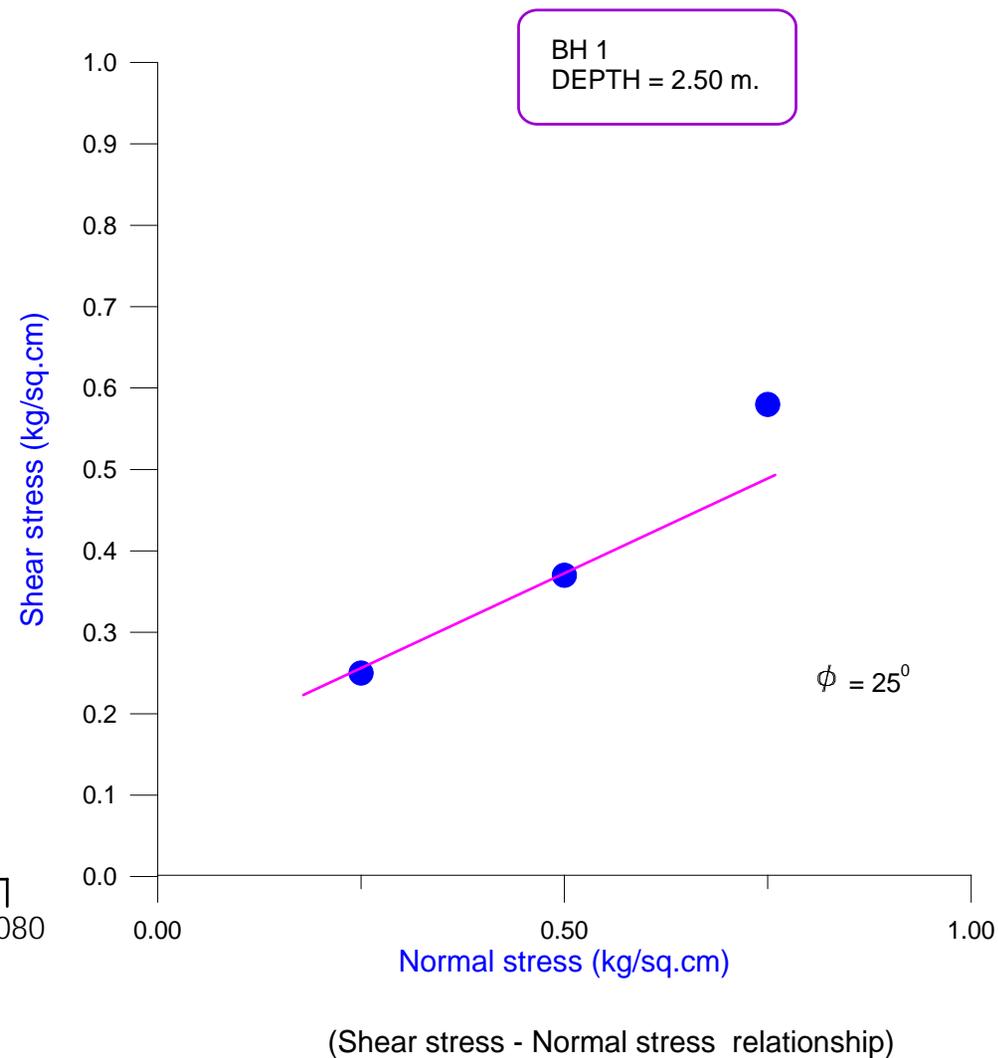
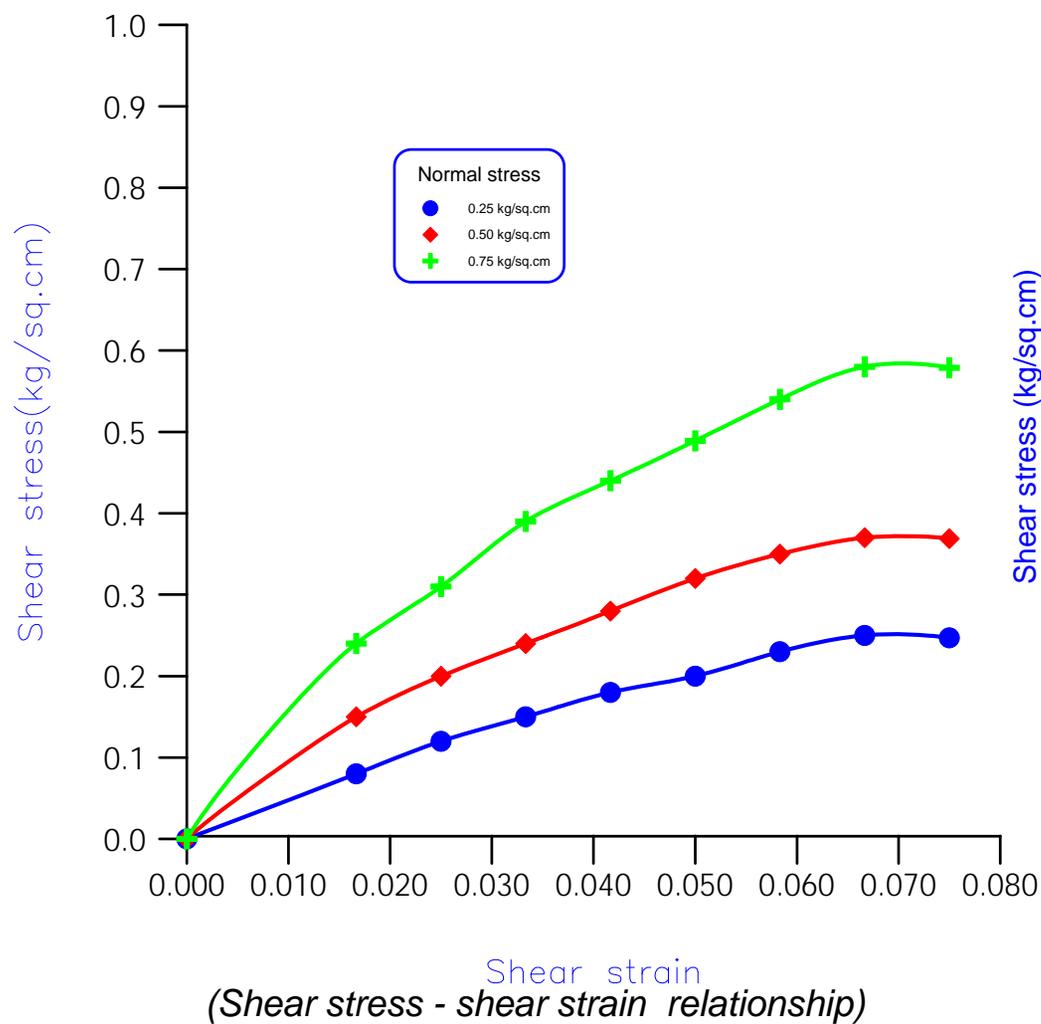


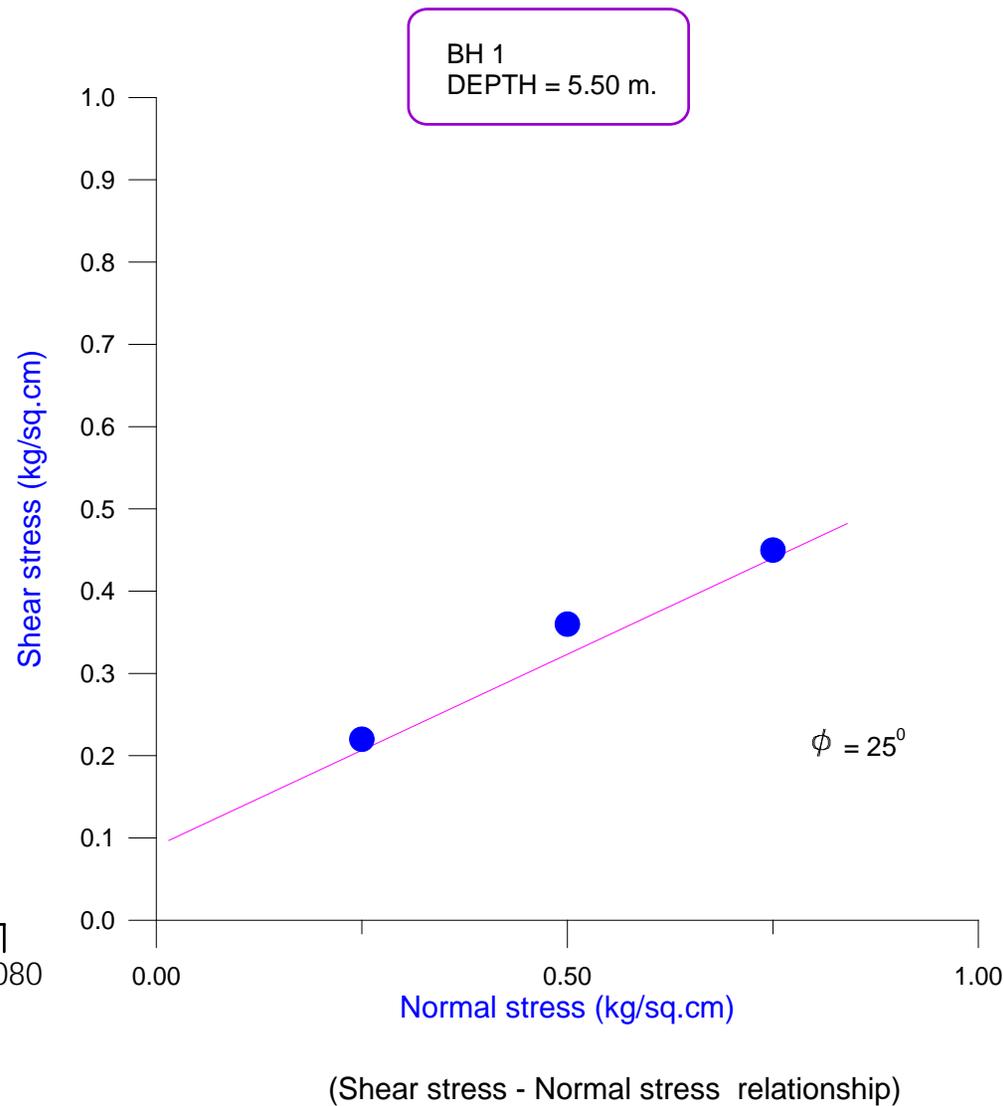
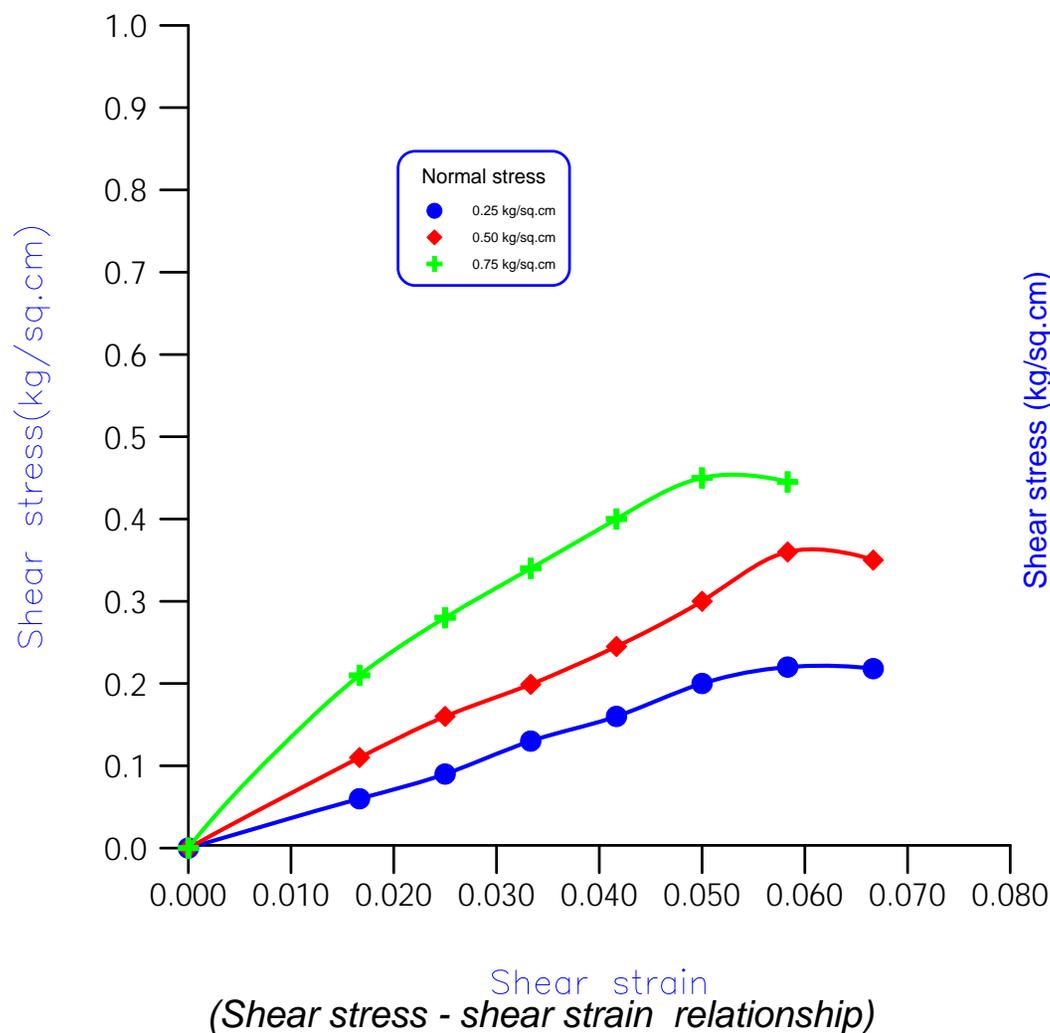
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Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot			Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc	
				Observed	Corrected		Gravel	Sand	Silt/Clay	r(wet)	r(dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)		
				0.00																
	1.80	SPT	Sandy Silt with Gravel (SM-ML)	1.00																
	2.50	UDS		2.00	11	15	0	33	67				Non Plastic							
	3.30	SPT	Silty Clay of Medium Plasticity (CI)	3.00	6	6	0	2	98				48 24				DST			
	4.80	SPT		4.00																
	5.50	UDS		5.00	10	10	0	2	98											
	6.30	SPT	Silty Sand with Gravel (SM)	6.00	12	11	0	65	35				Non Plastic							
	7.80	SPT		7.00										Non Plastic						
	8.50	UDS		8.00	18	15	0	56	44					Non Plastic						
	9.30	SPT		9.00	21	17	0	79	21					Non Plastic						
	10.80	SPT		10.00	20	15	0	76	24					Non Plastic						
	12.30	SPT		12.00	31	19	0	80	20					Non Plastic						
	13.80	SPT		13.00	28	17	1	83	16					Non Plastic						
	15.30	SPT		14.00	32	19	18	74	8					Non Plastic						
	16.80	SPT		15.00	36	20	1	78	21					Non Plastic						
	18.30	SPT		16.00	44	22	6	88	6					Non Plastic						
	19.80	SPT	17.00	41	21	1	83	16					Non Plastic							
	21.30	SPT	18.00	39	20	1	81	18					Non Plastic							
	22.80	SPT	19.00	47	22	0	81	19					Non Plastic							
	24.30	SPT	20.00	58	25	0	93	7					Non Plastic							
	25.80	SPT	21.00	56	24	2	86	12					Non Plastic							
	27.30	SPT	22.00	63	26	0	72	28					Non Plastic							
	28.80	SPT	23.00	76	30	0	89	11					Non Plastic							
	30.30	SPT	24.00	81	31	1	87	12					Non Plastic							

Soil Engineering Constants

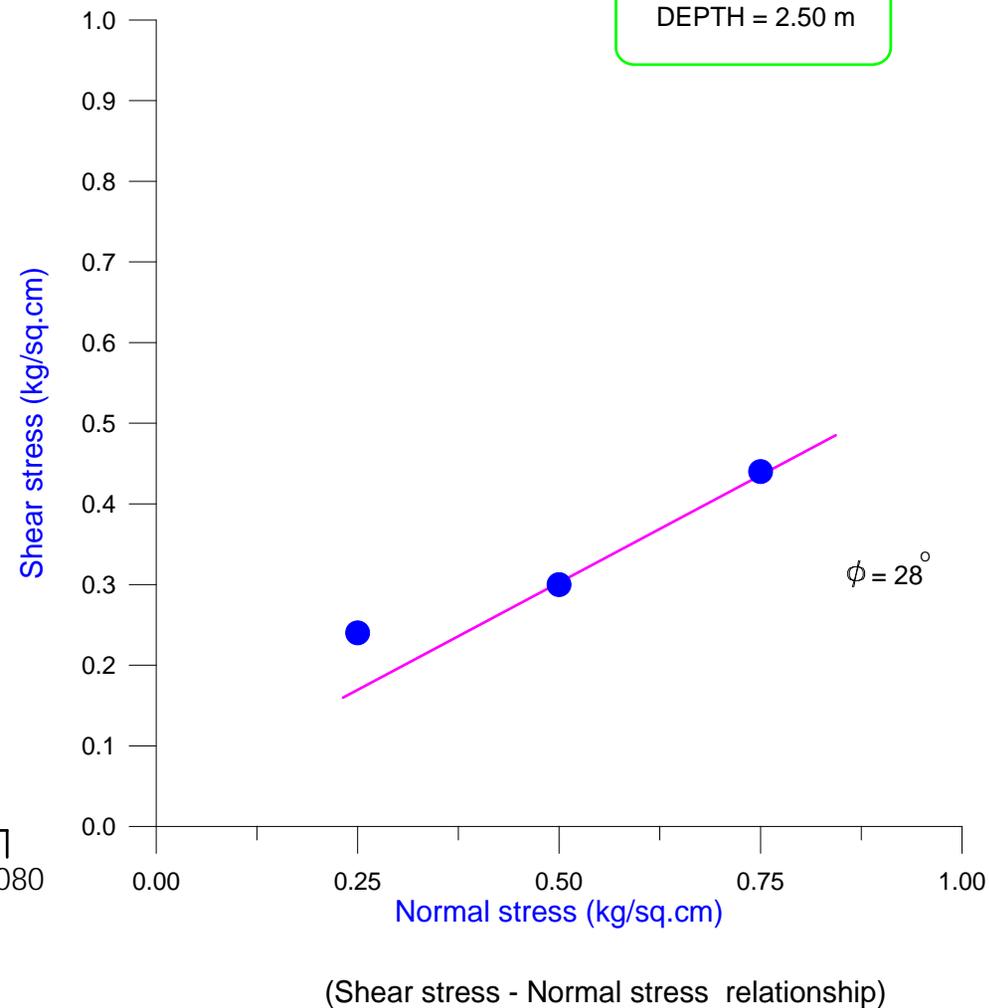
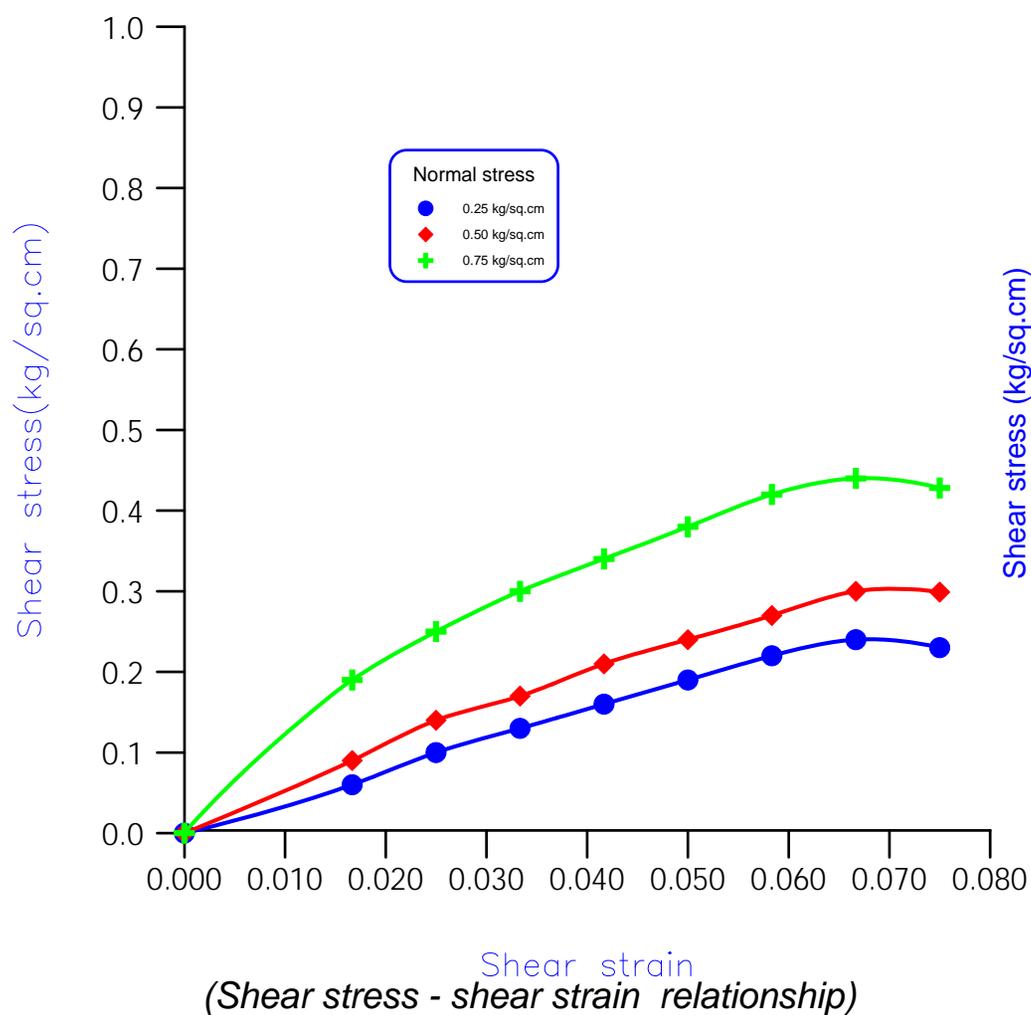
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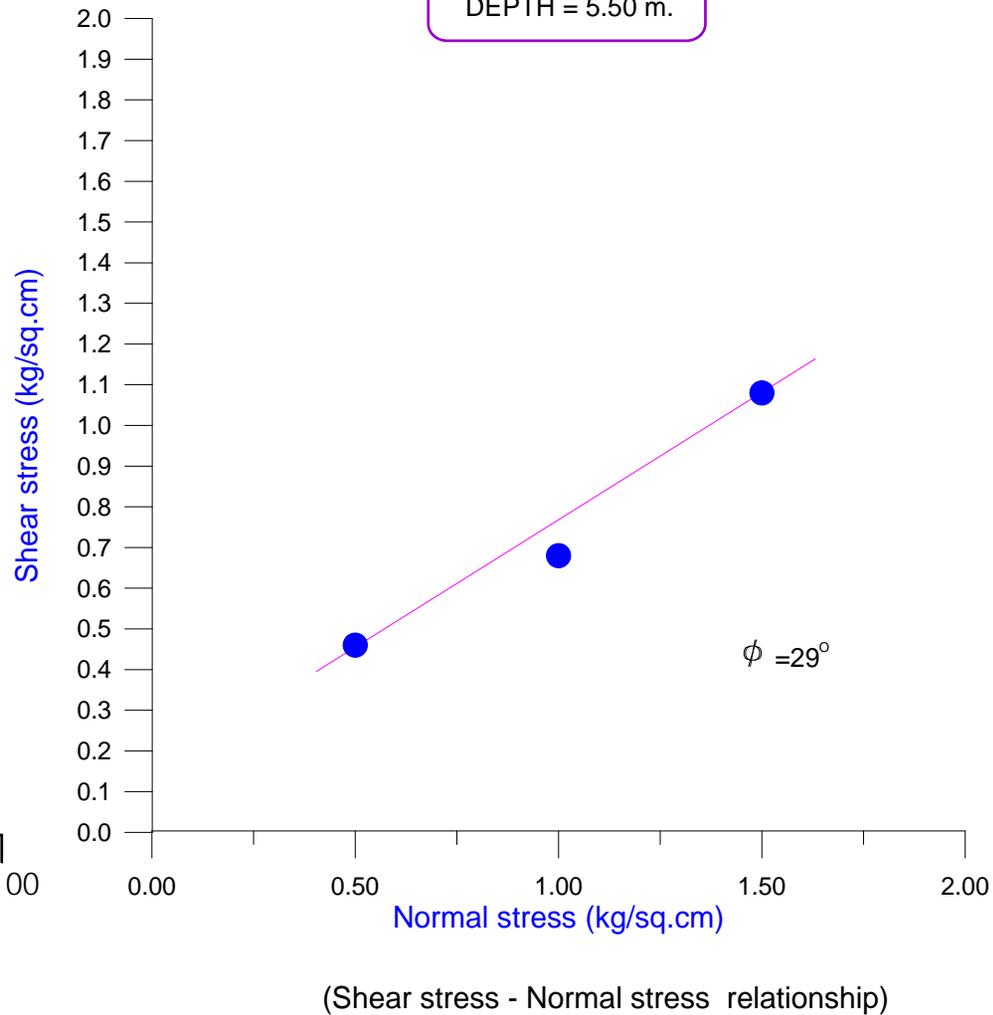
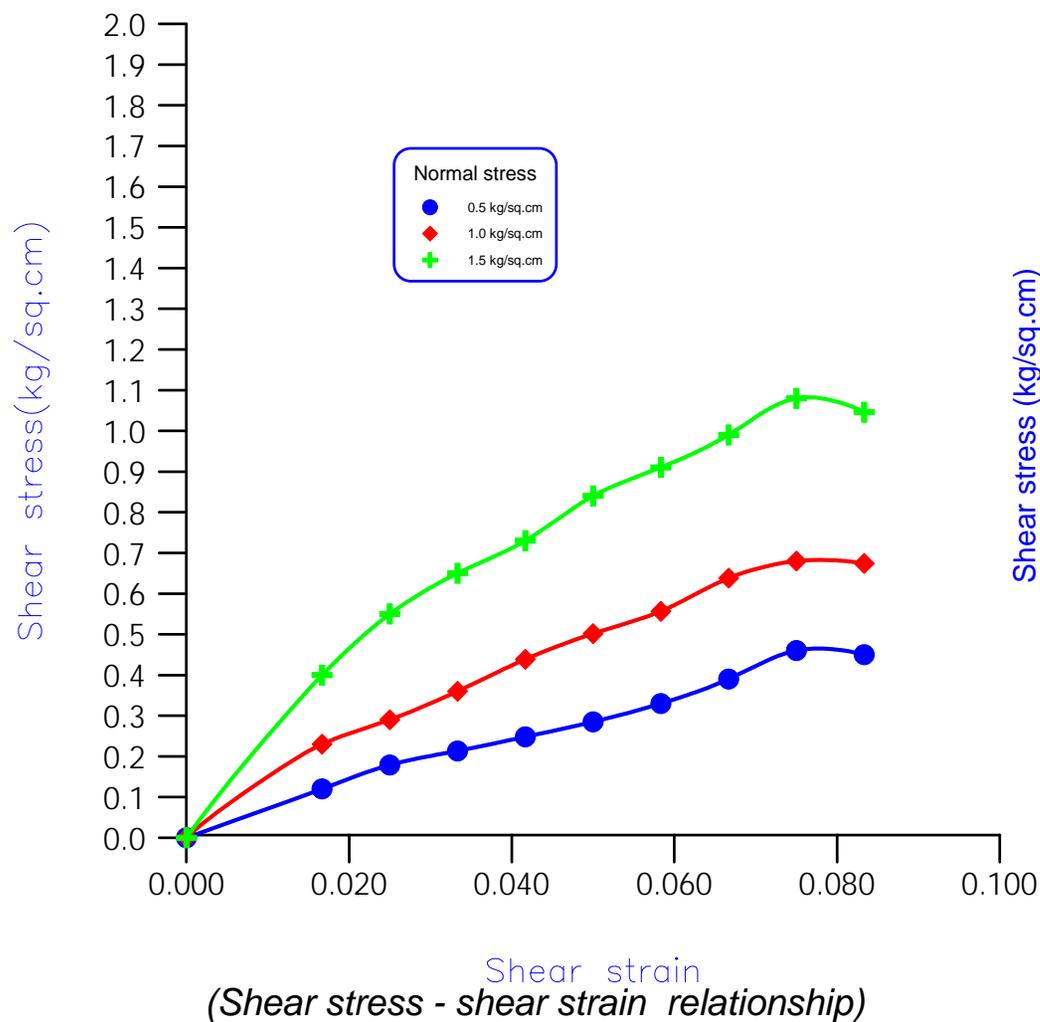
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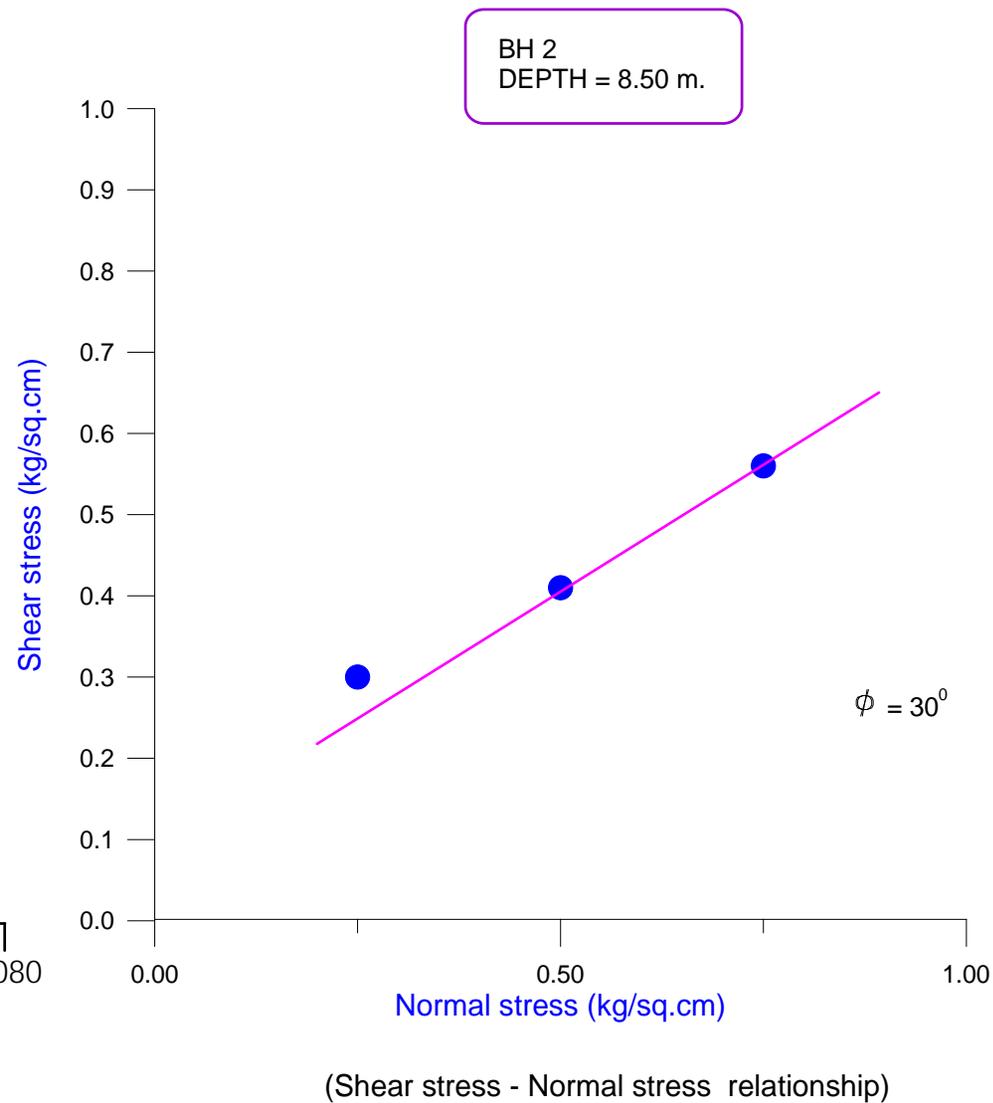
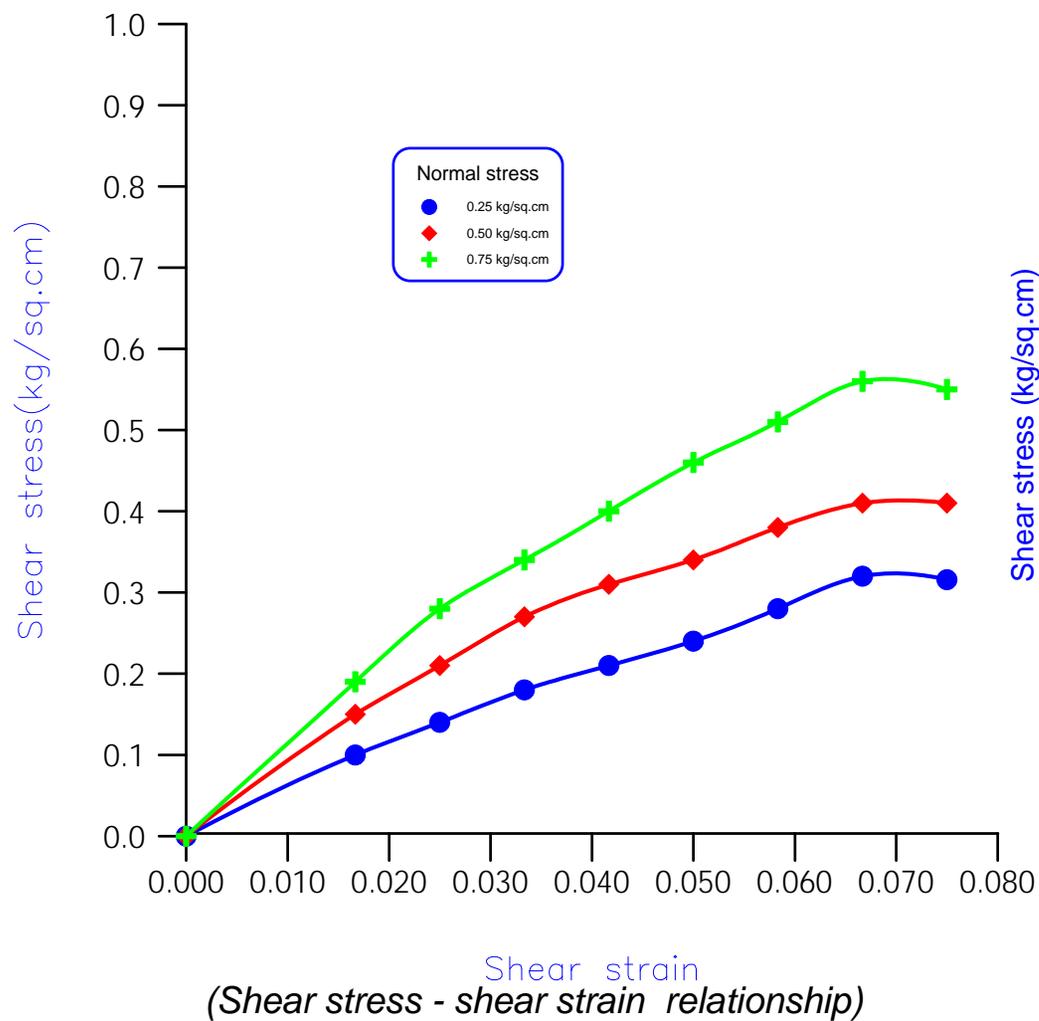
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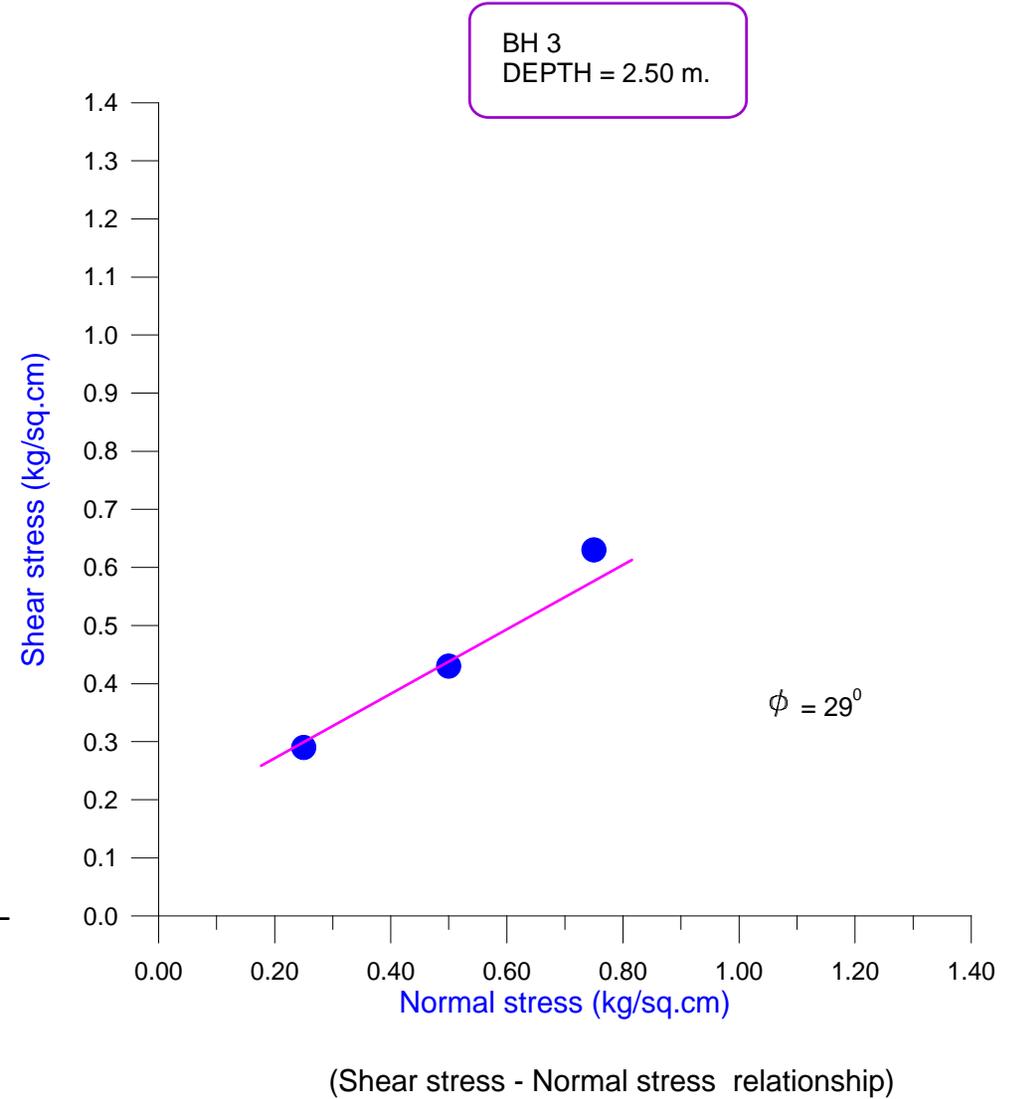
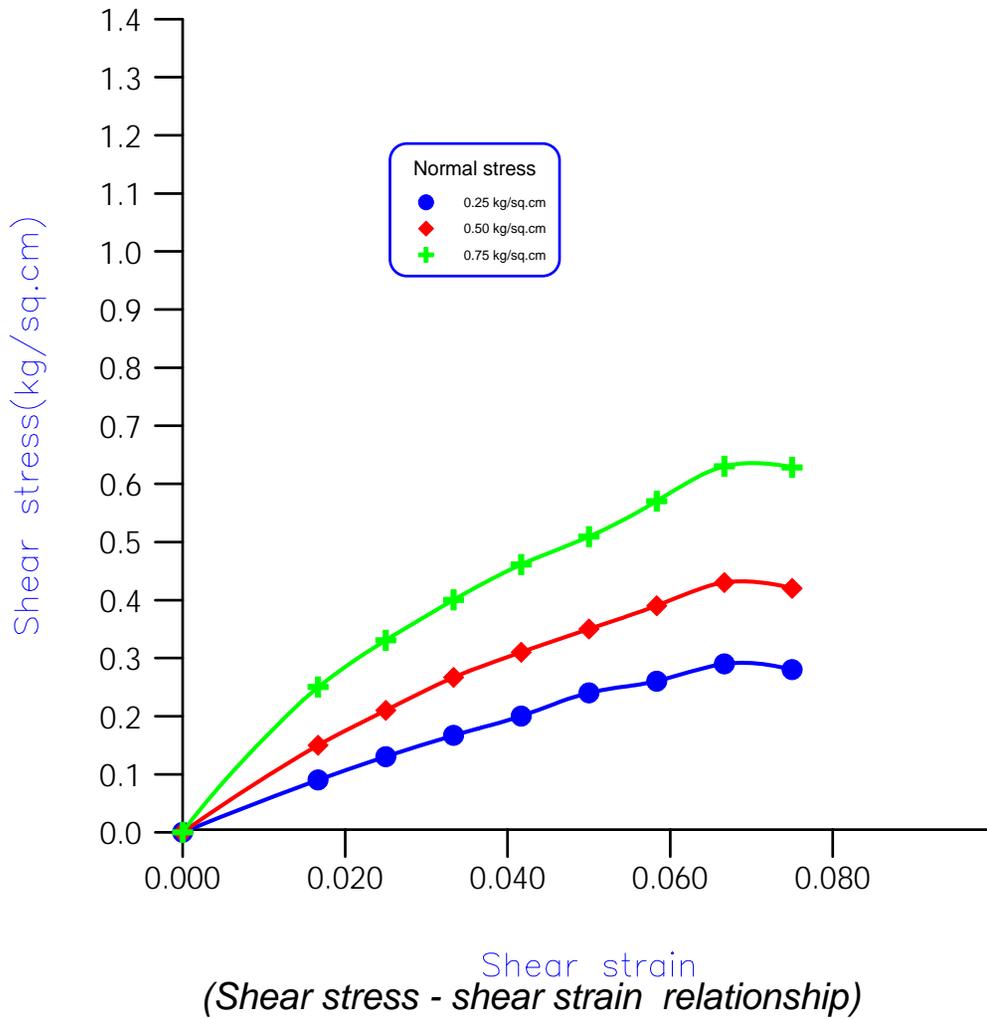


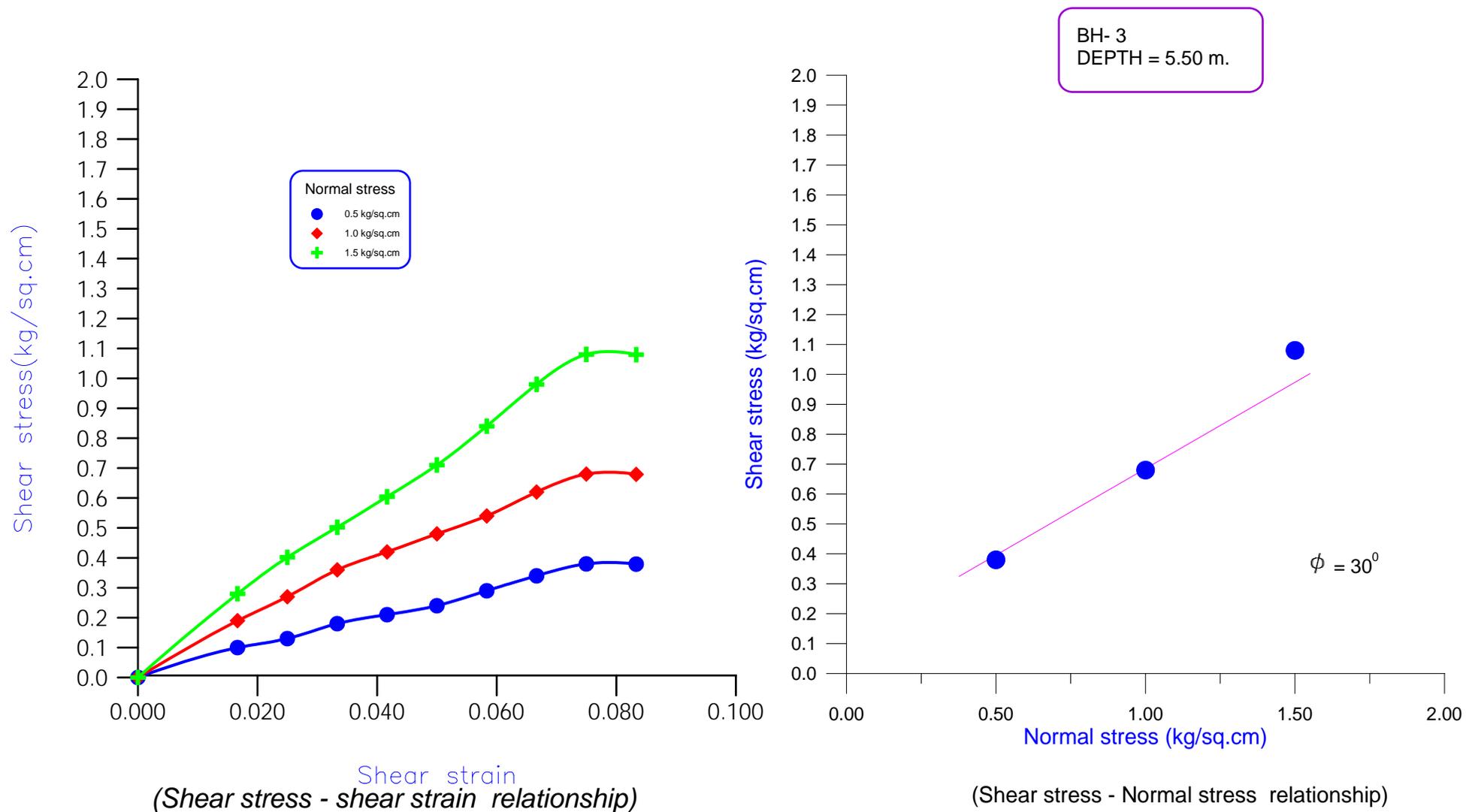
Soil Engineering Constants

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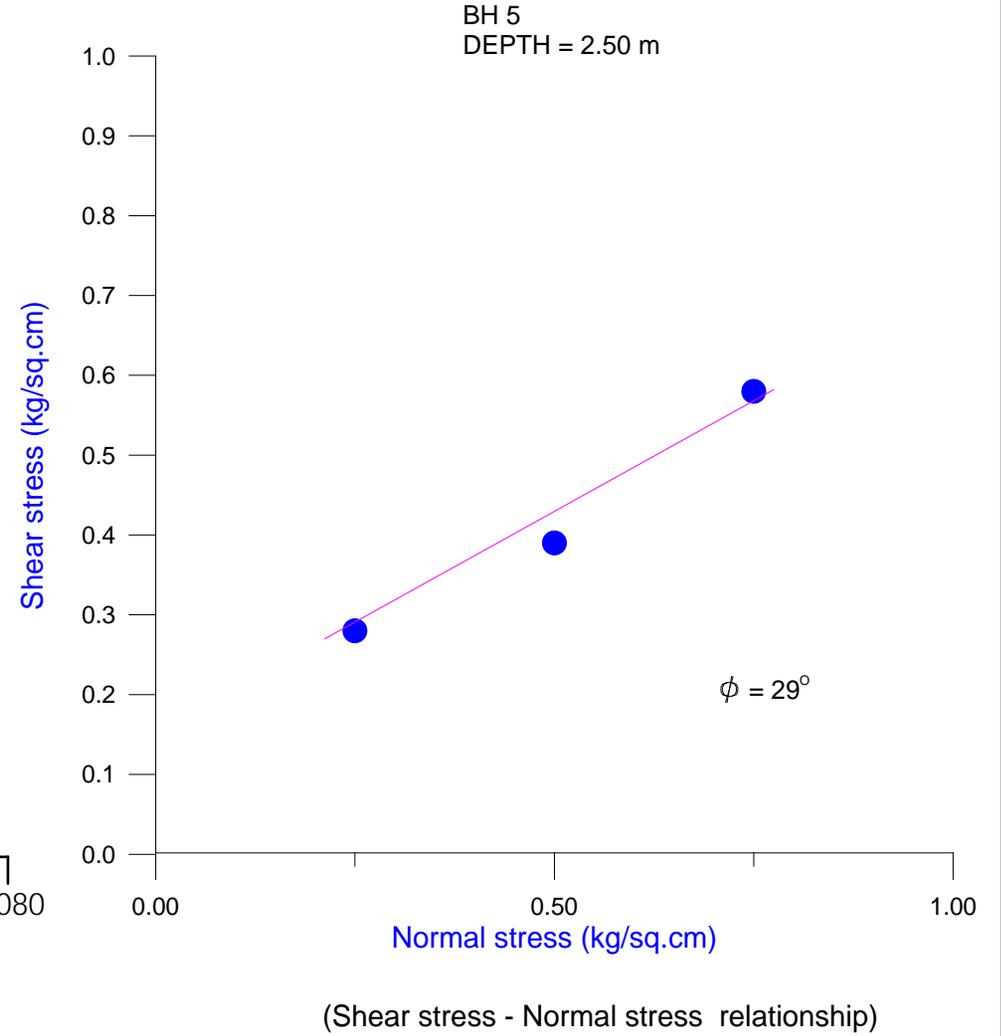
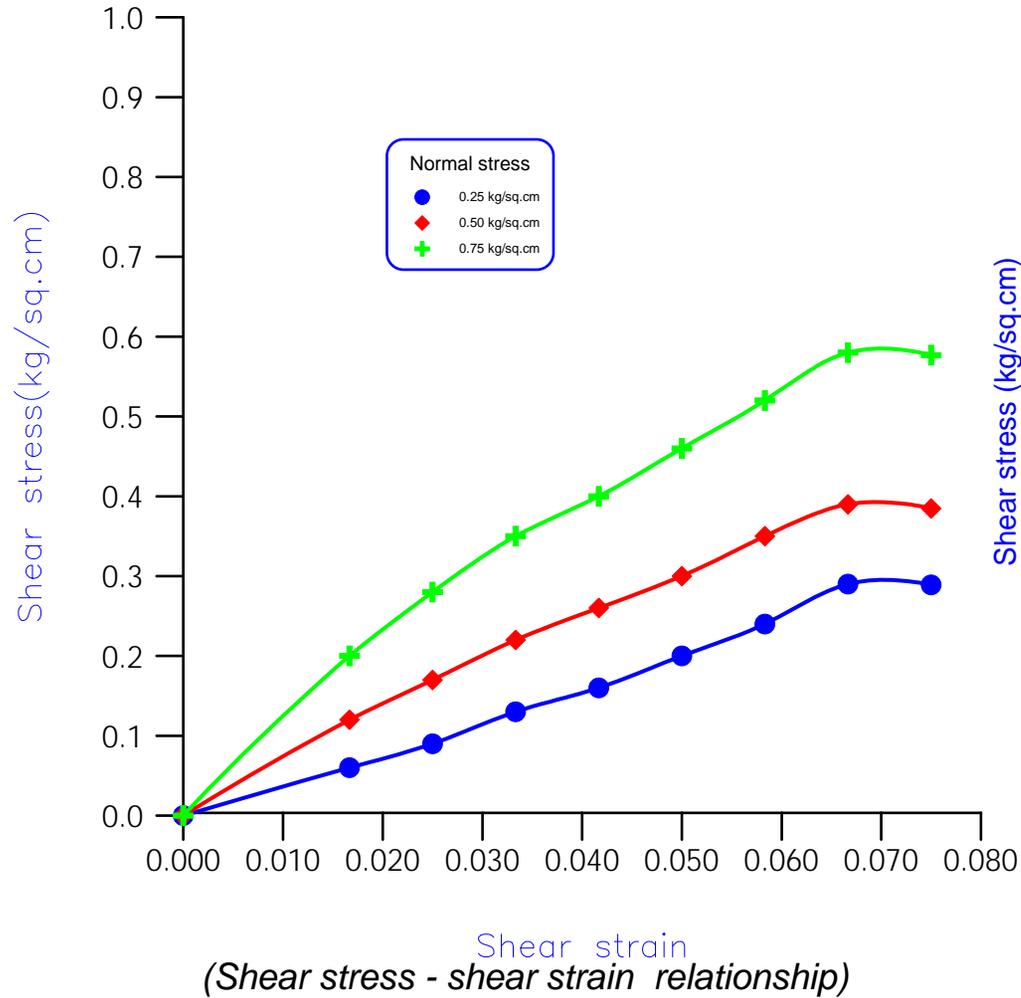


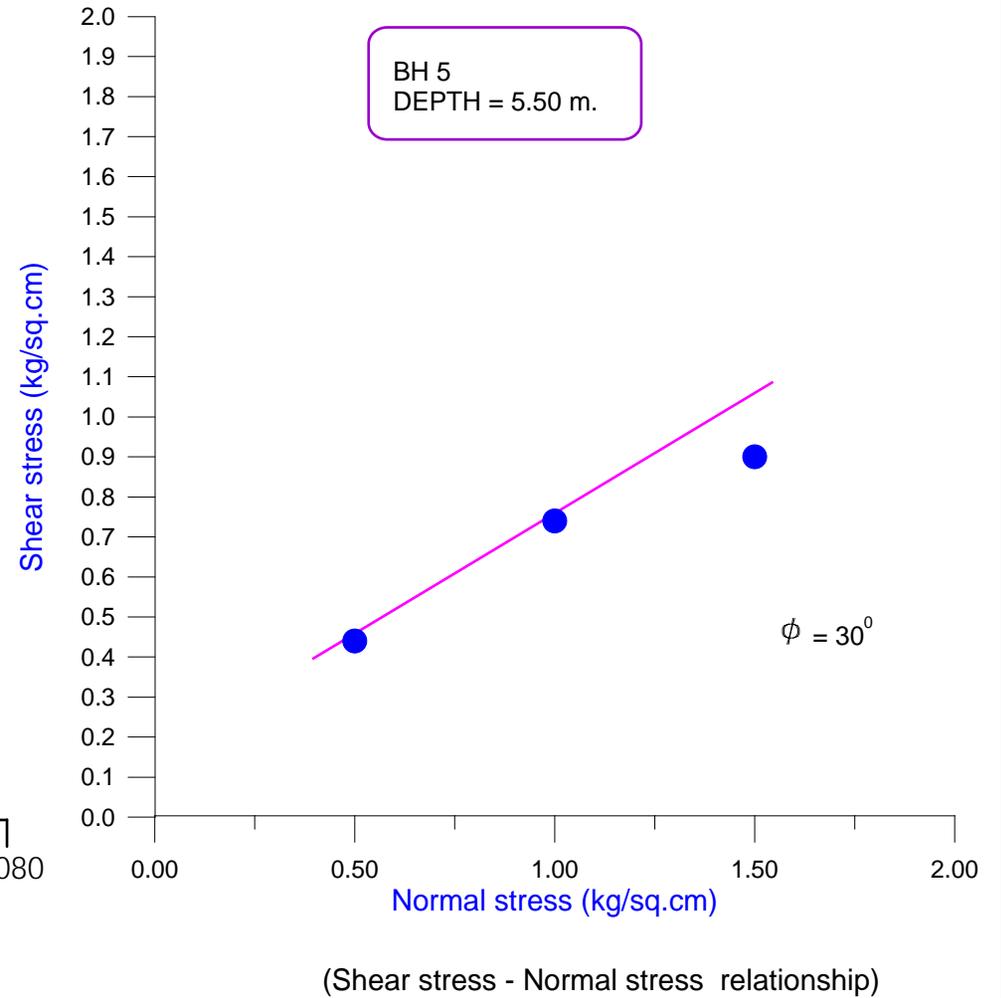
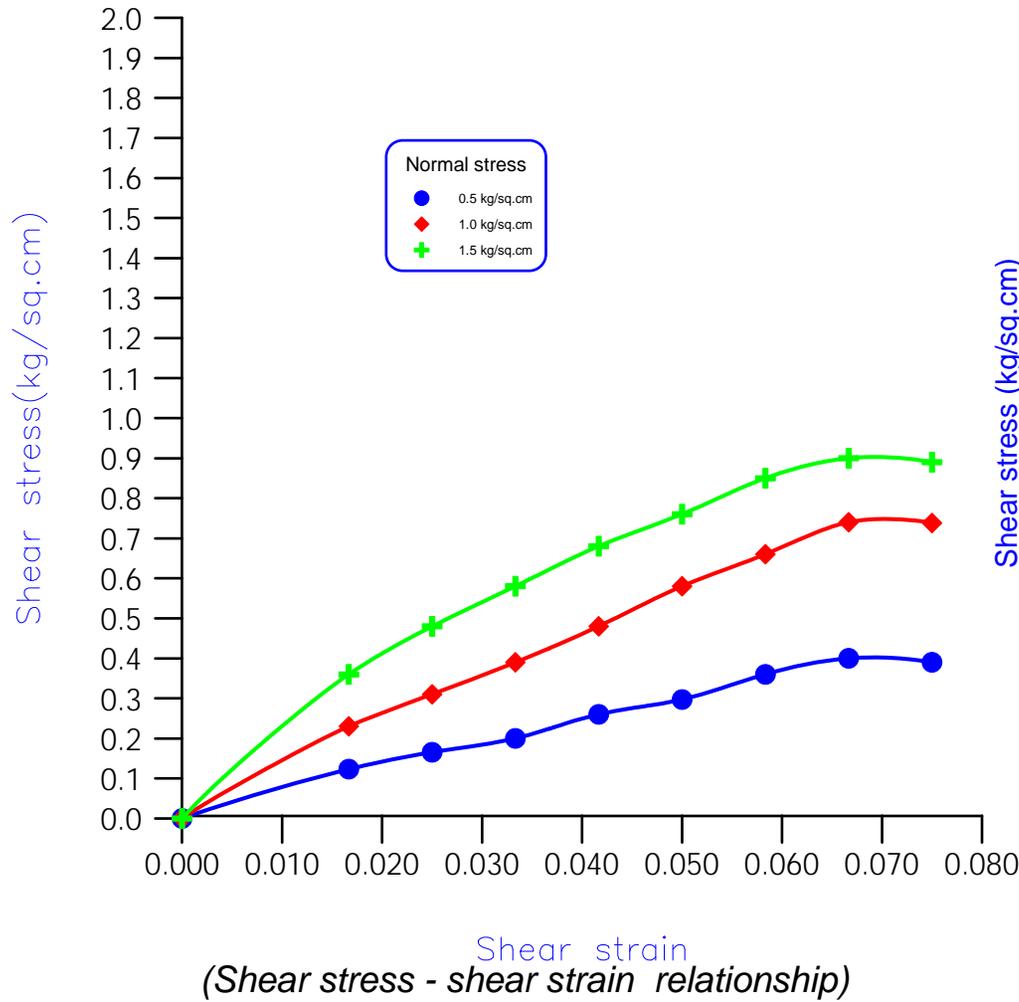




Soil Engineering Constants

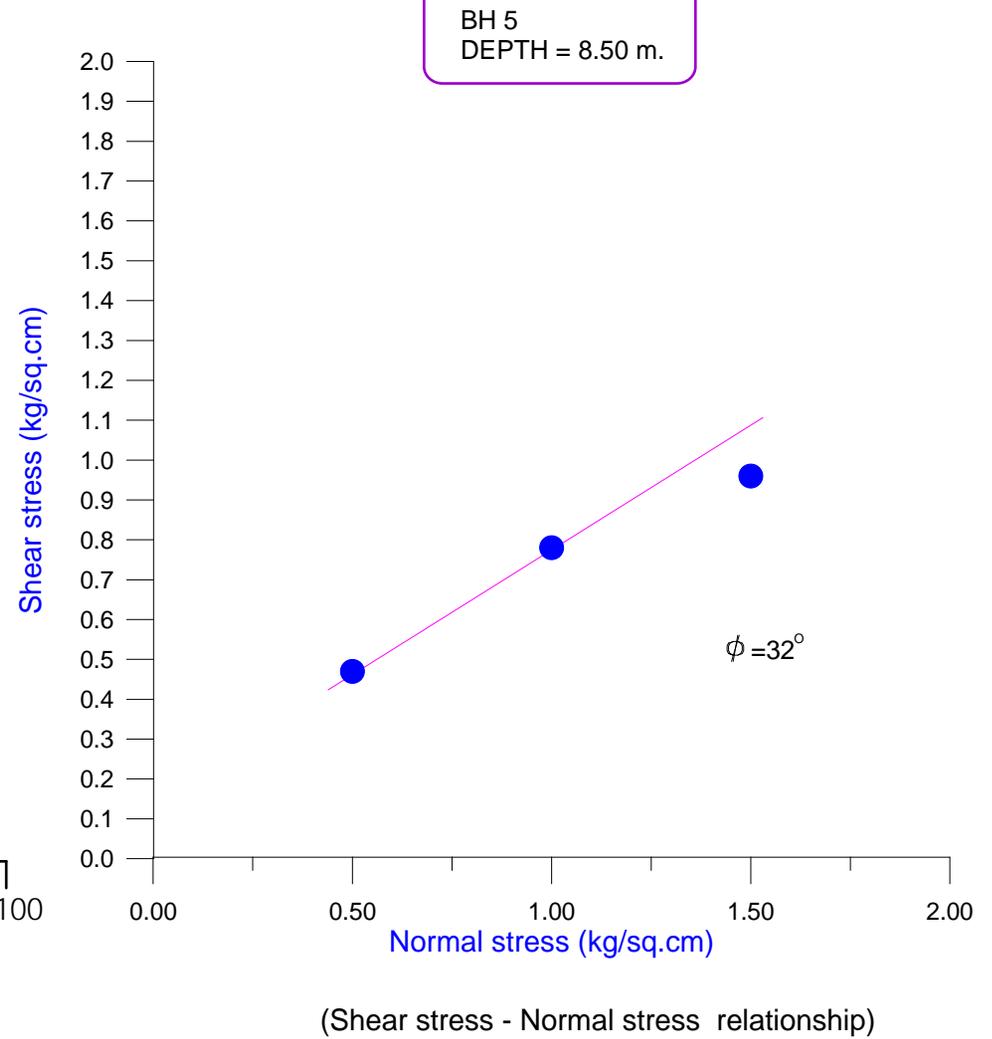
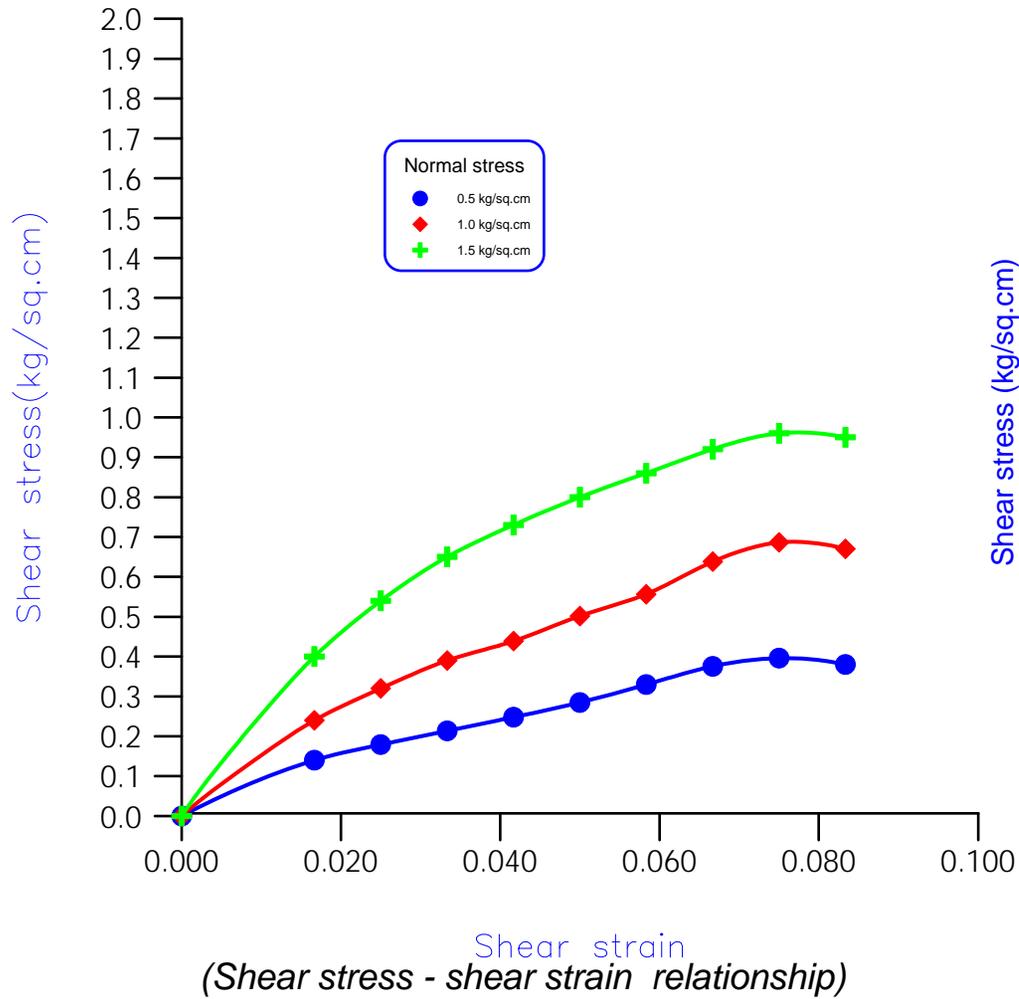
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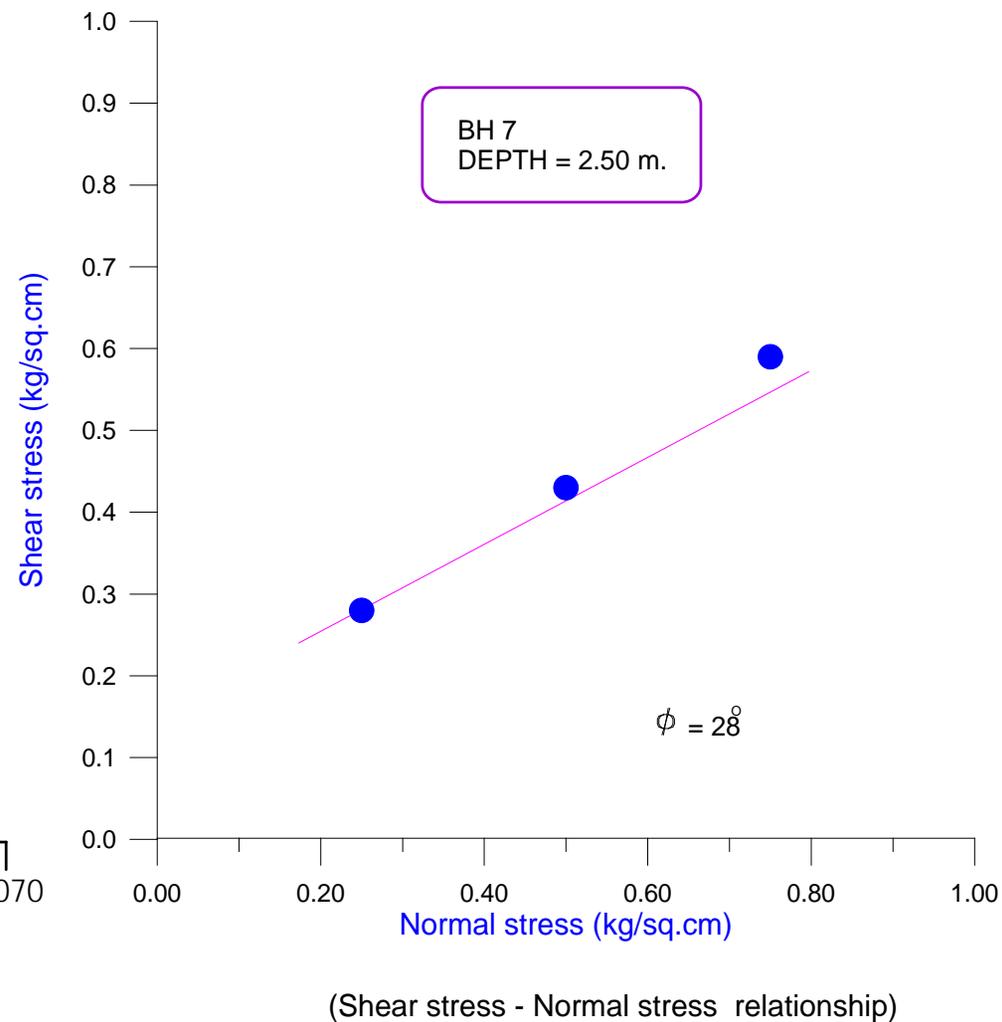
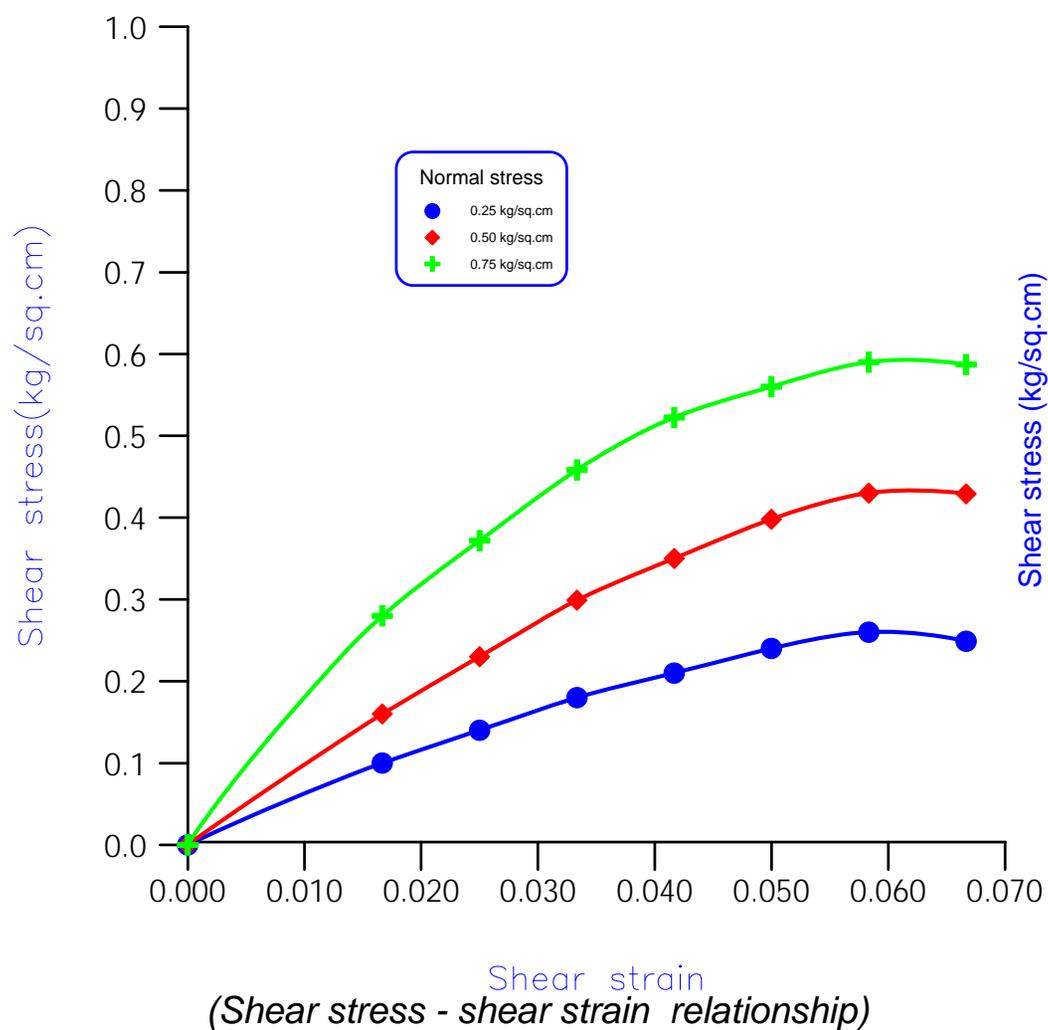




Soil Engineering Constants

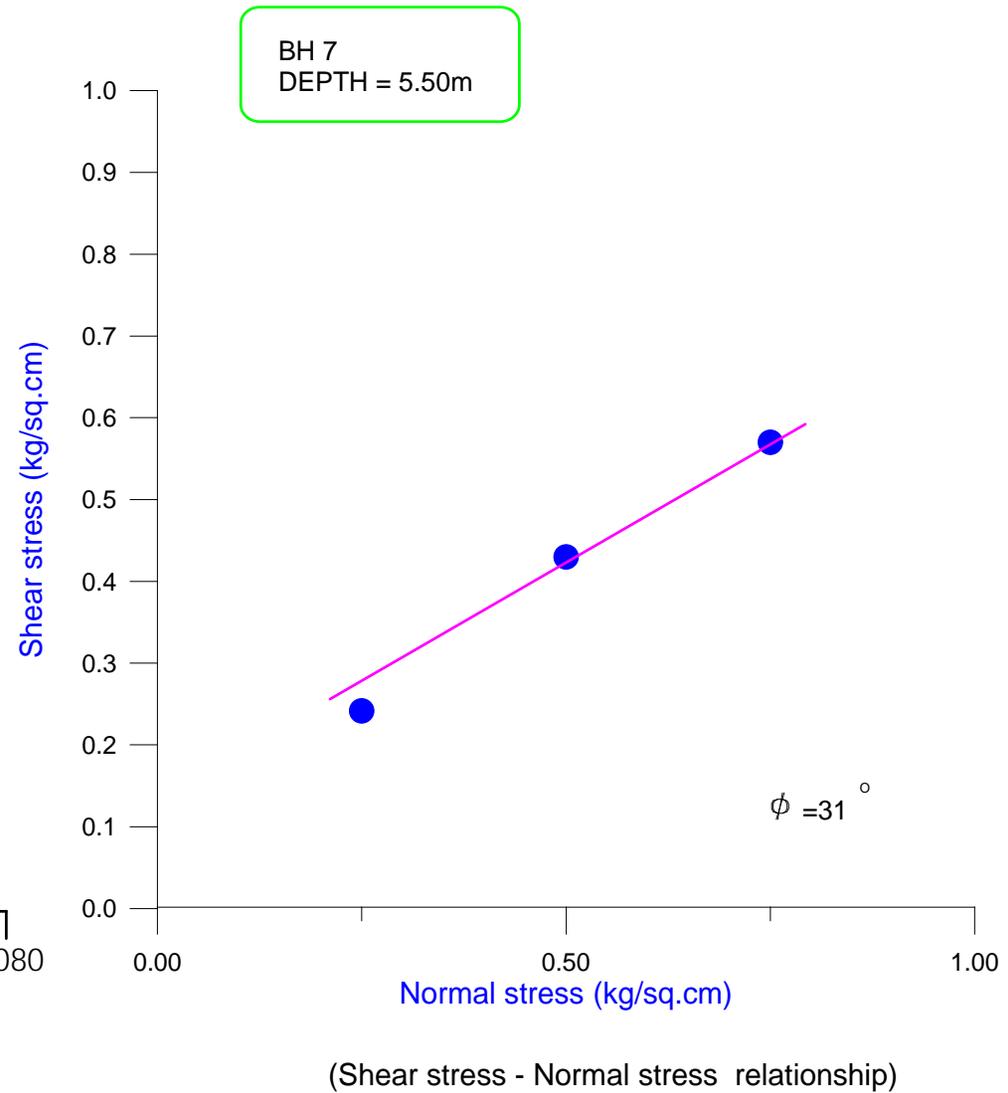
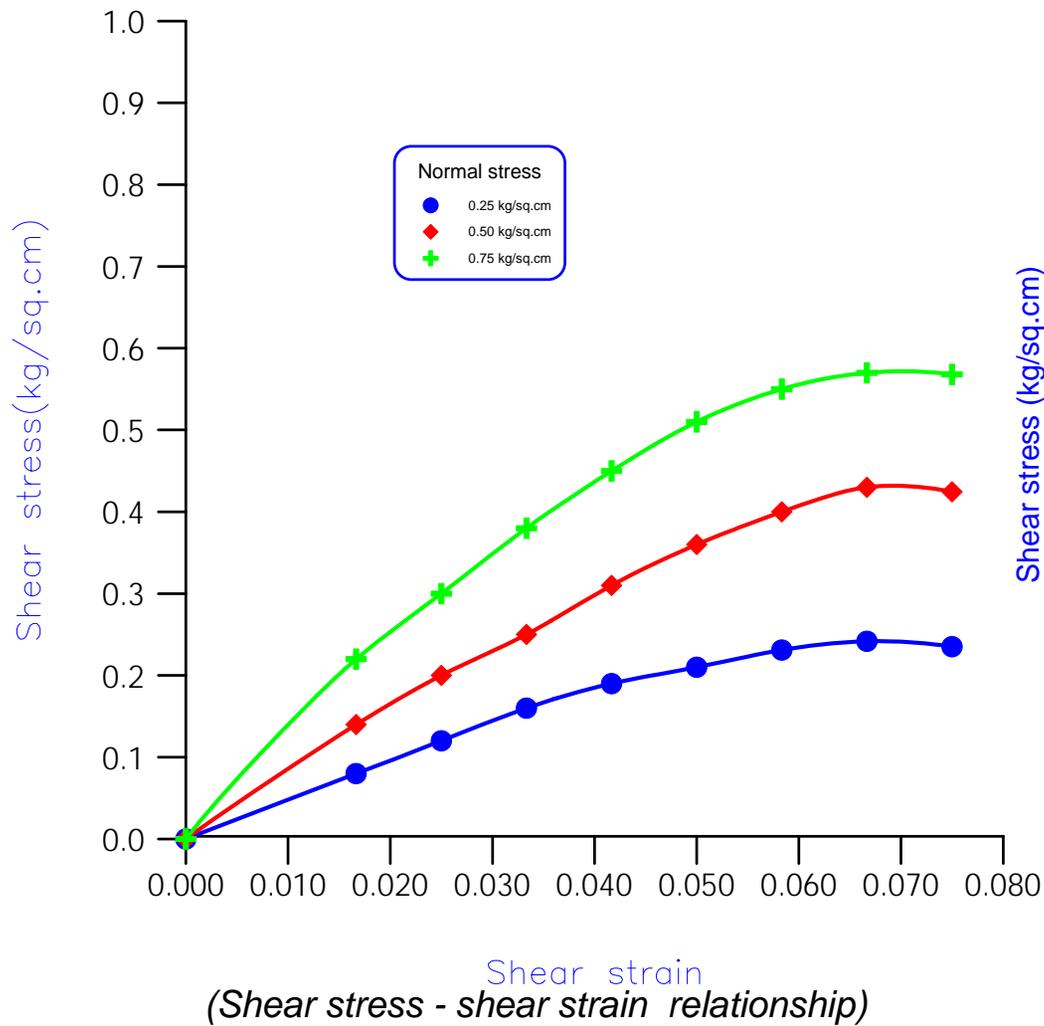
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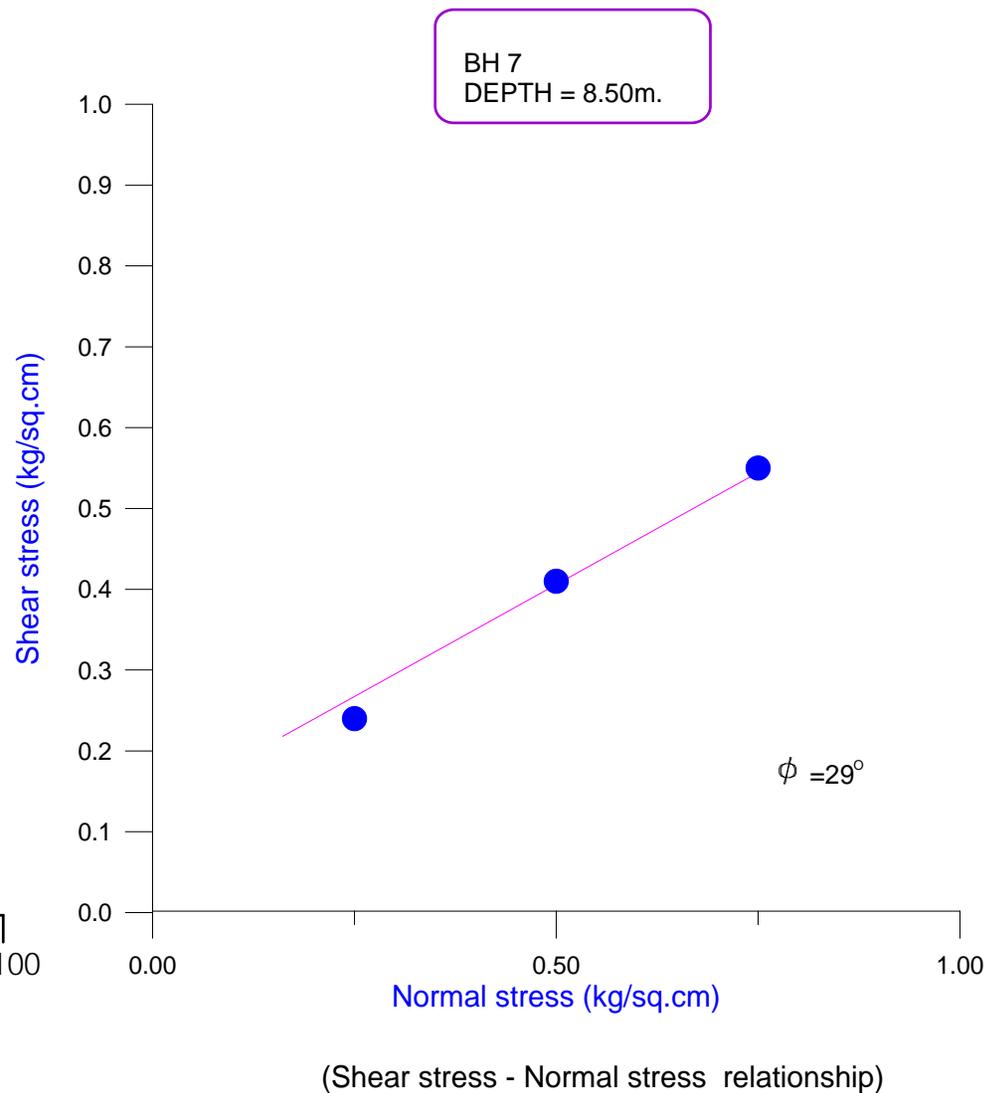
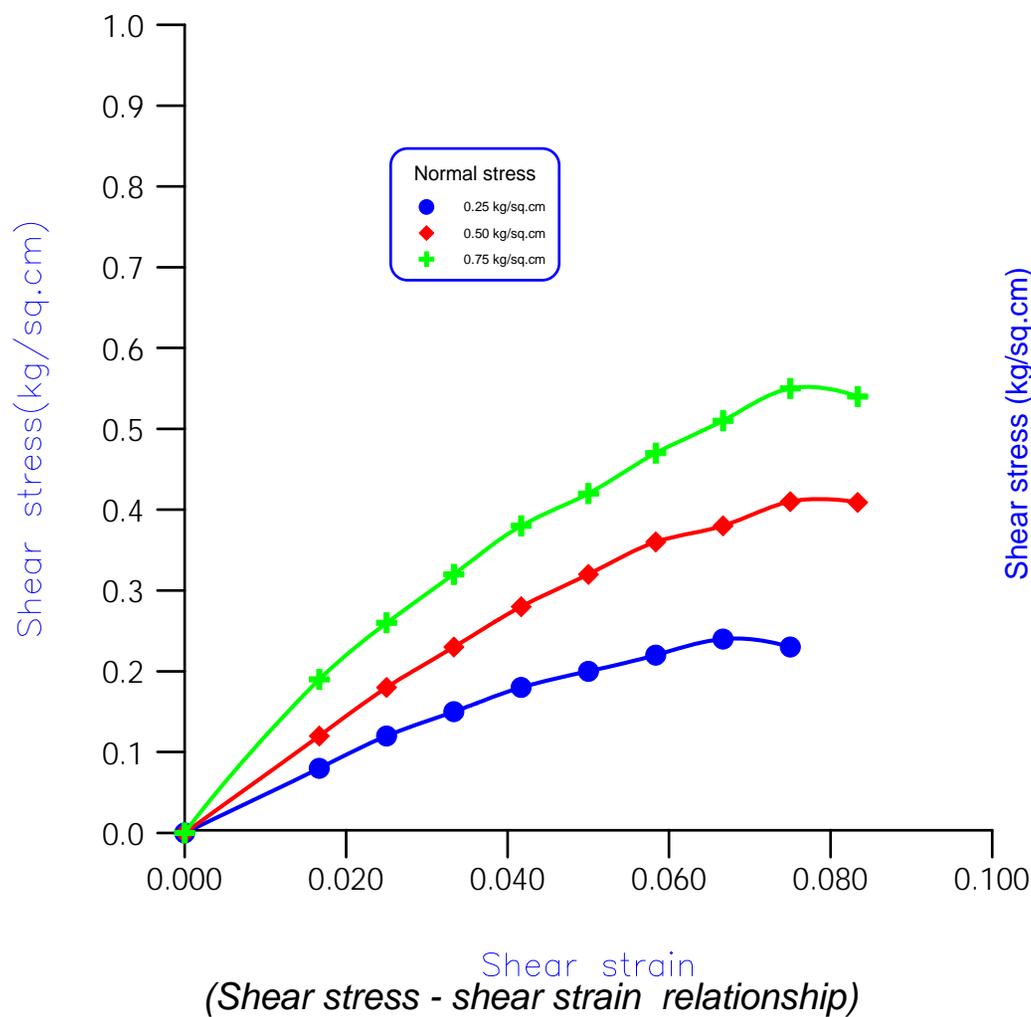
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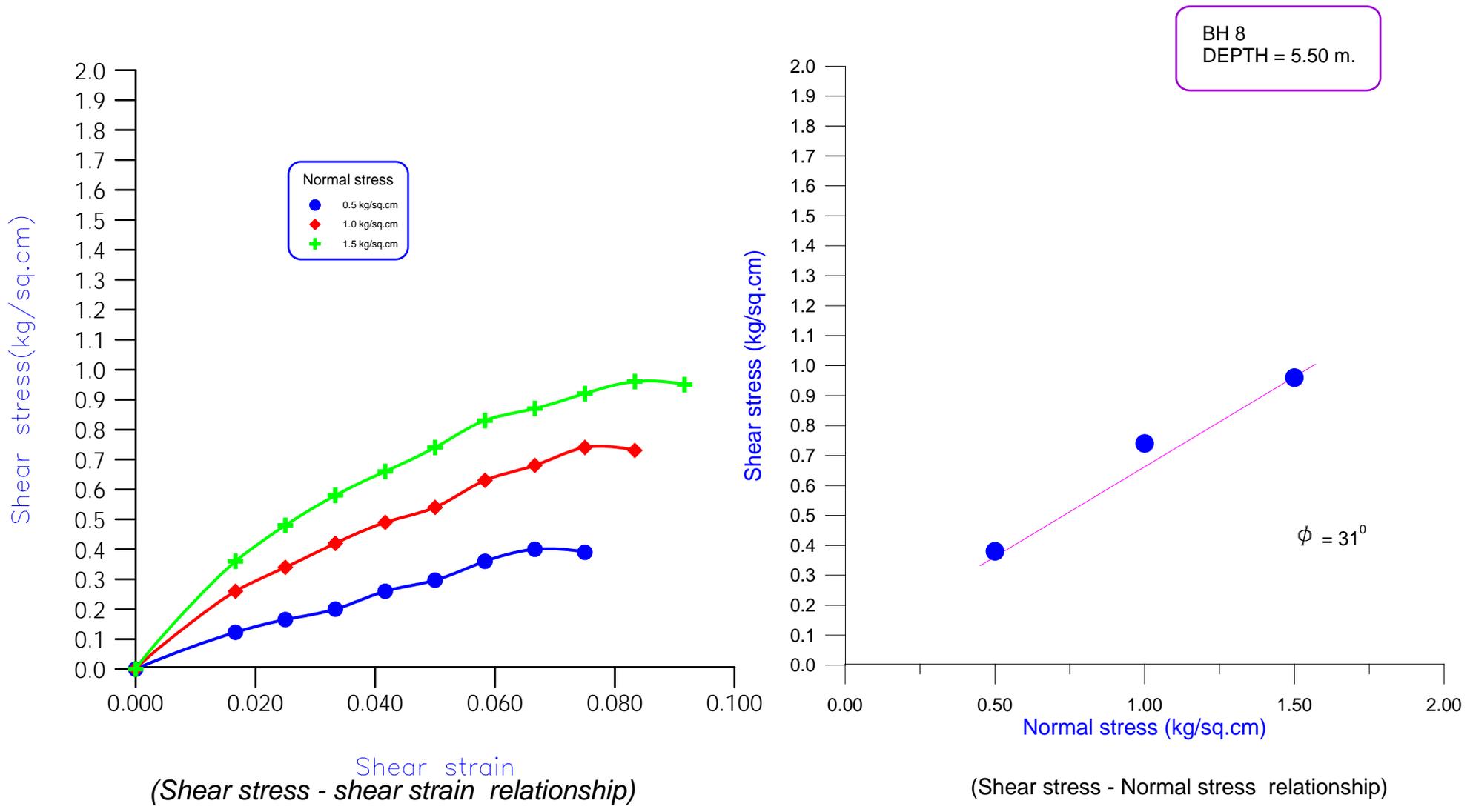
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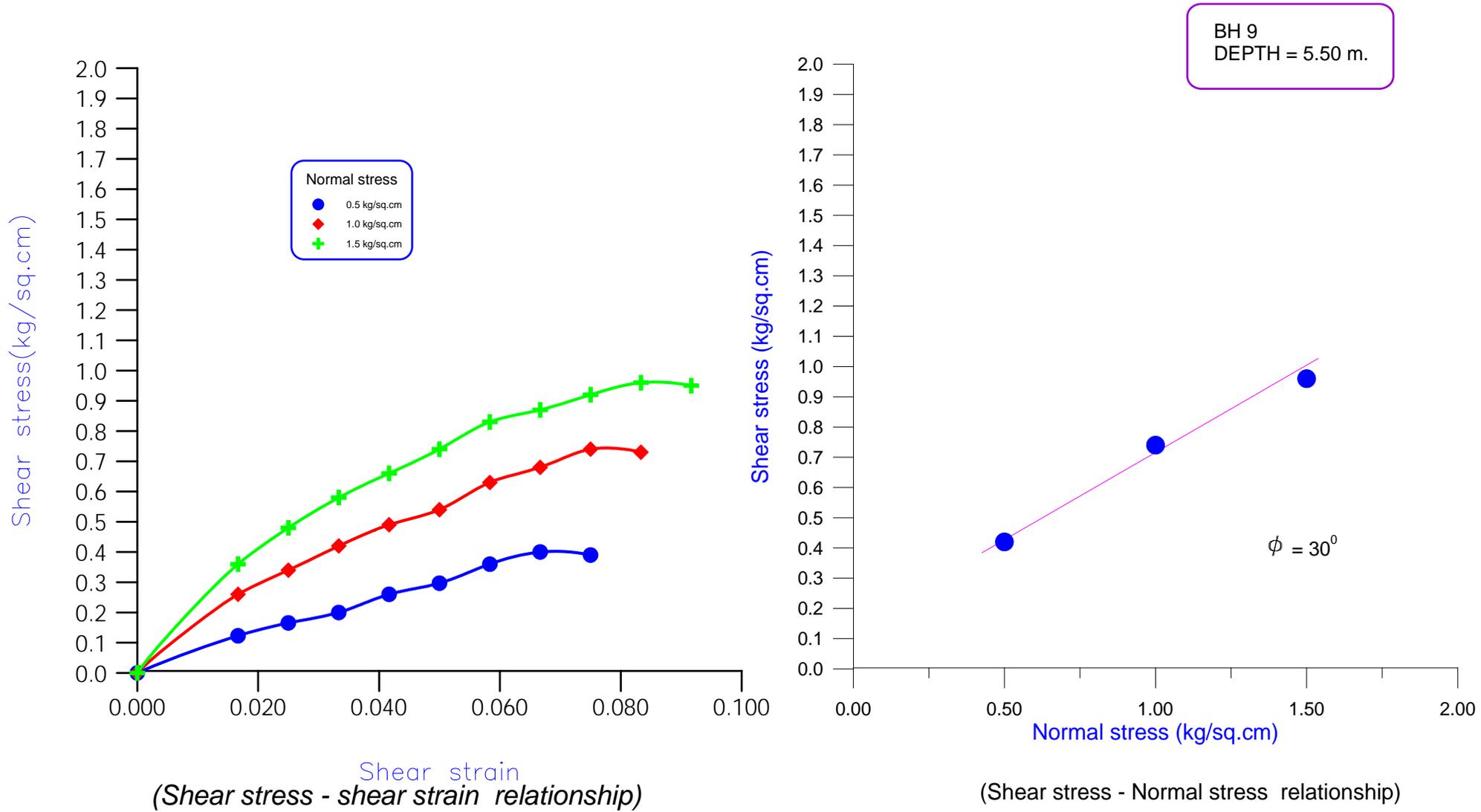
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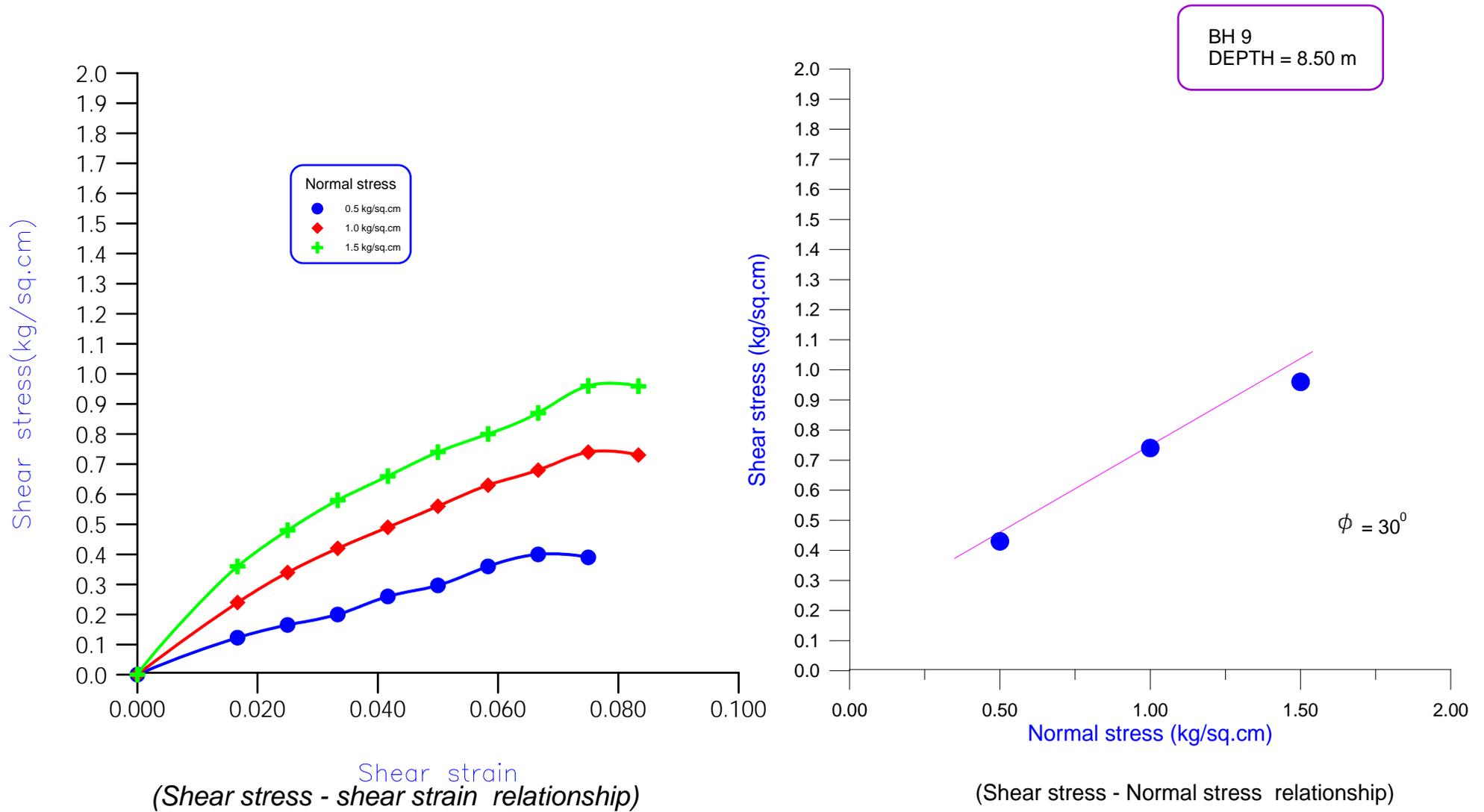
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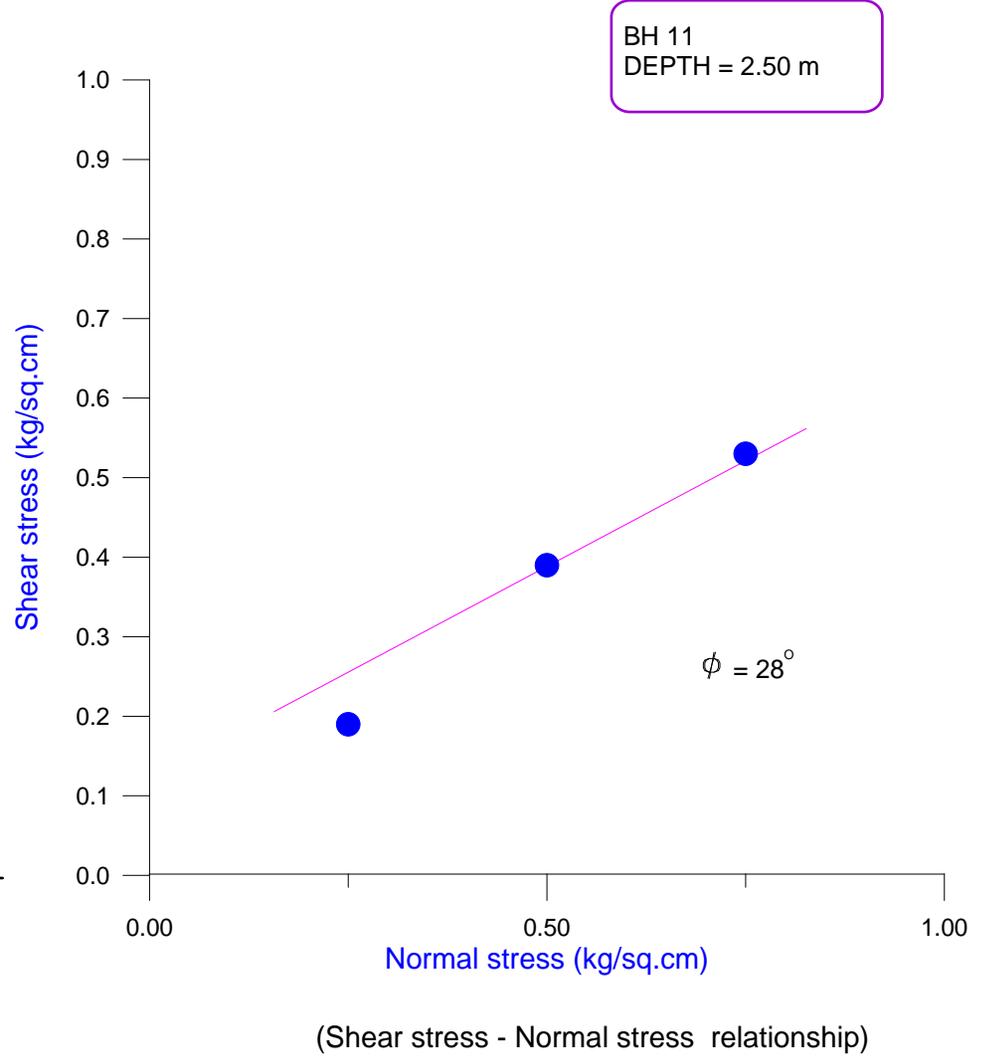
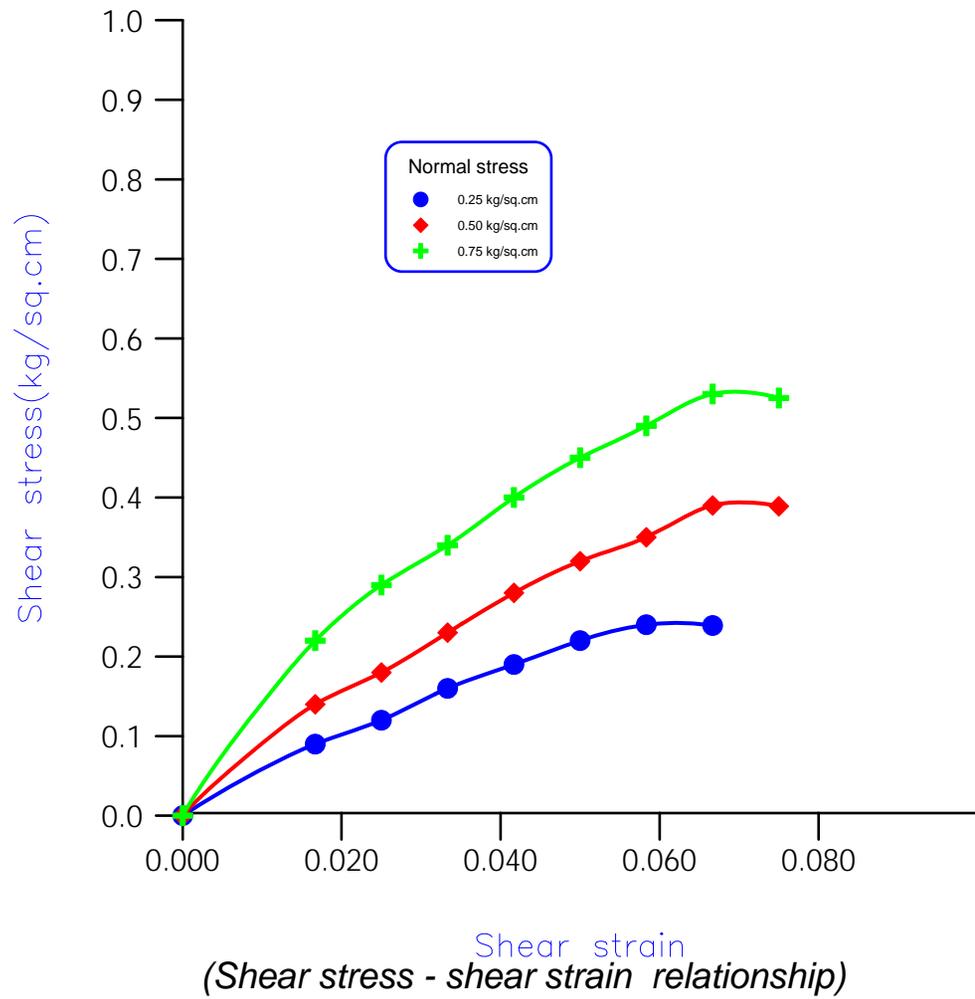


Soil Engineering Constants

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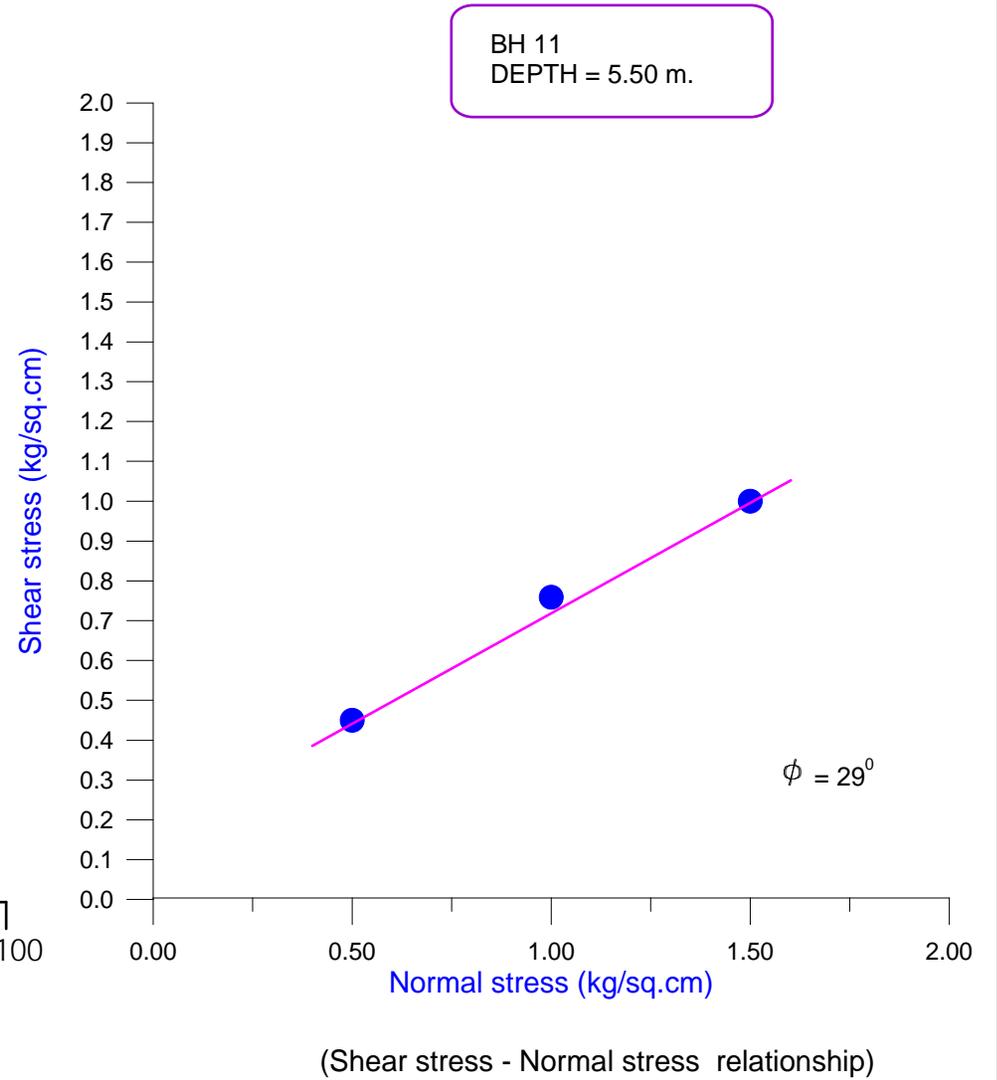
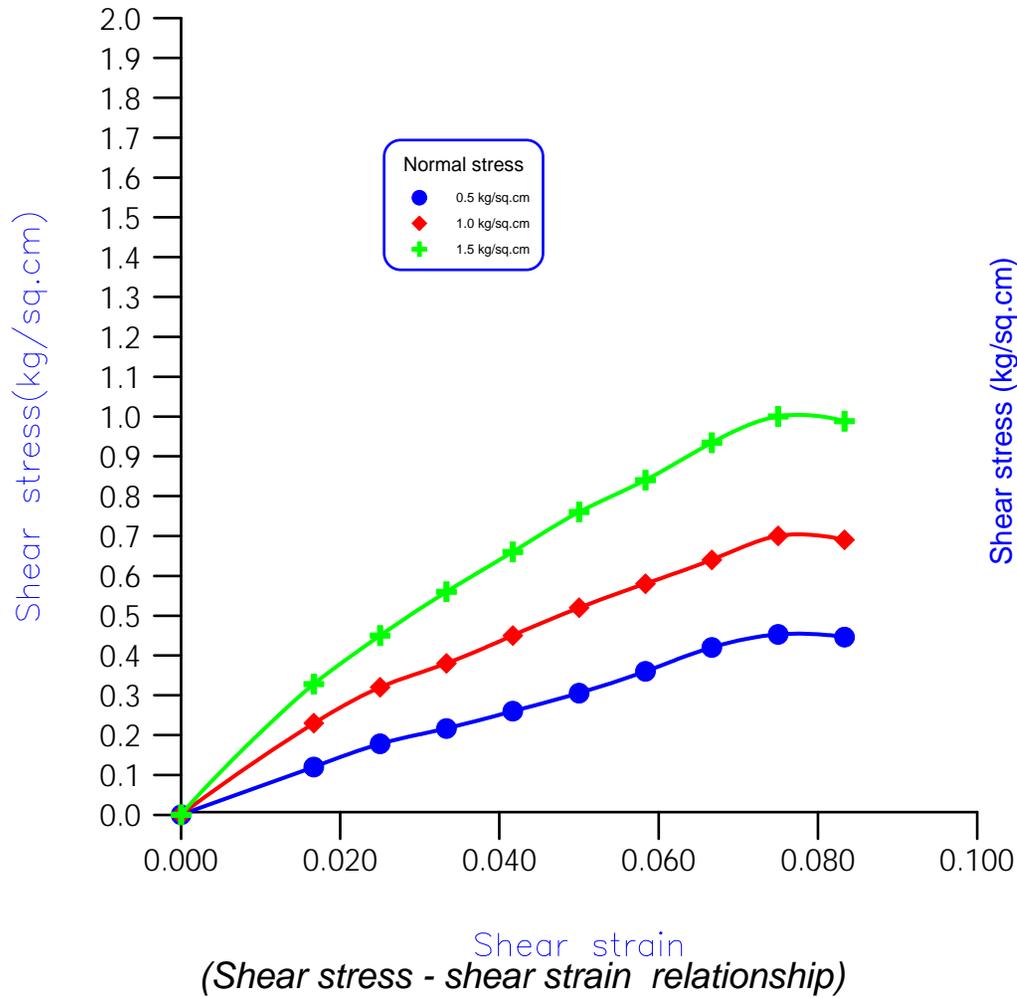






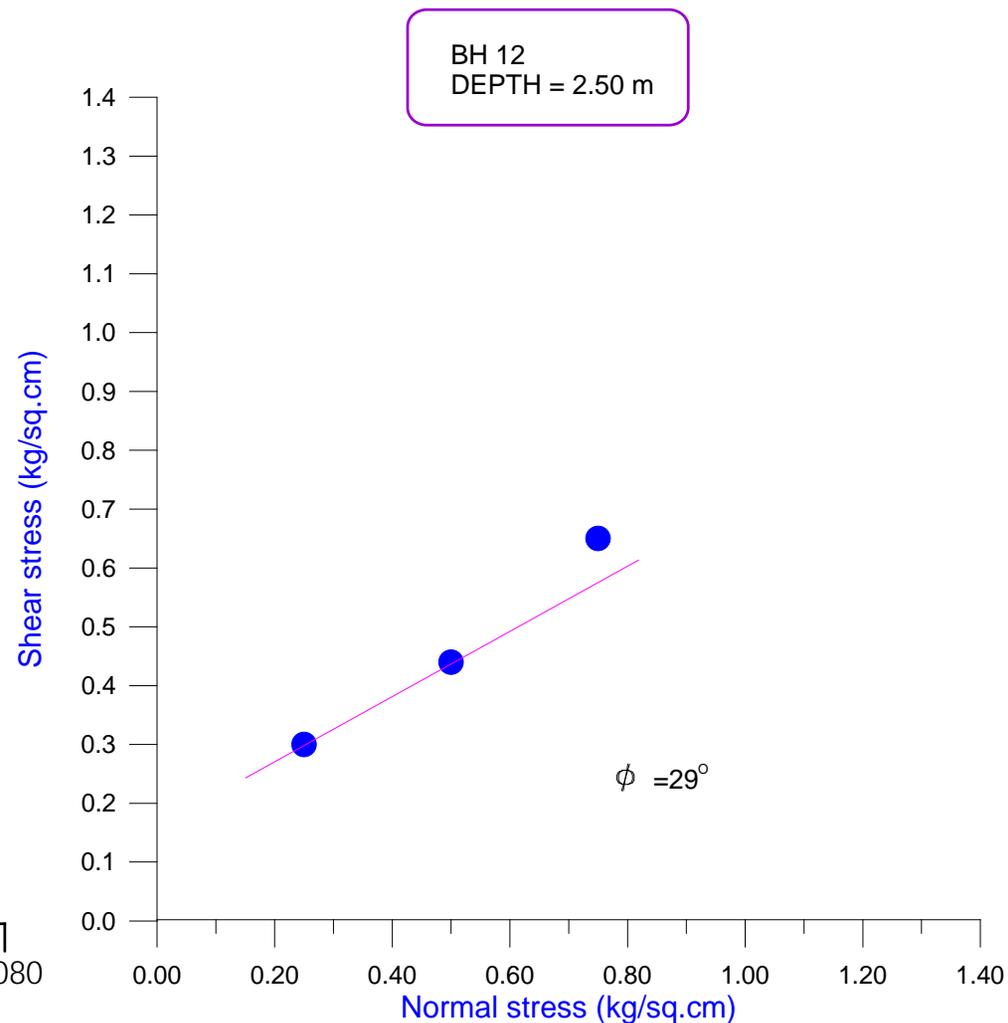
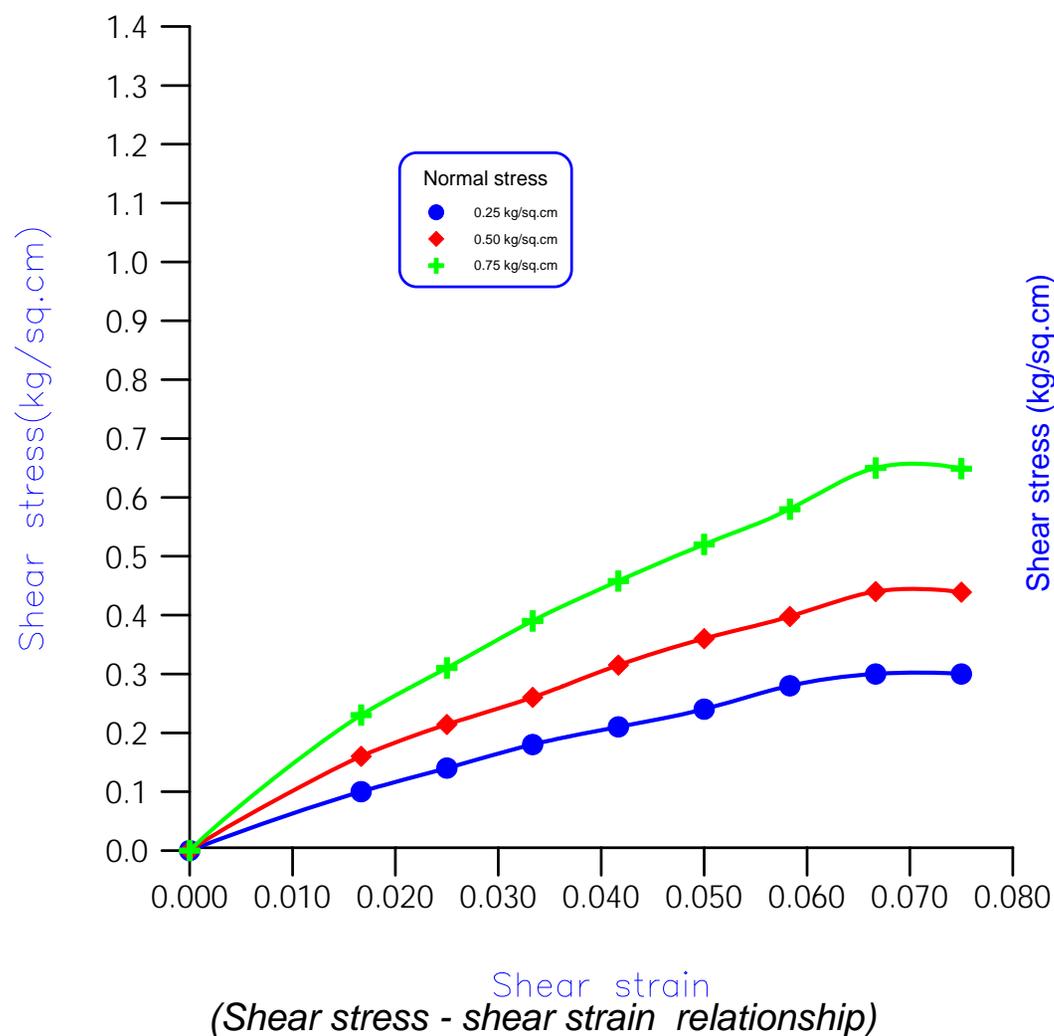
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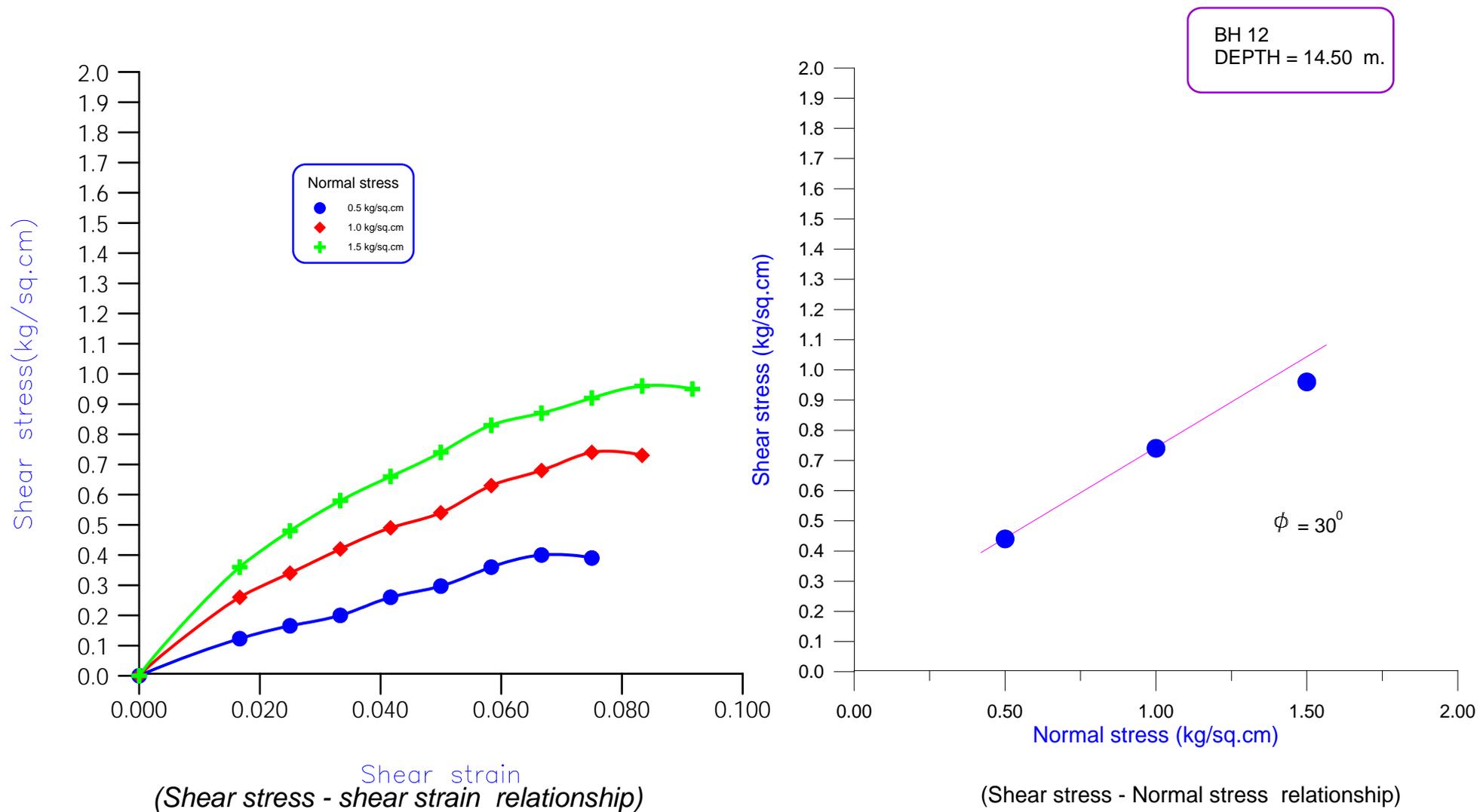
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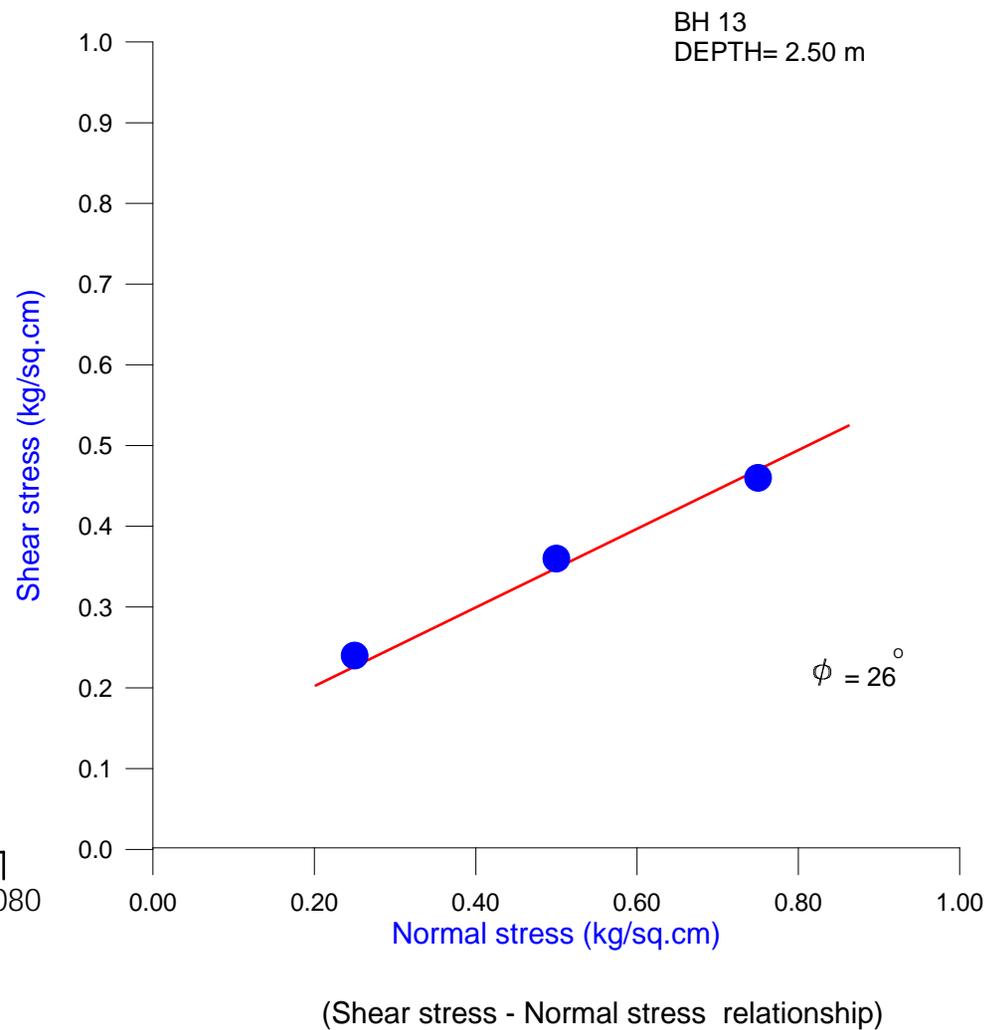
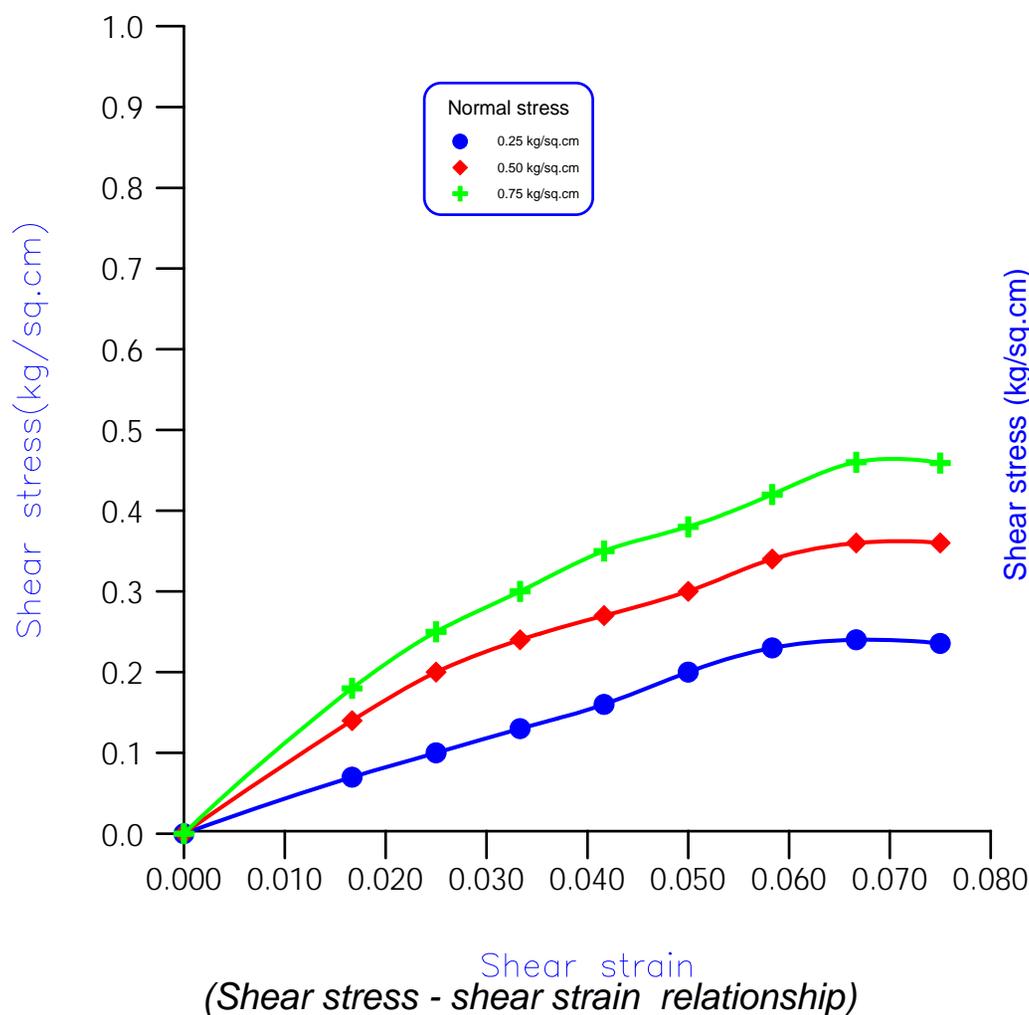
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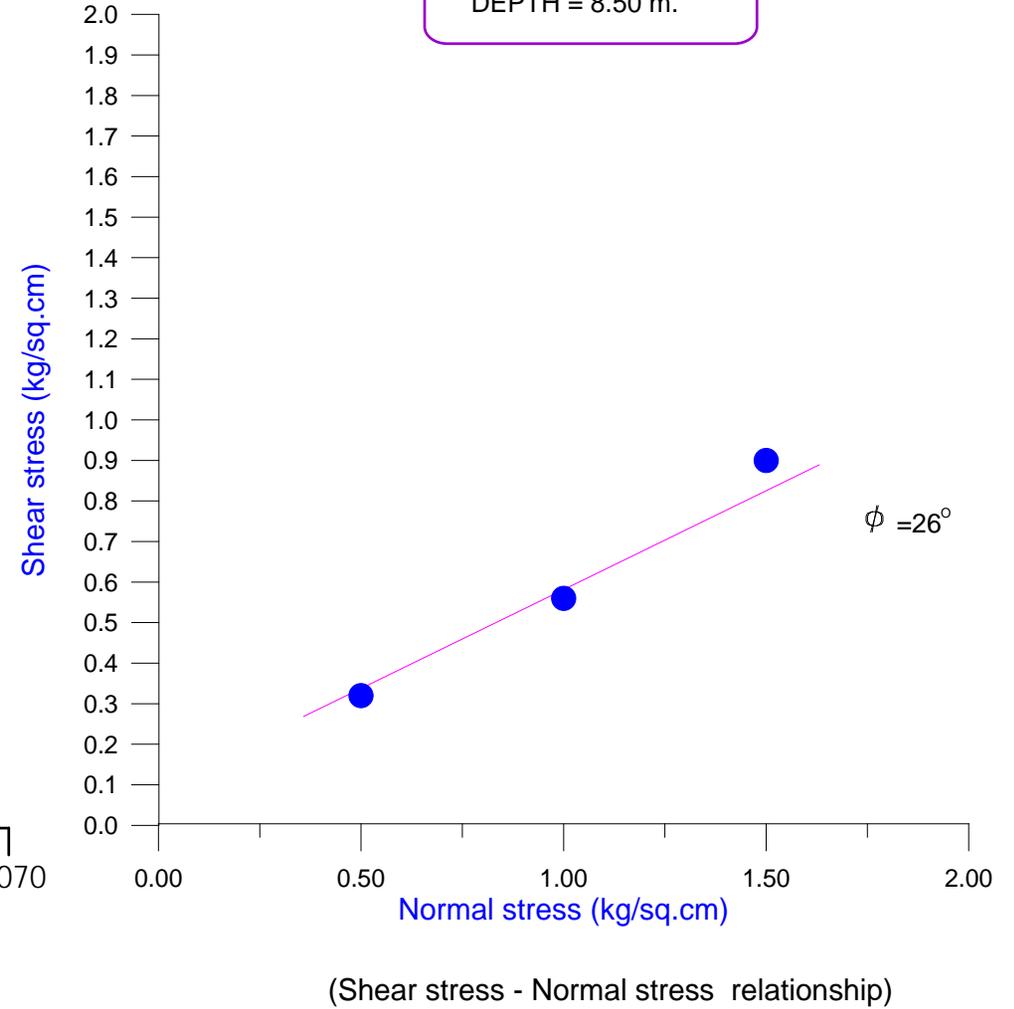
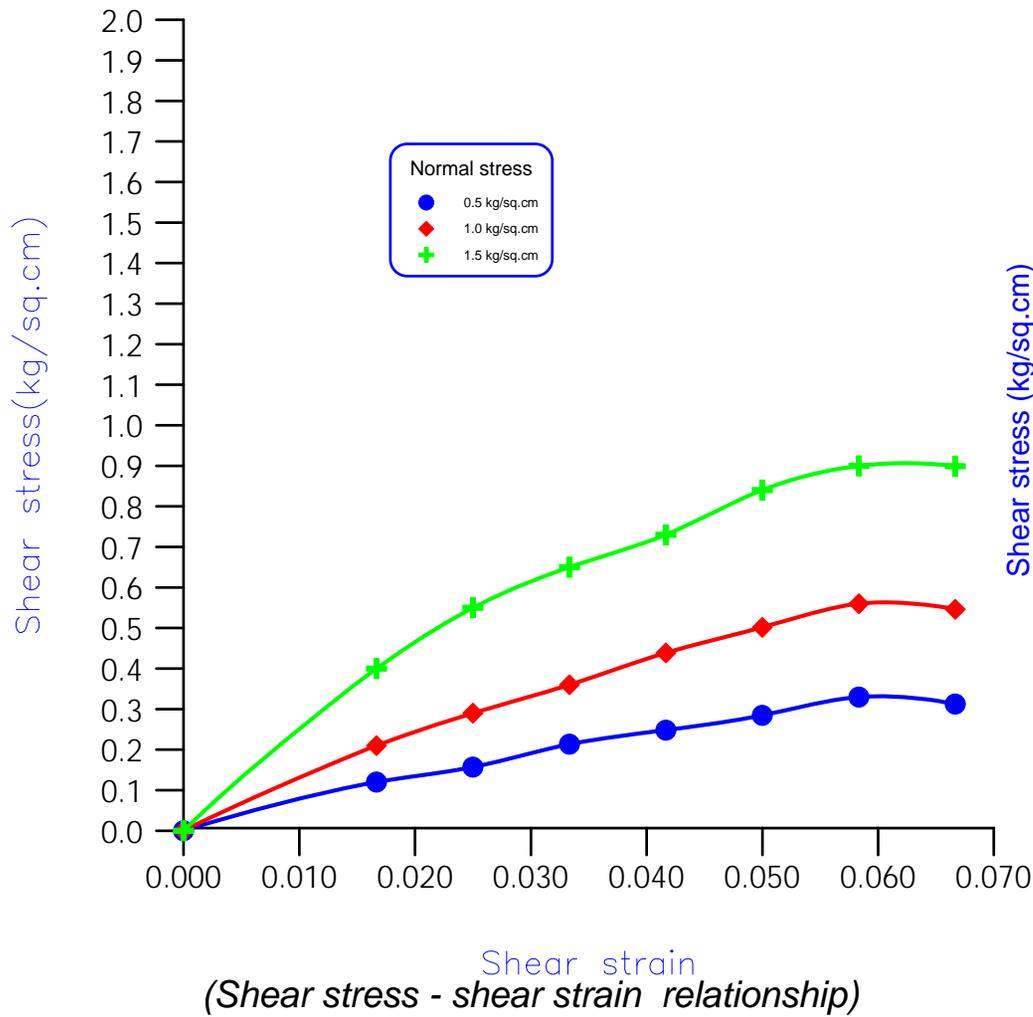
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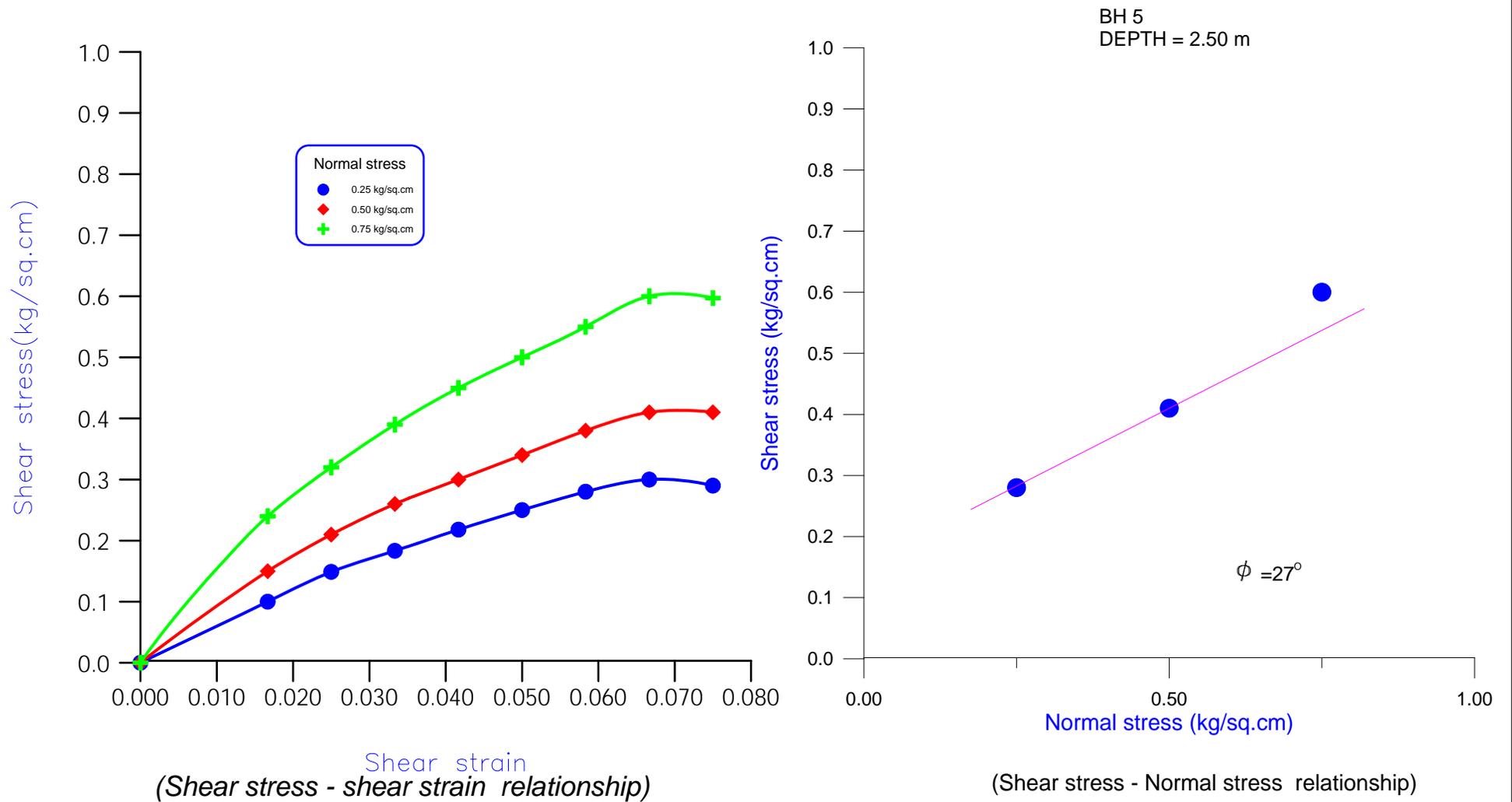
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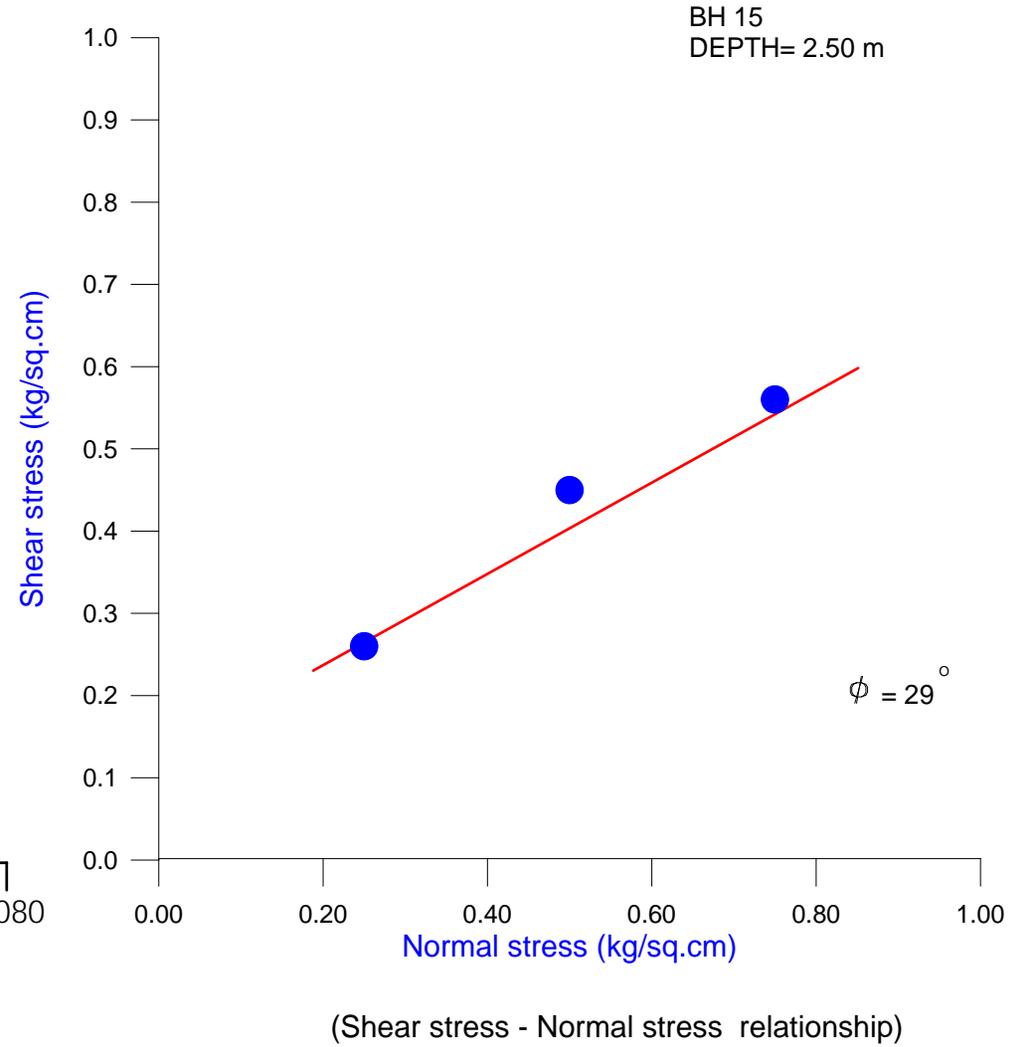
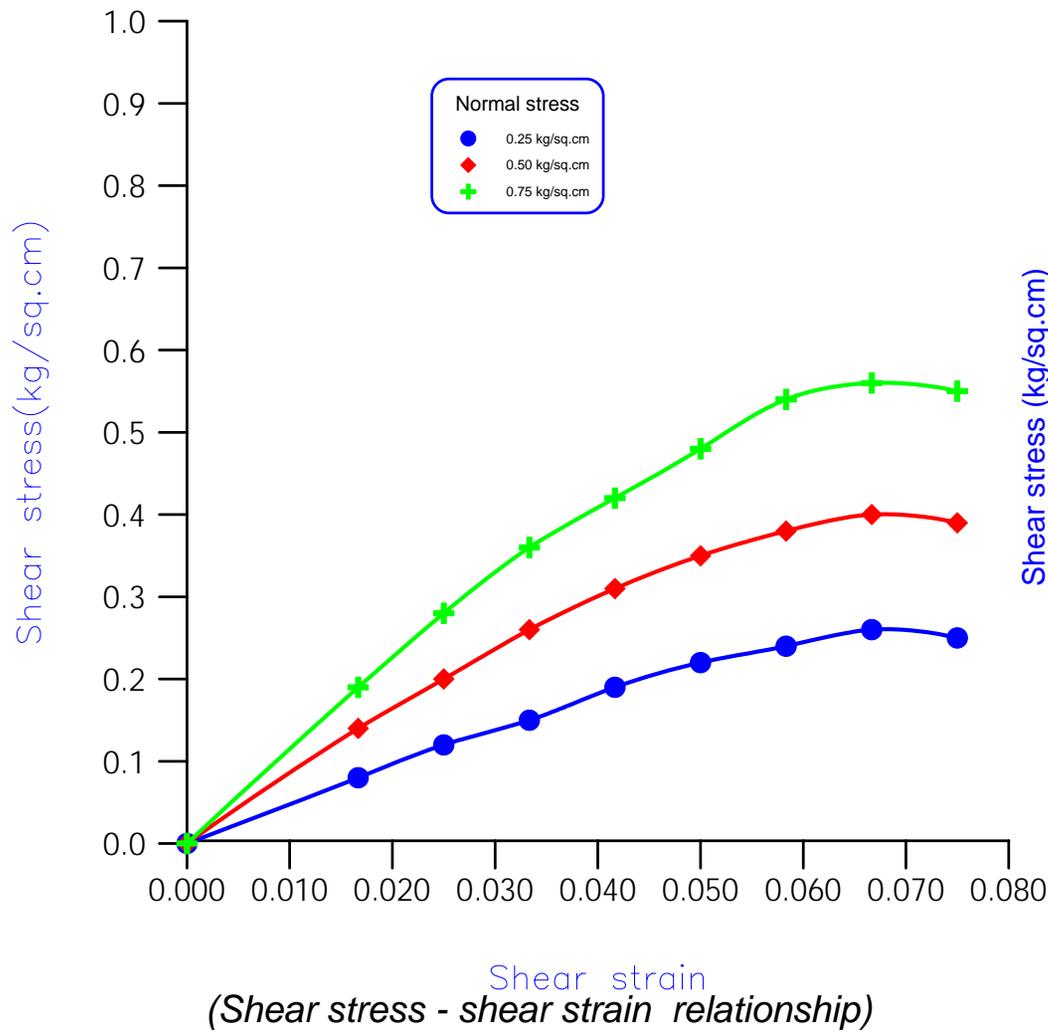
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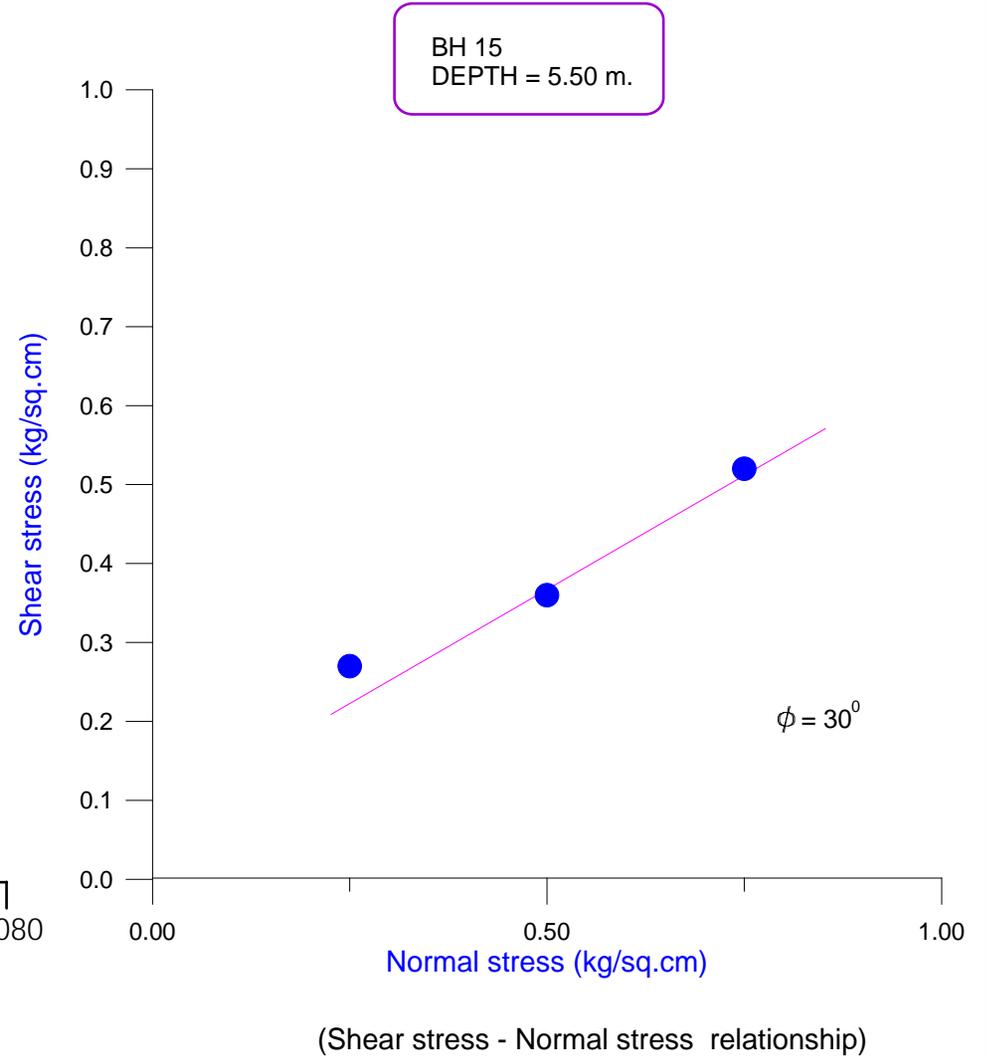
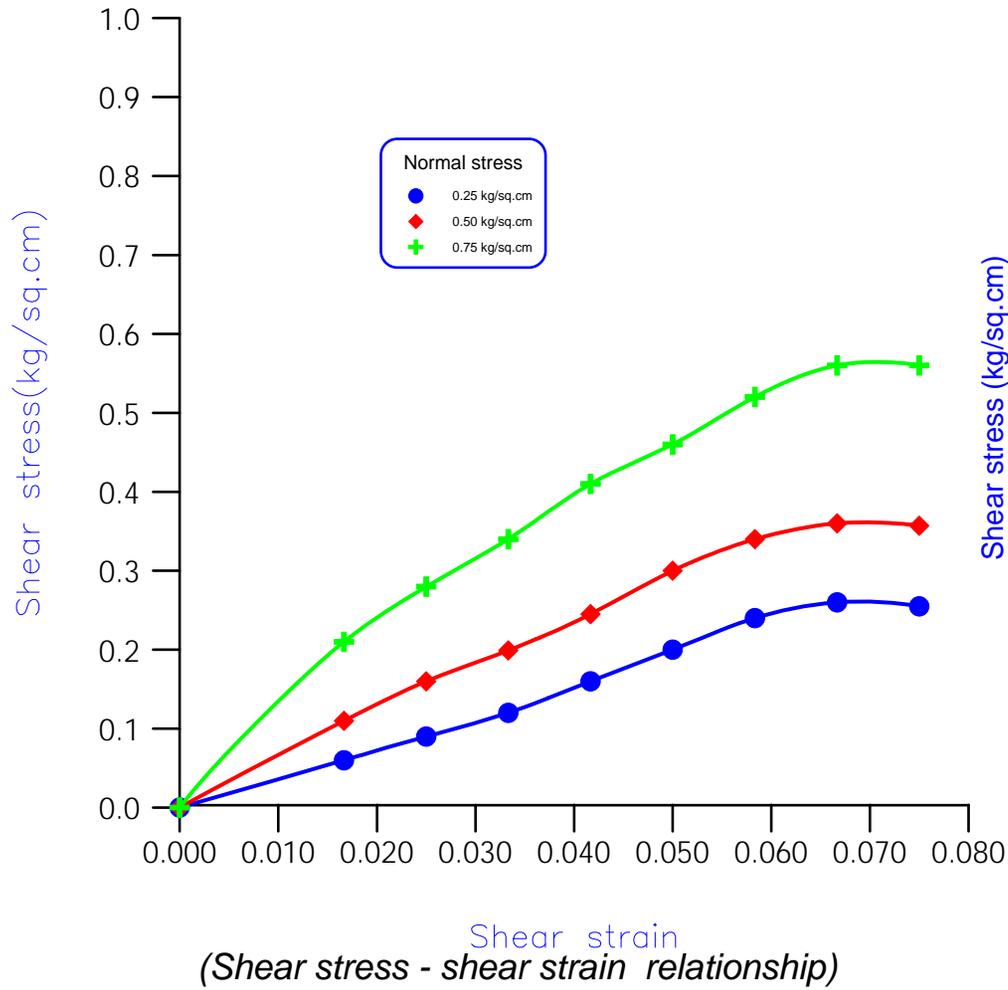
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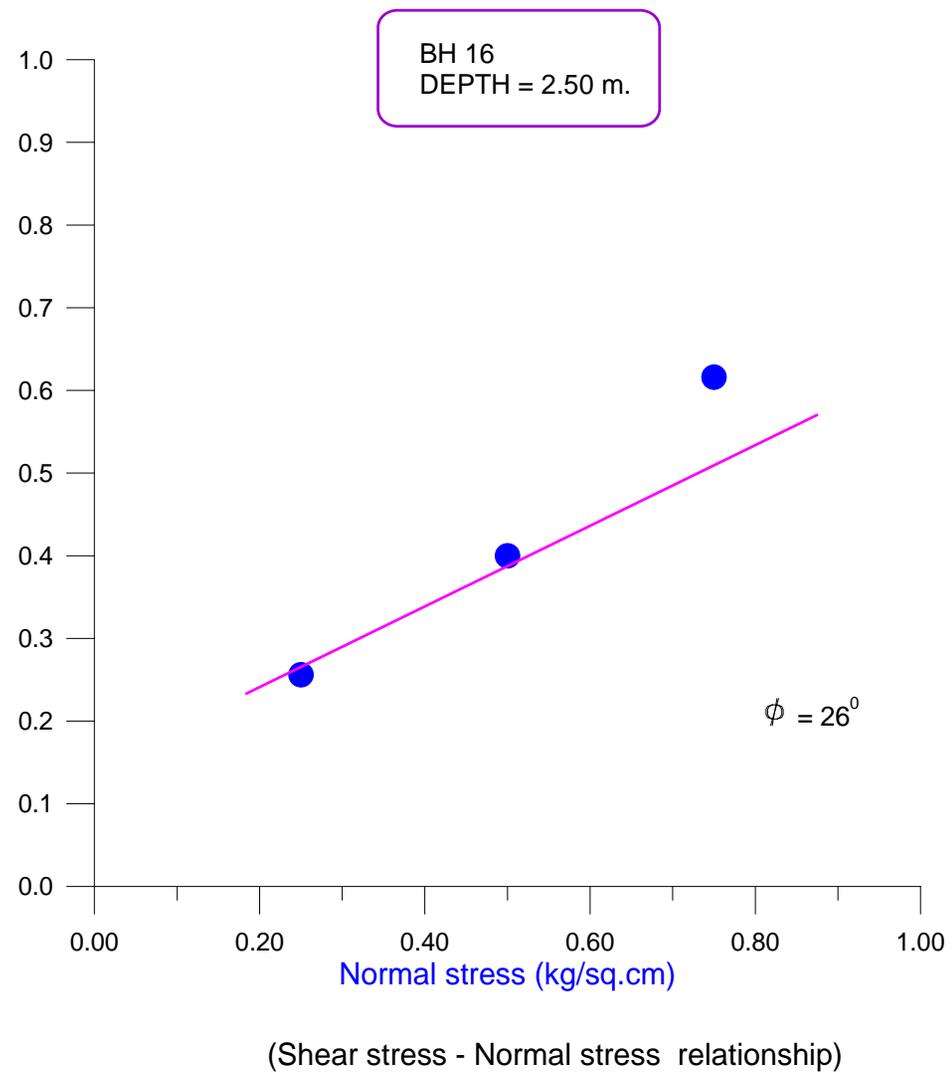
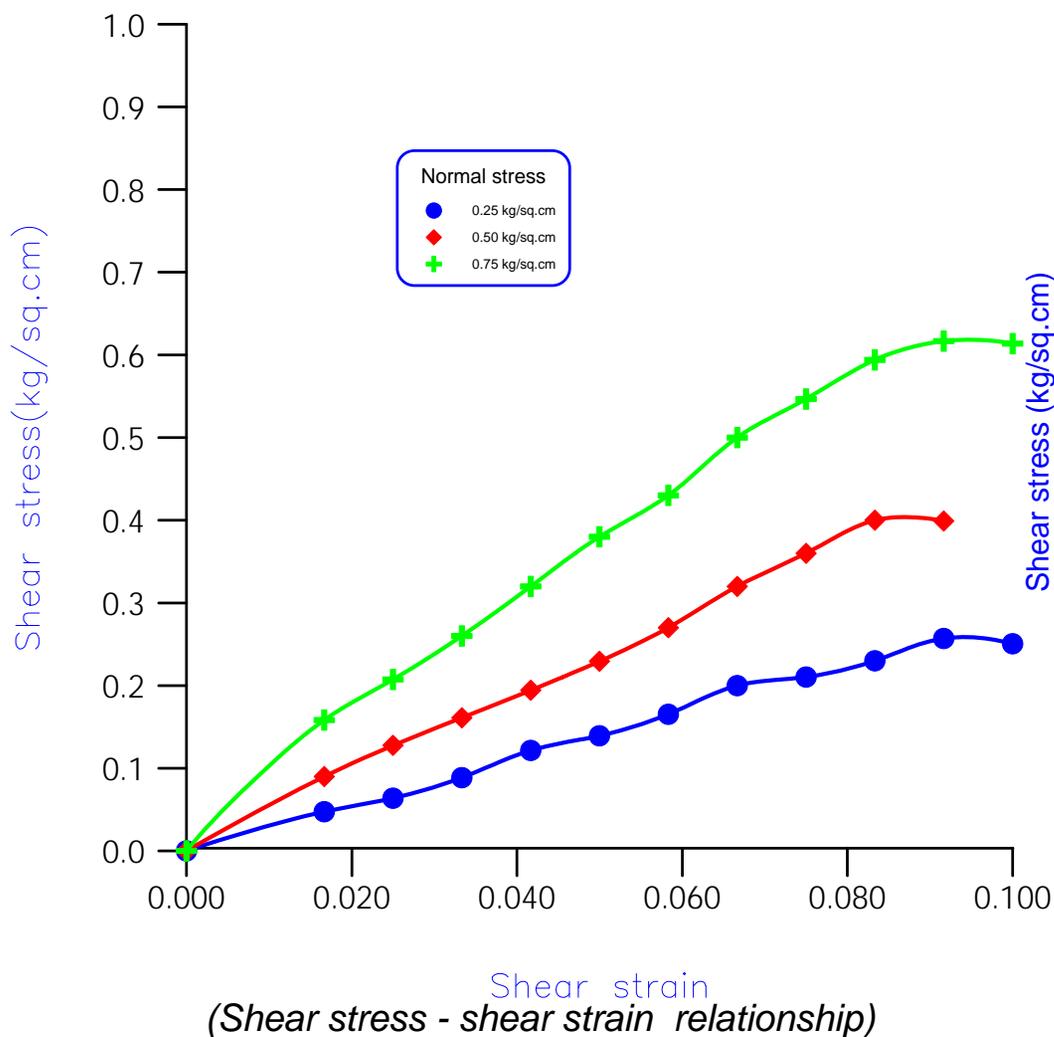
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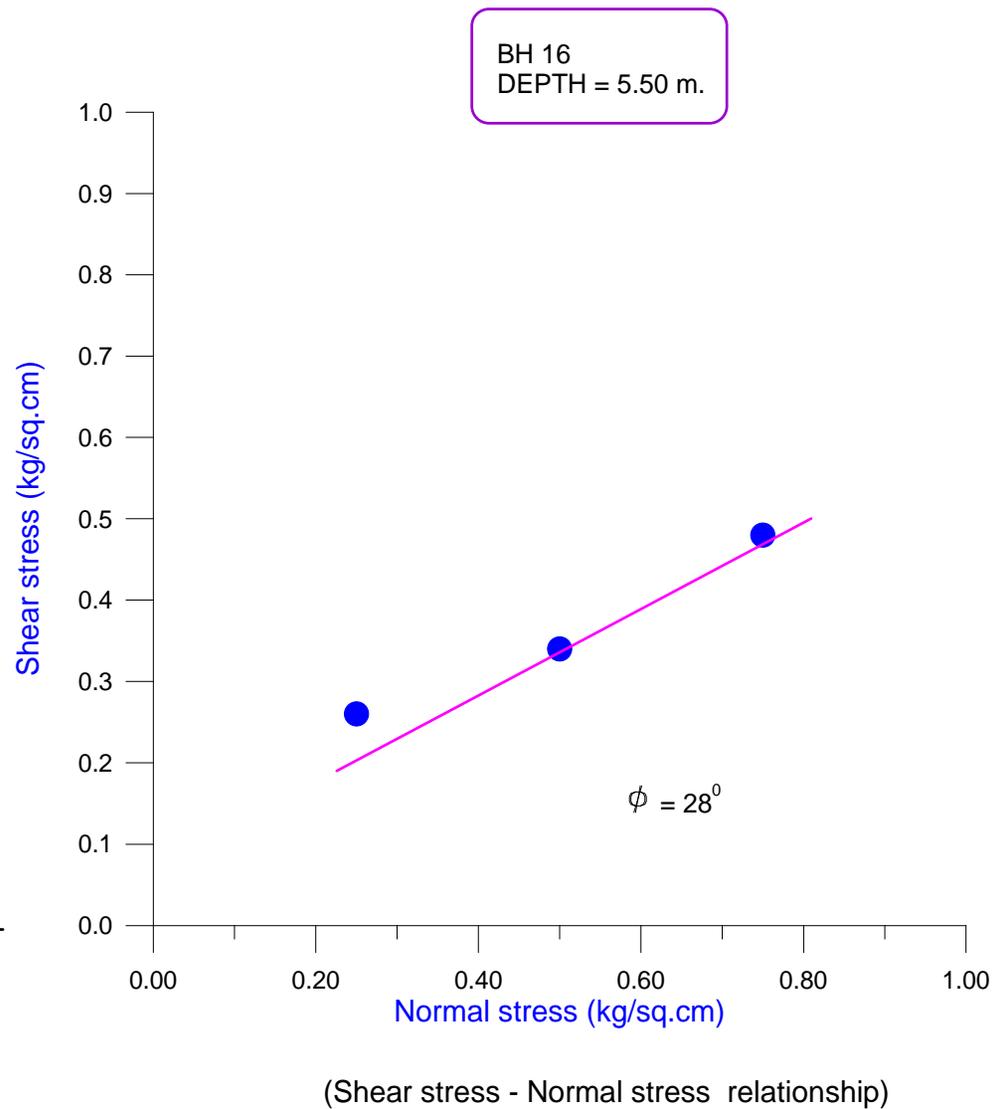
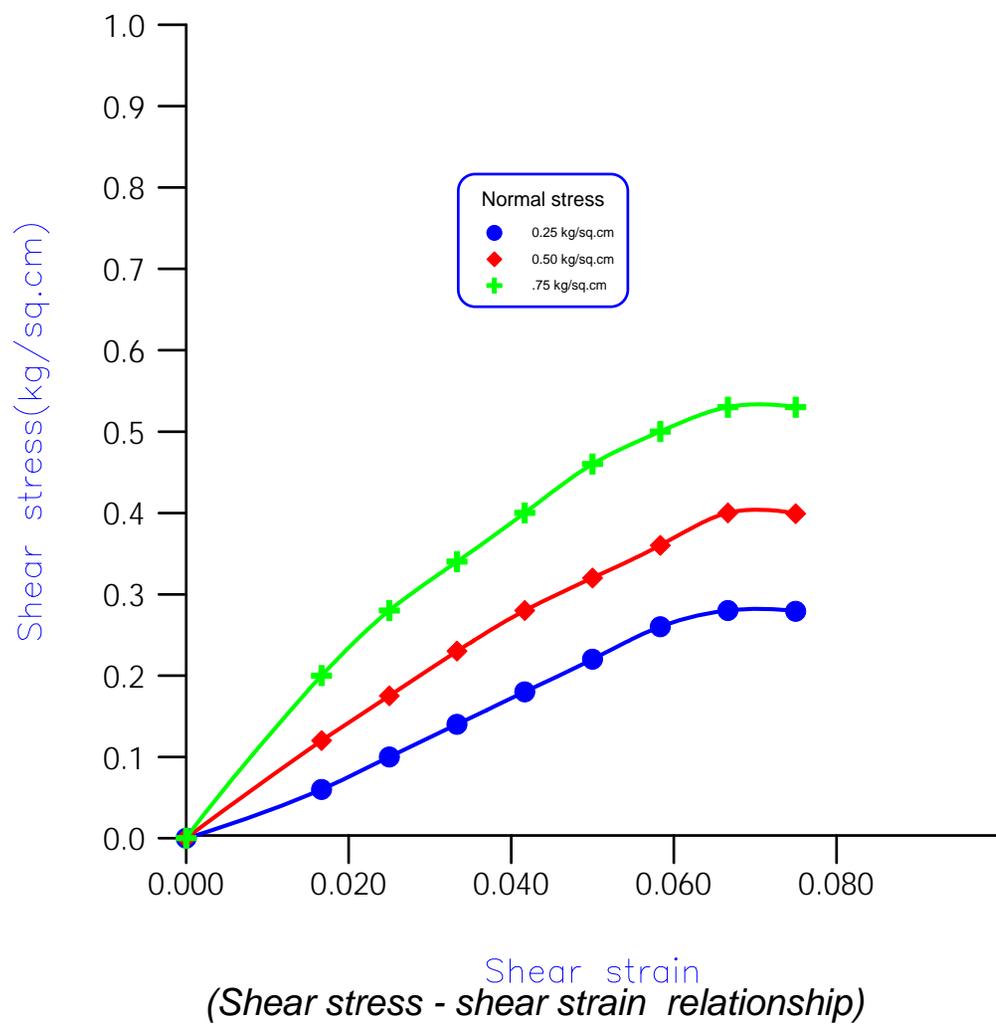
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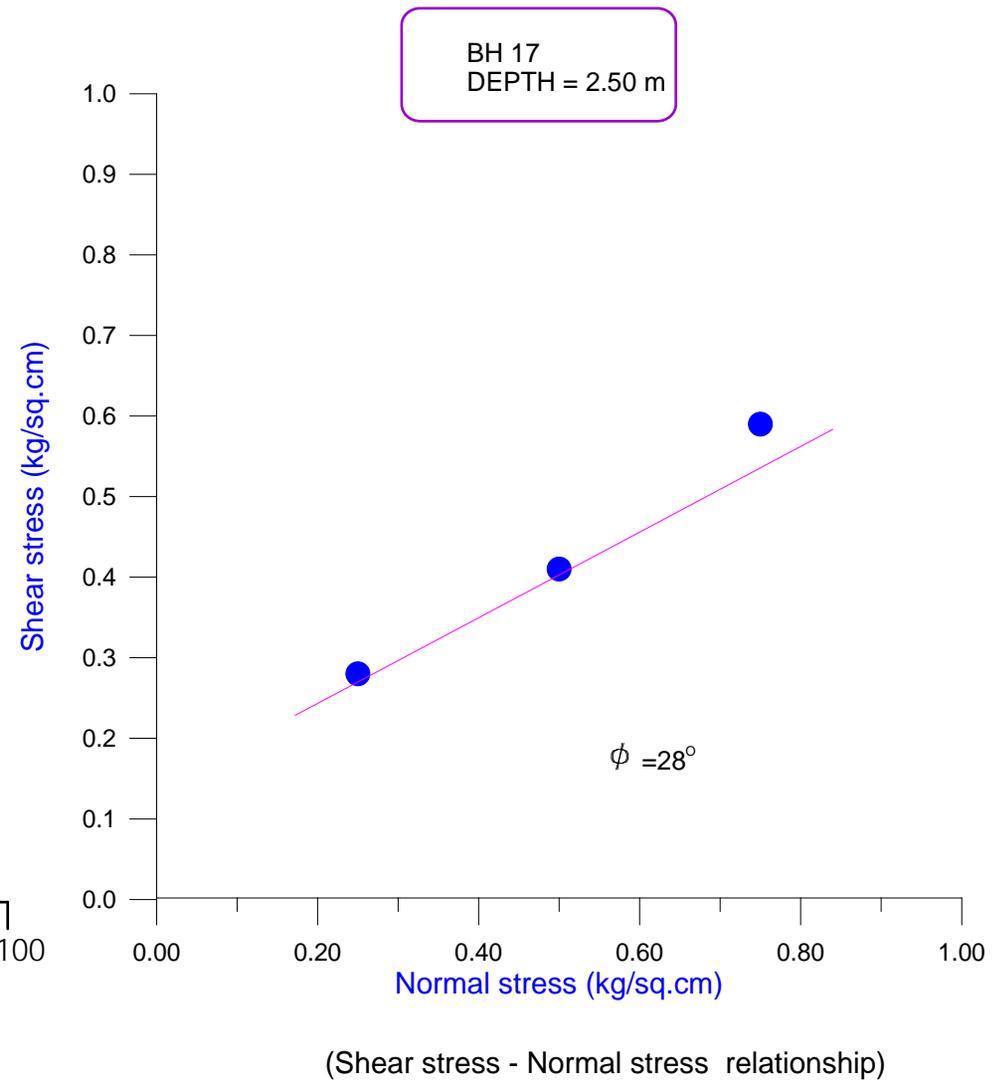
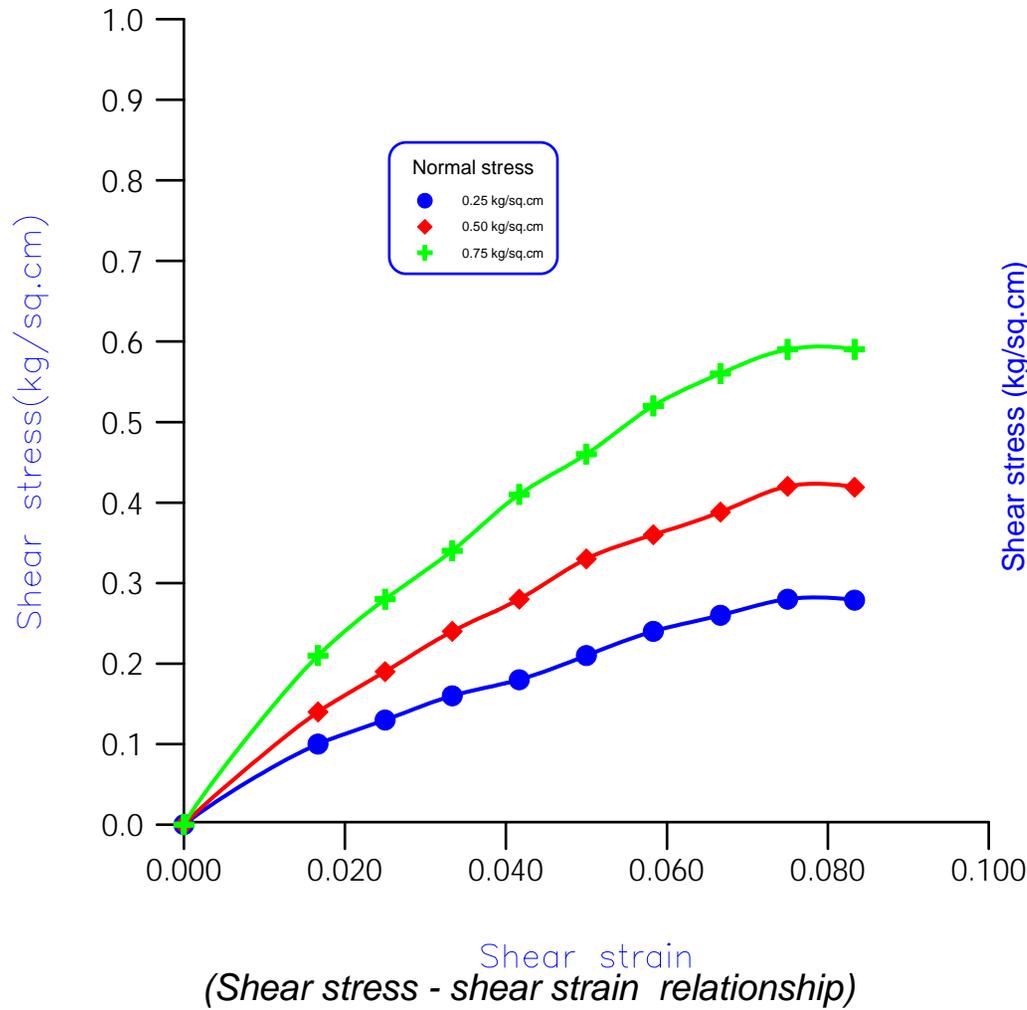
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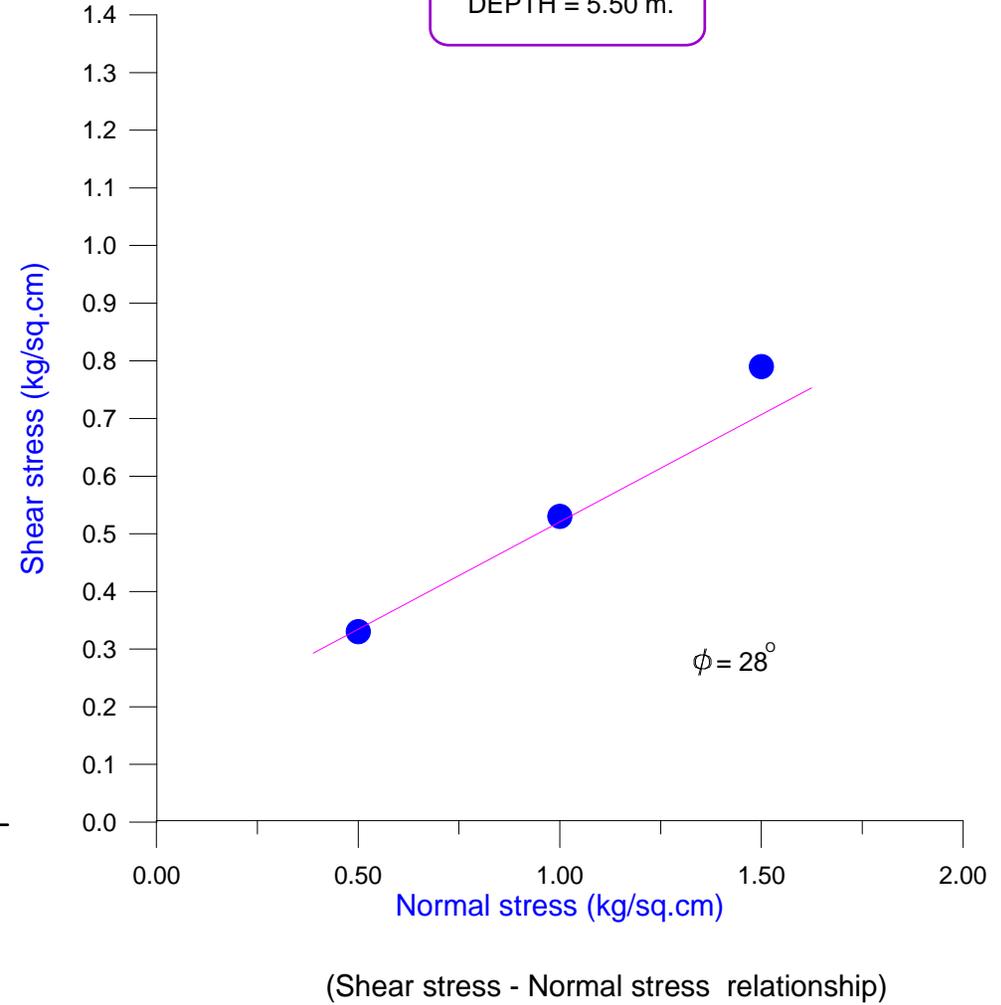
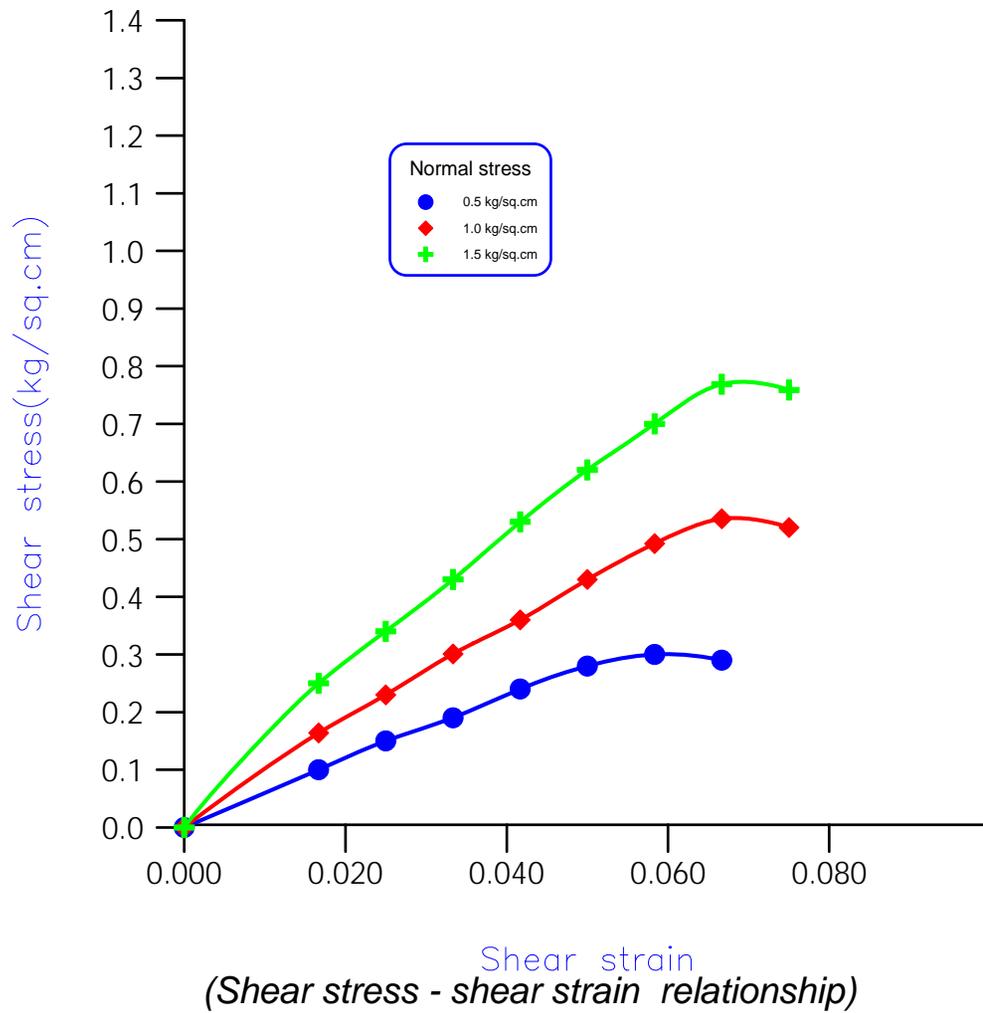
Soil Engineering Constants

Job. 2152



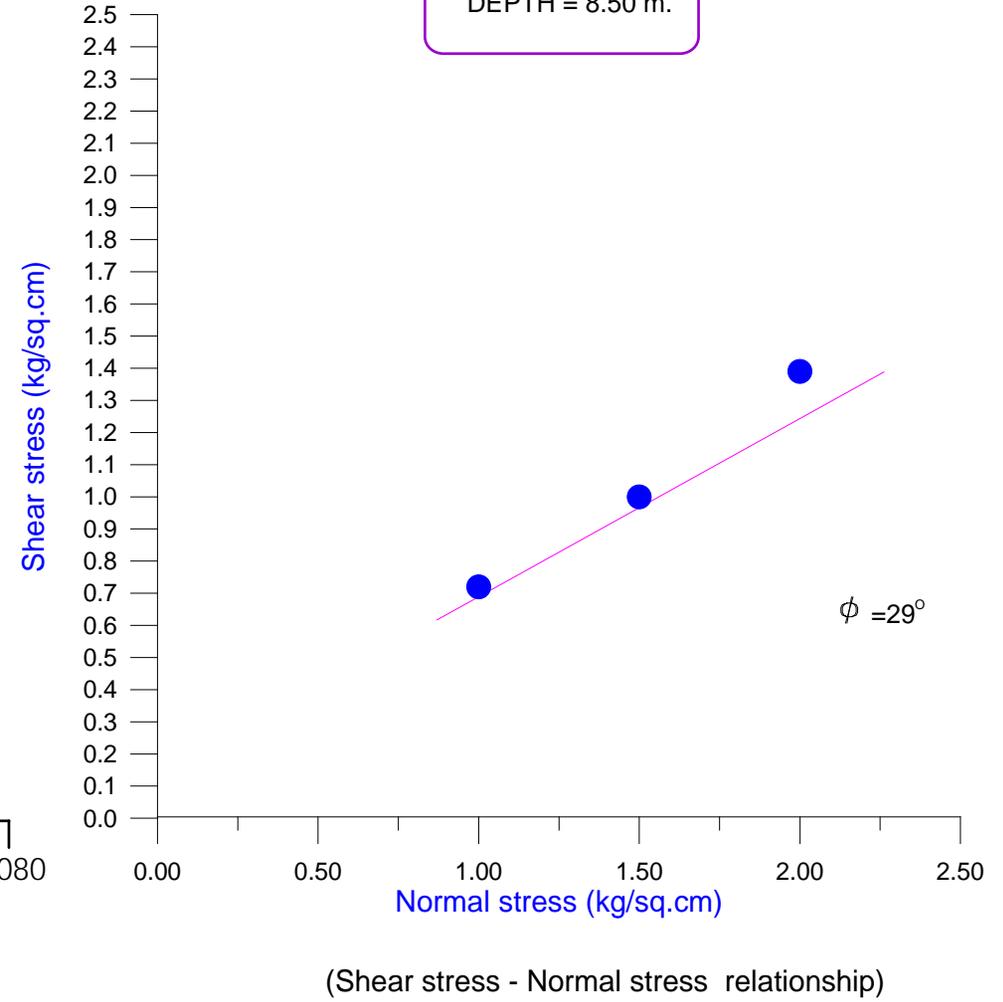
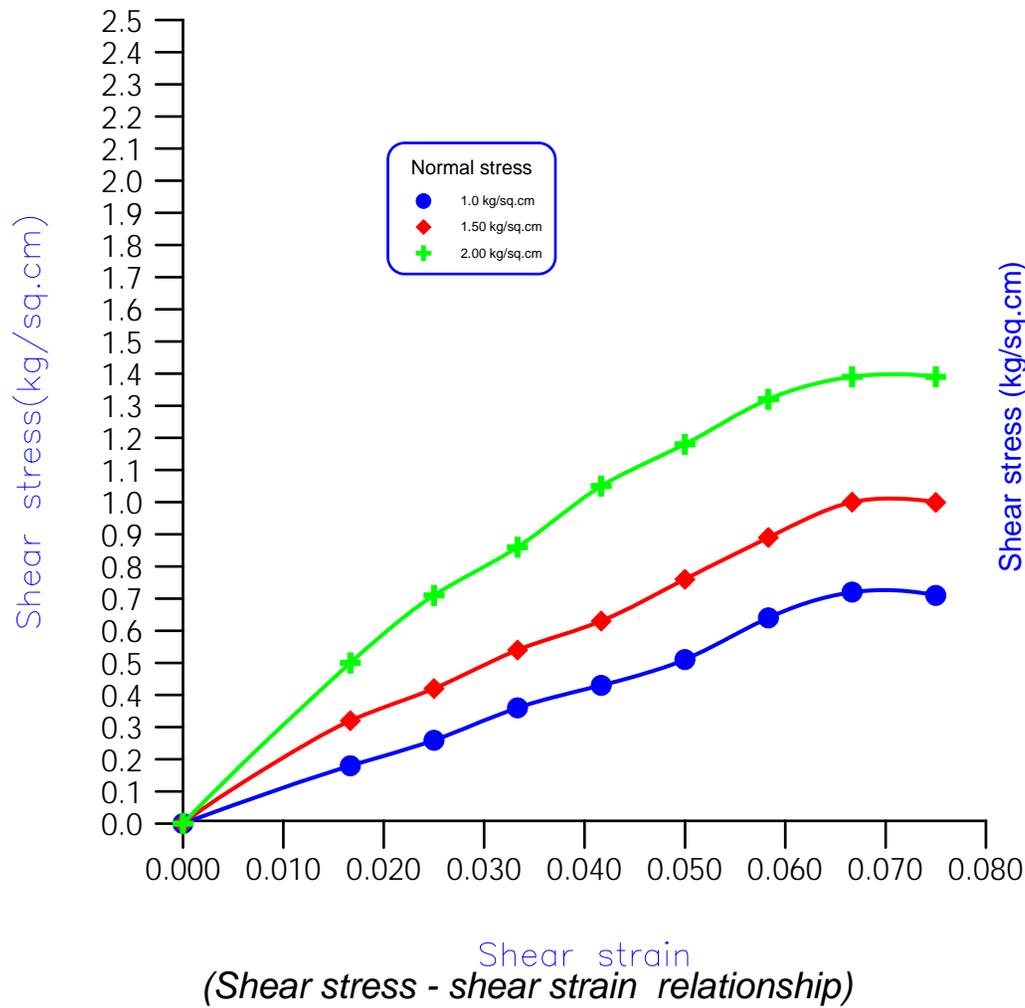
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Job. 2152



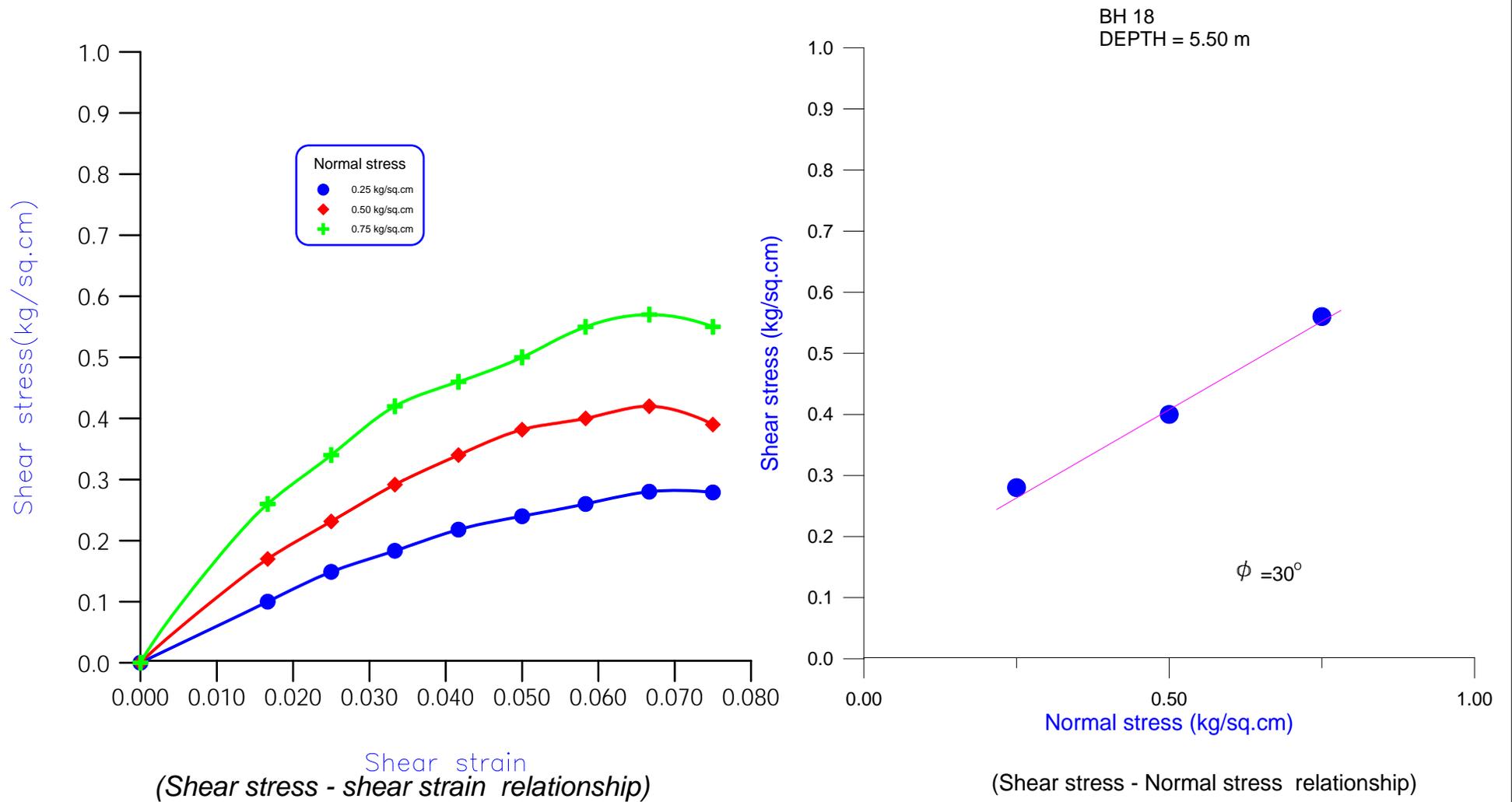
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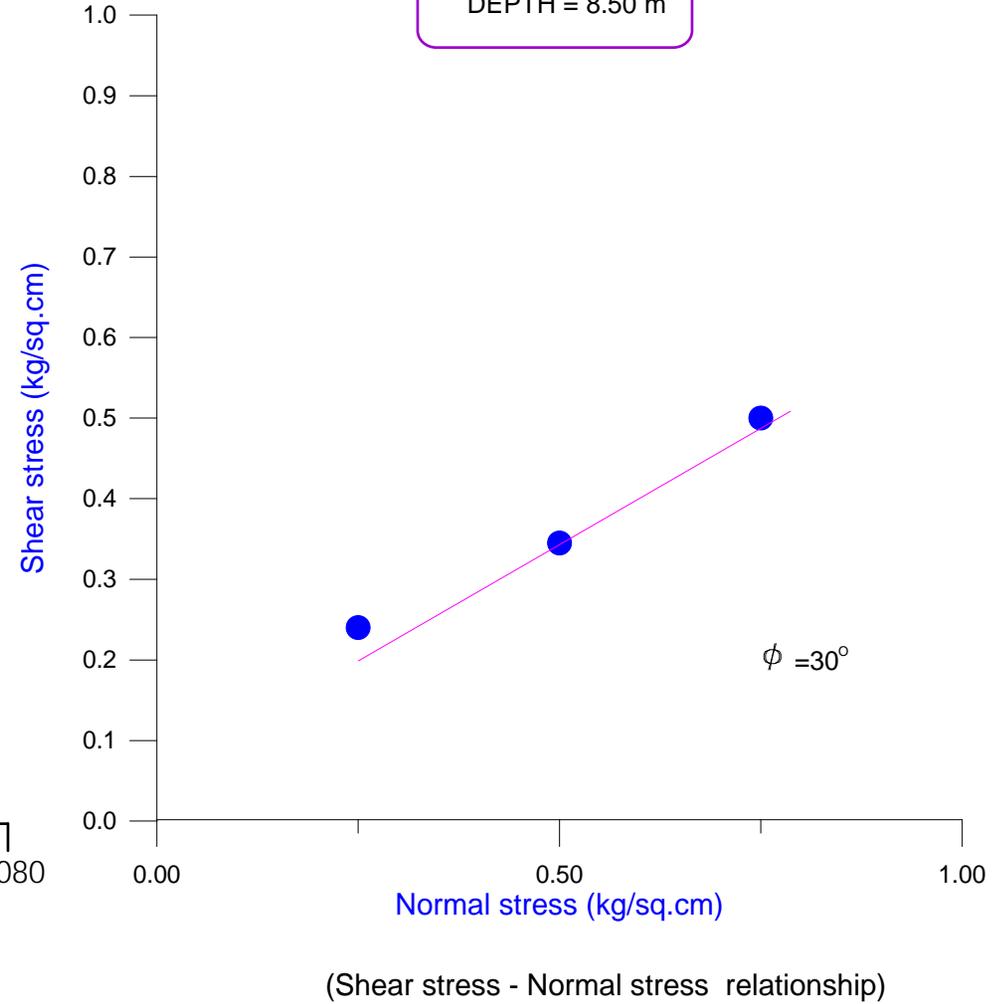
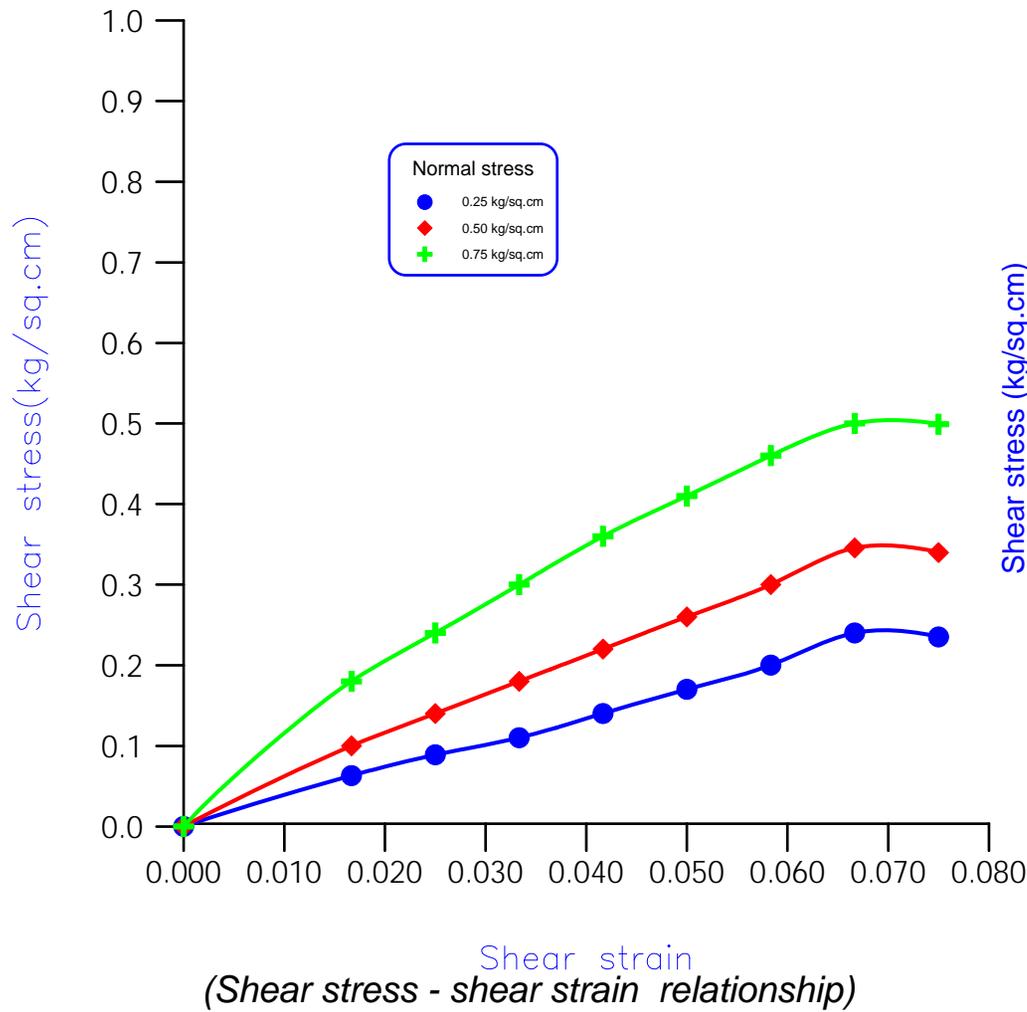
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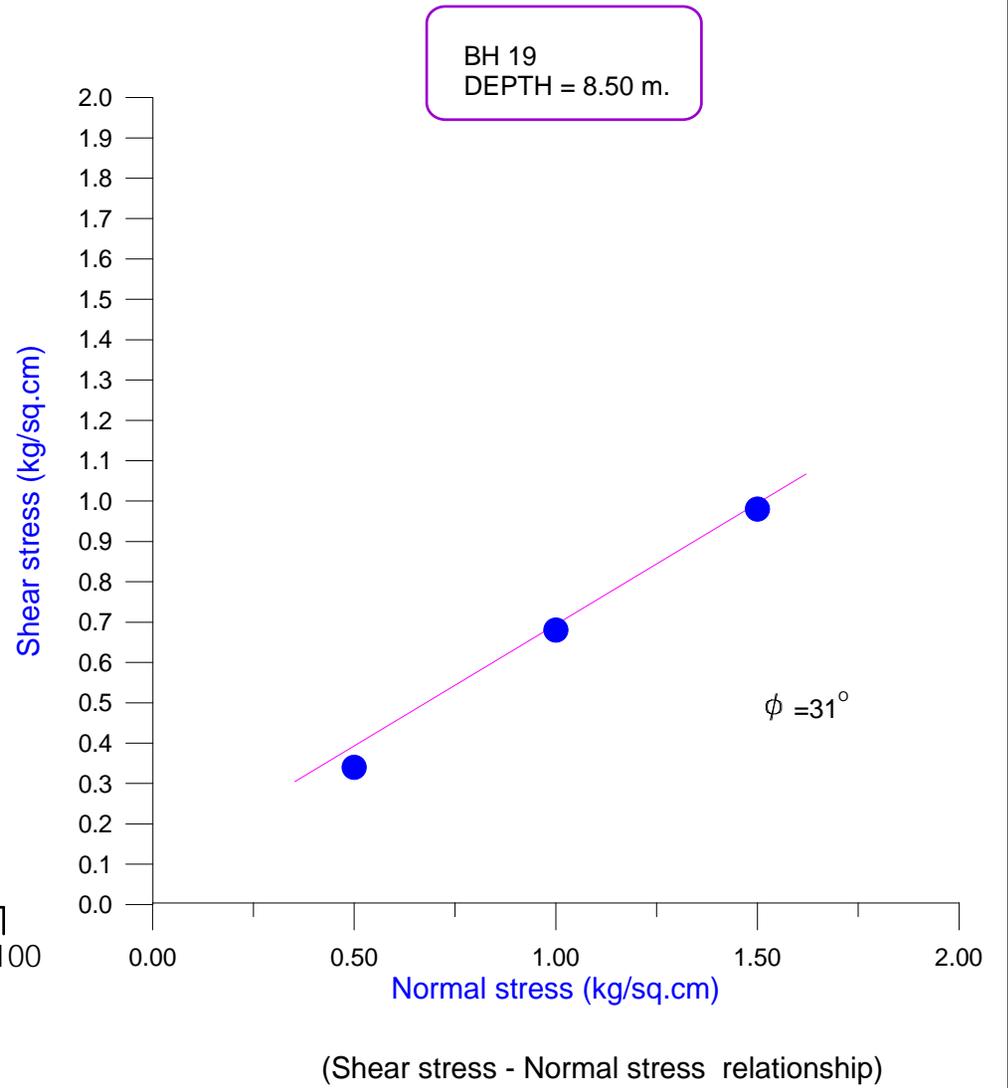
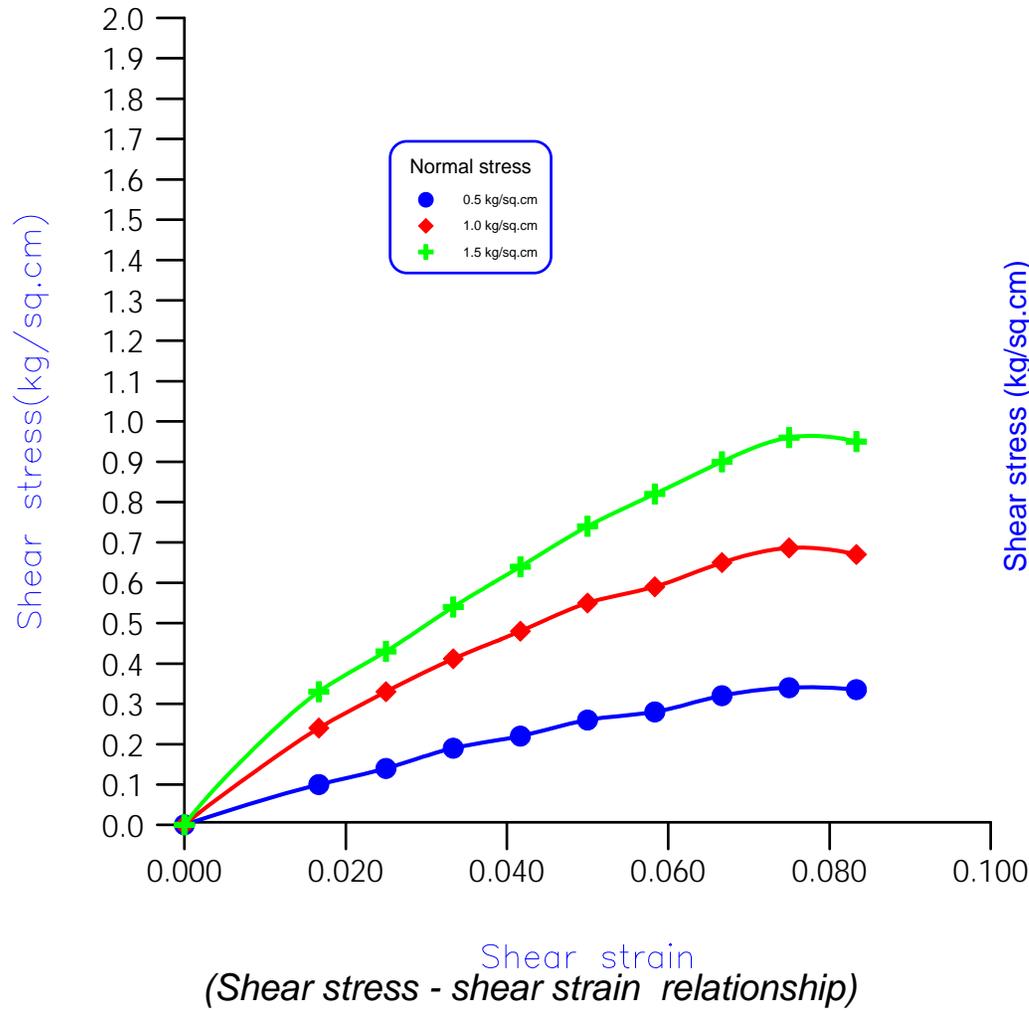
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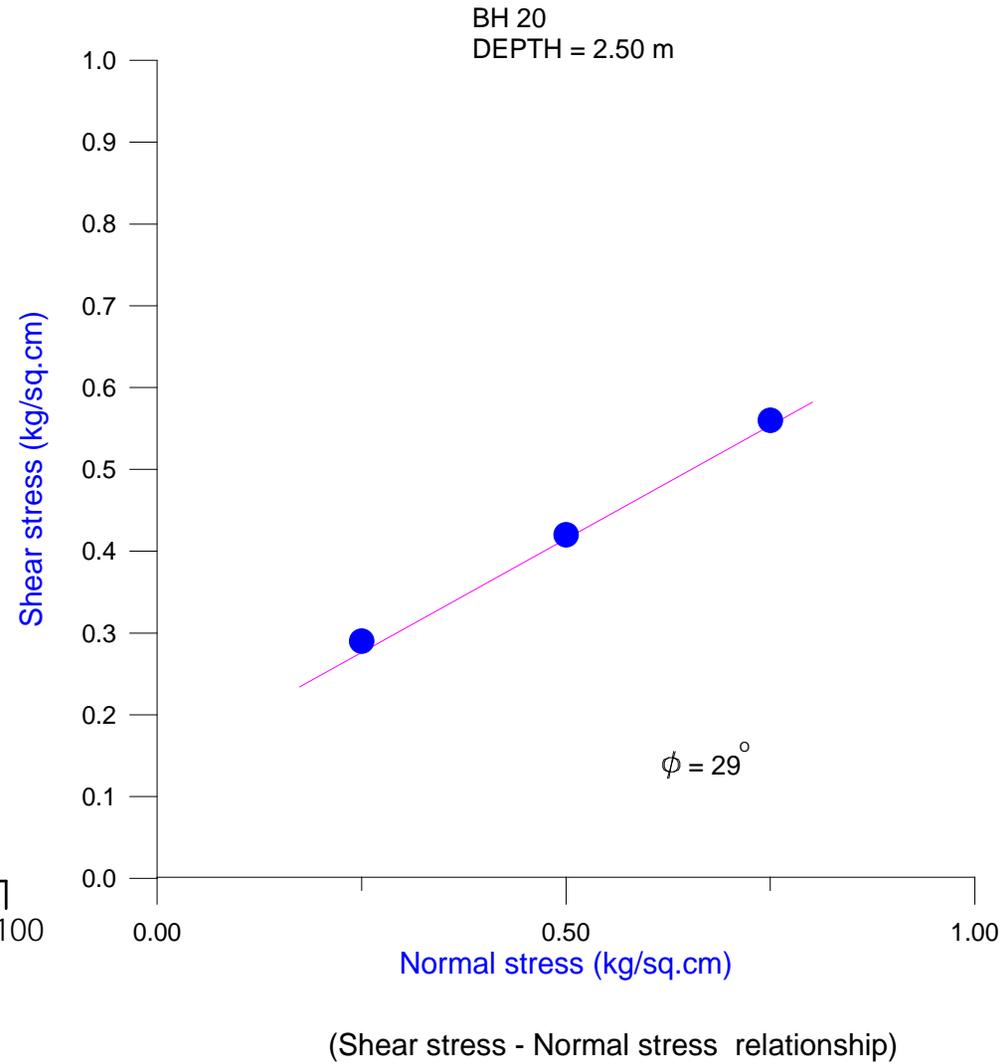
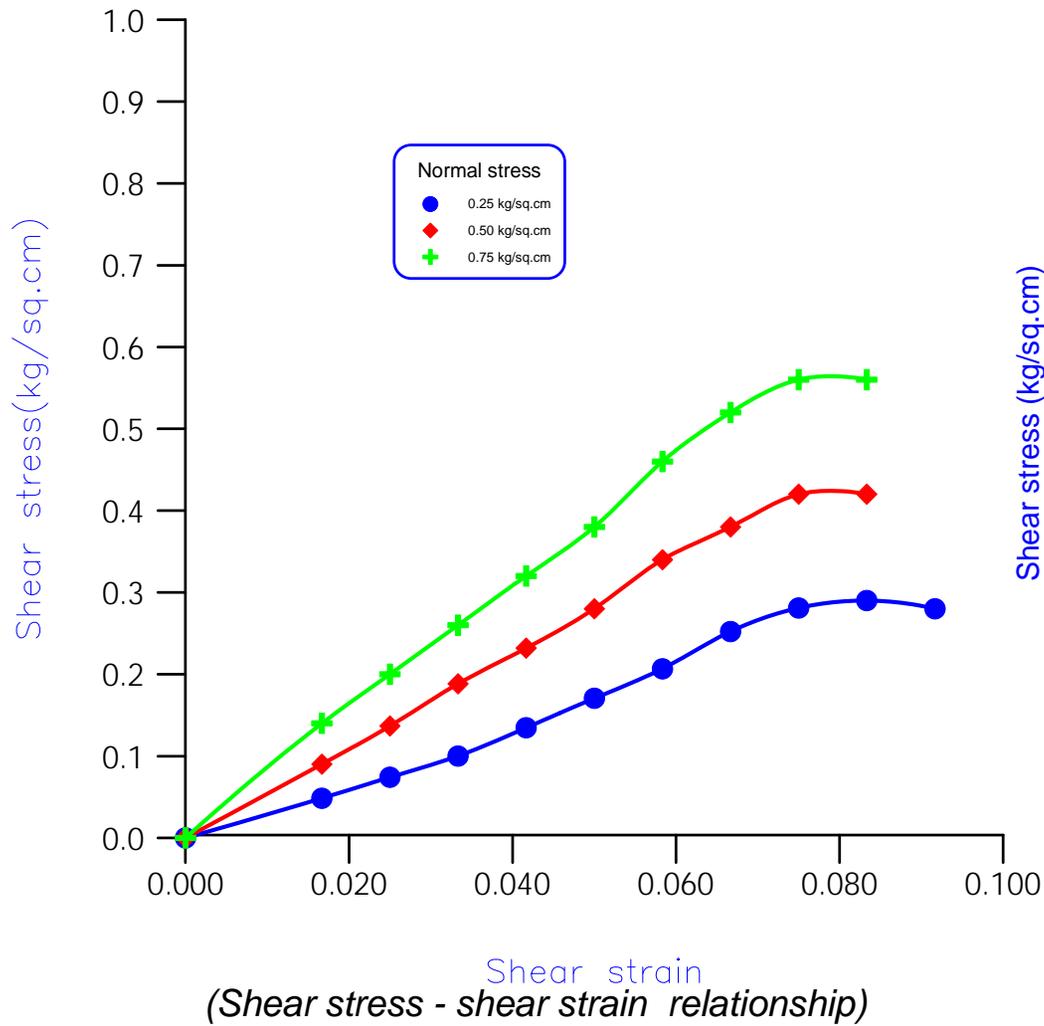
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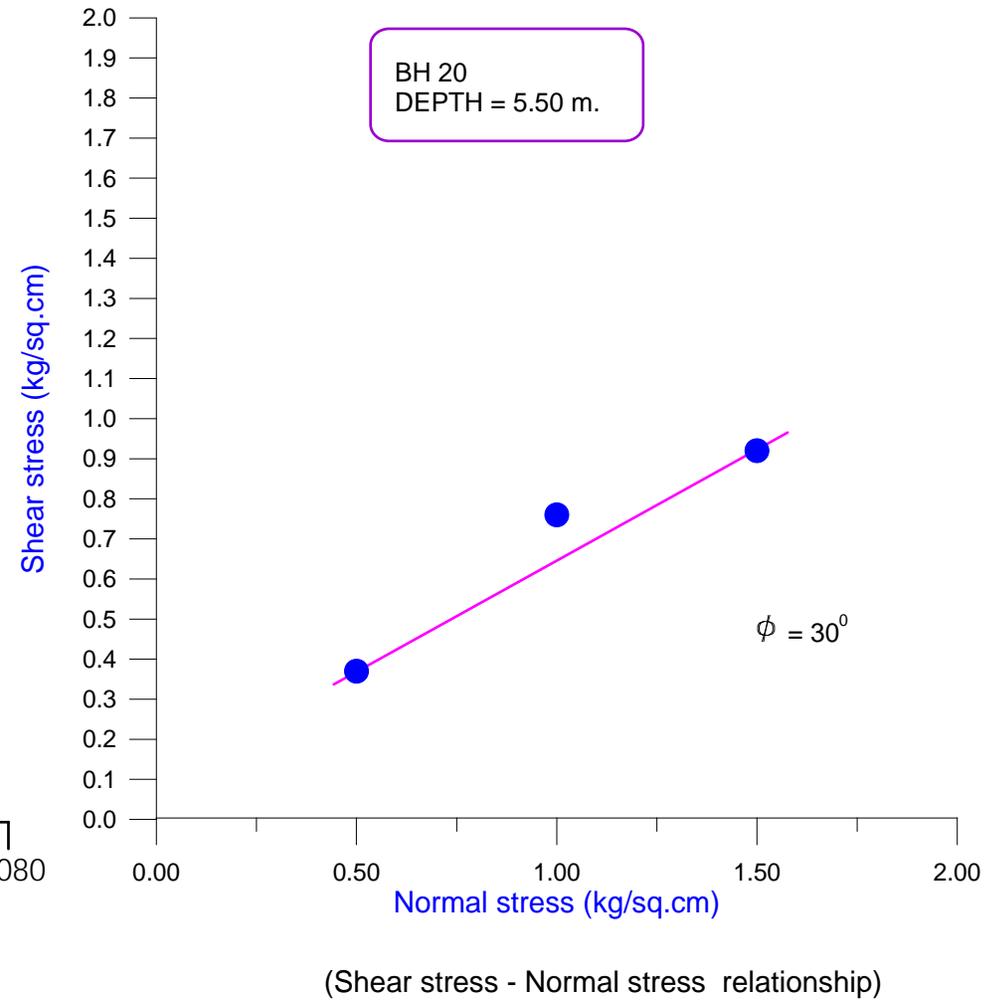
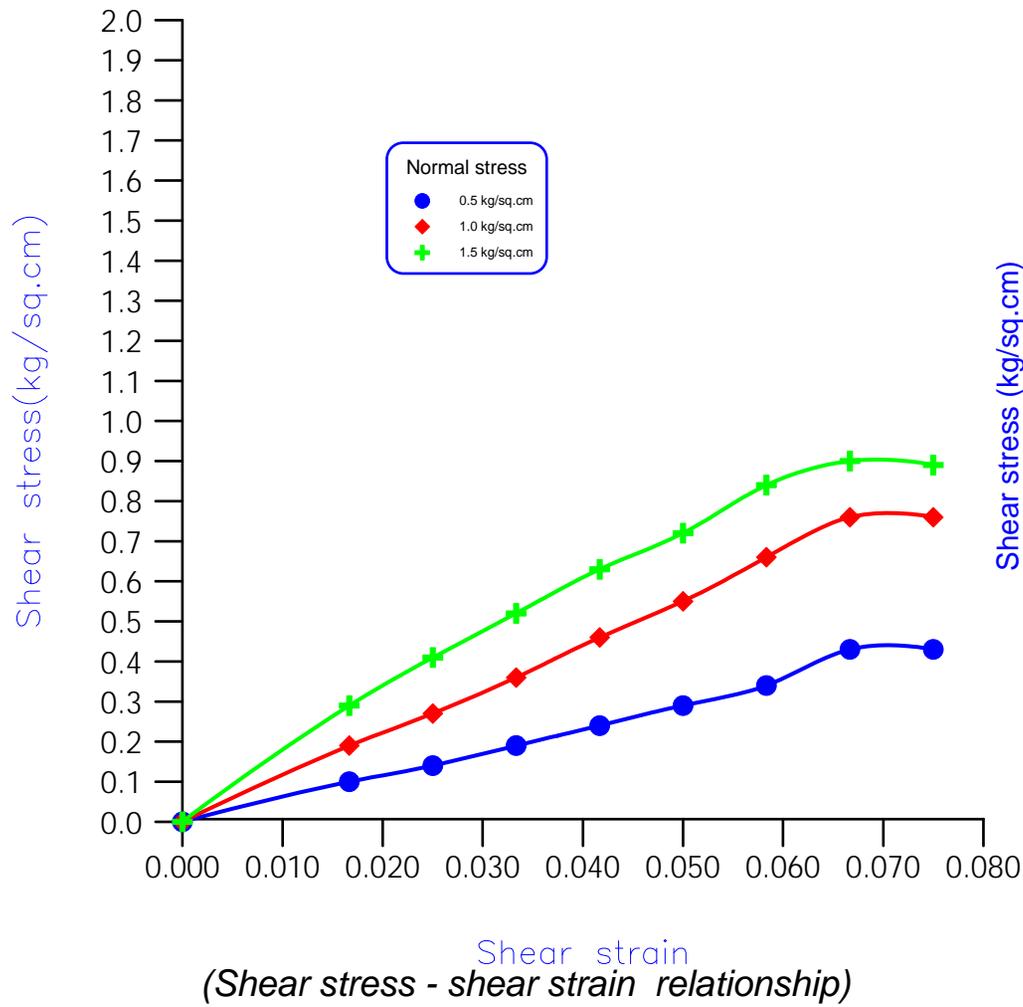
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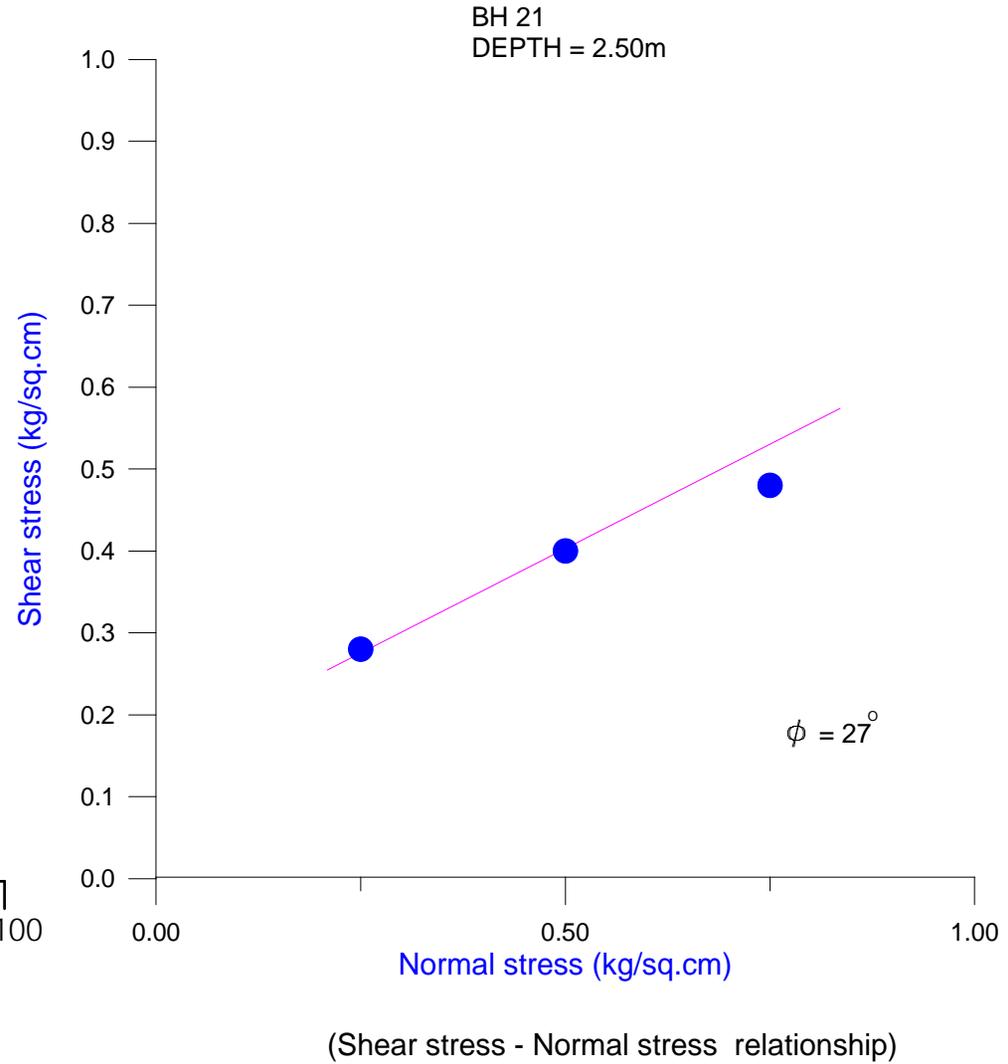
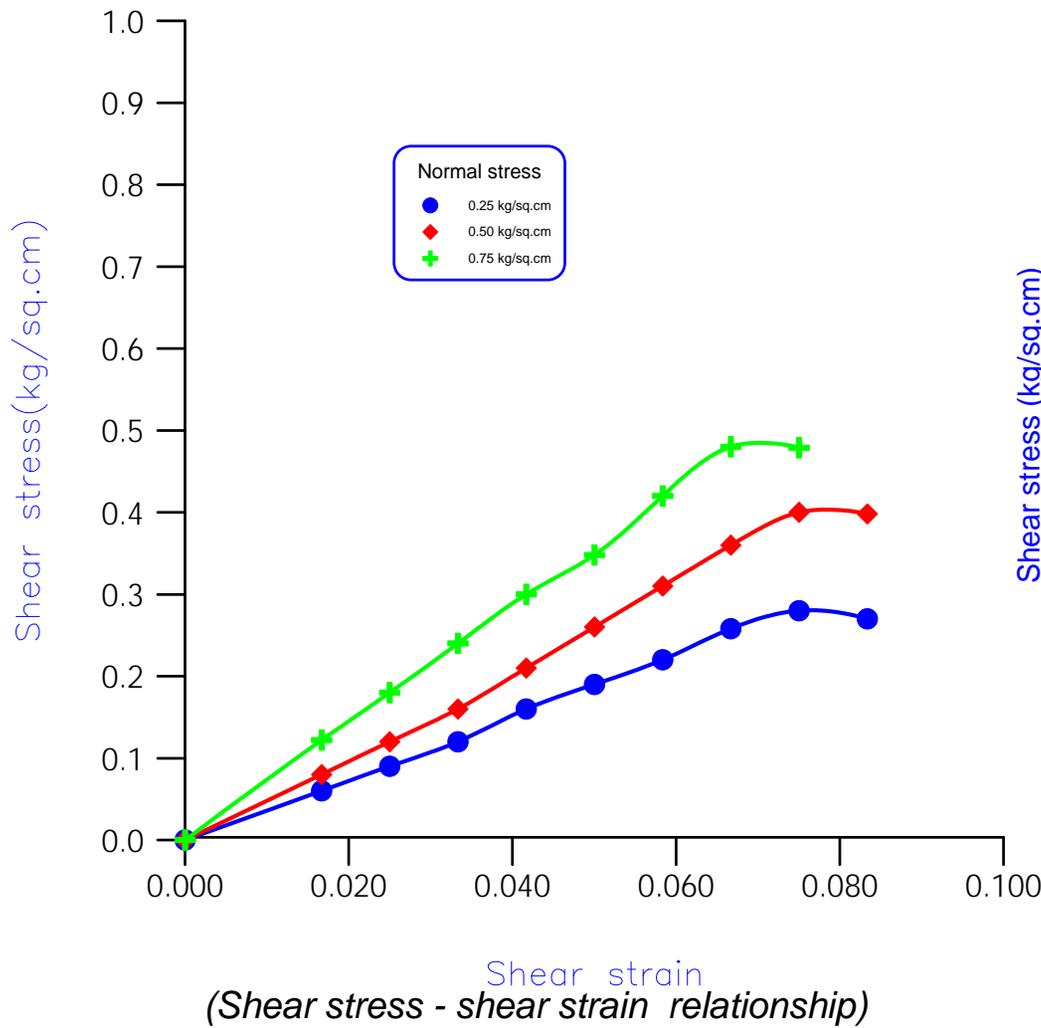
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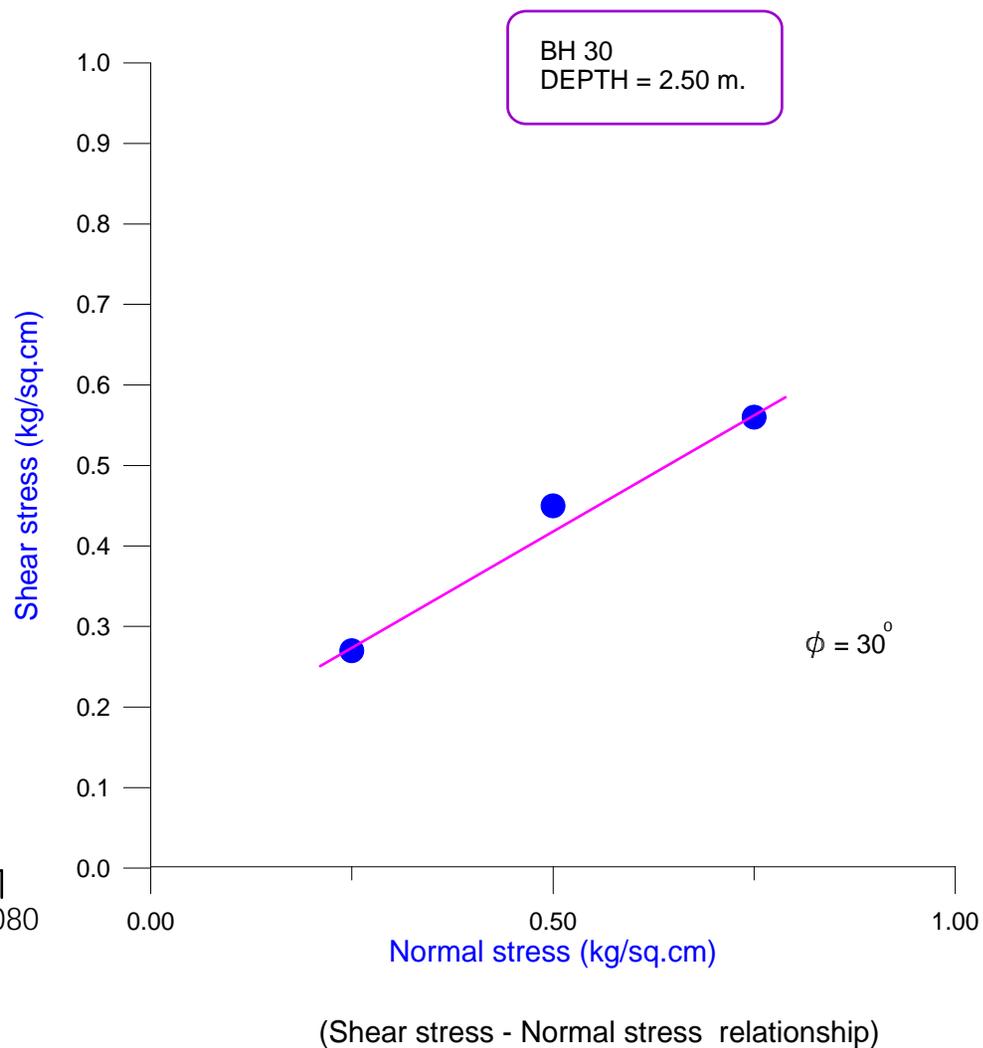
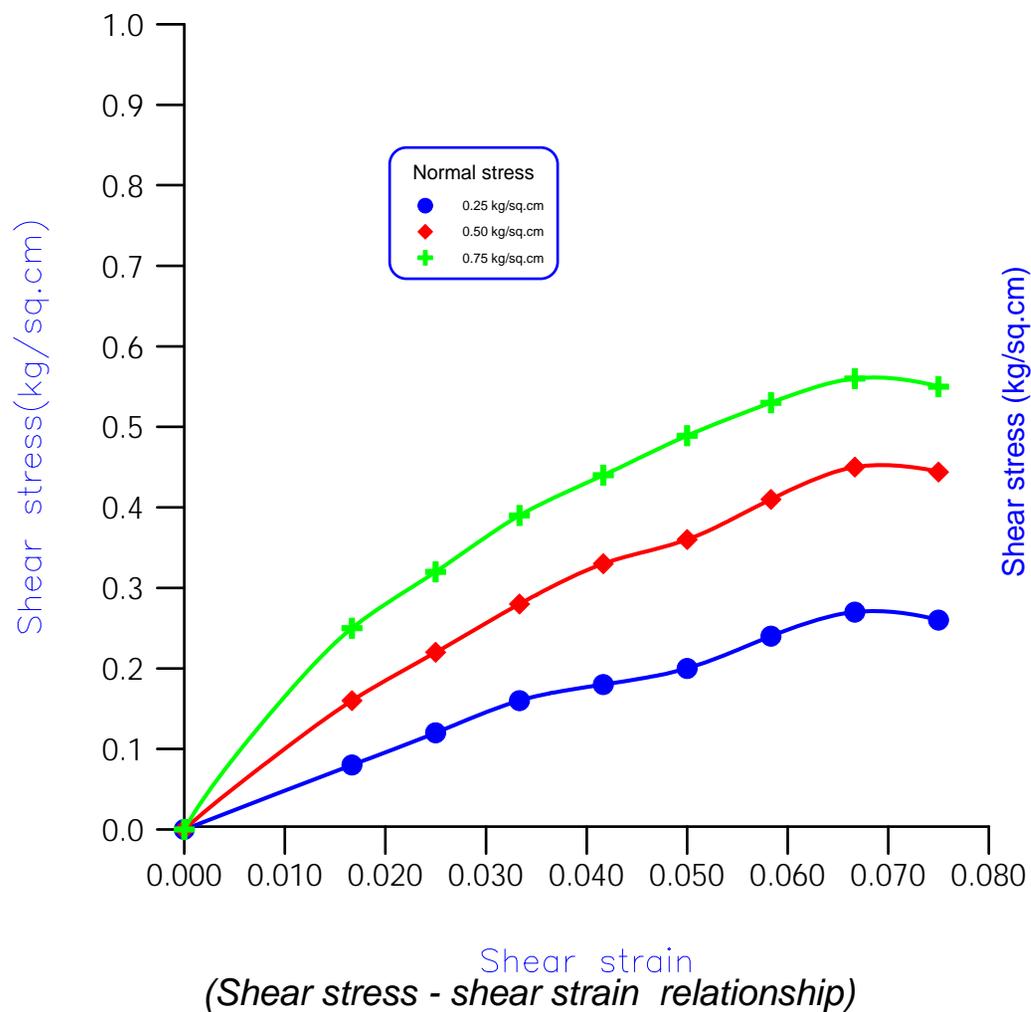
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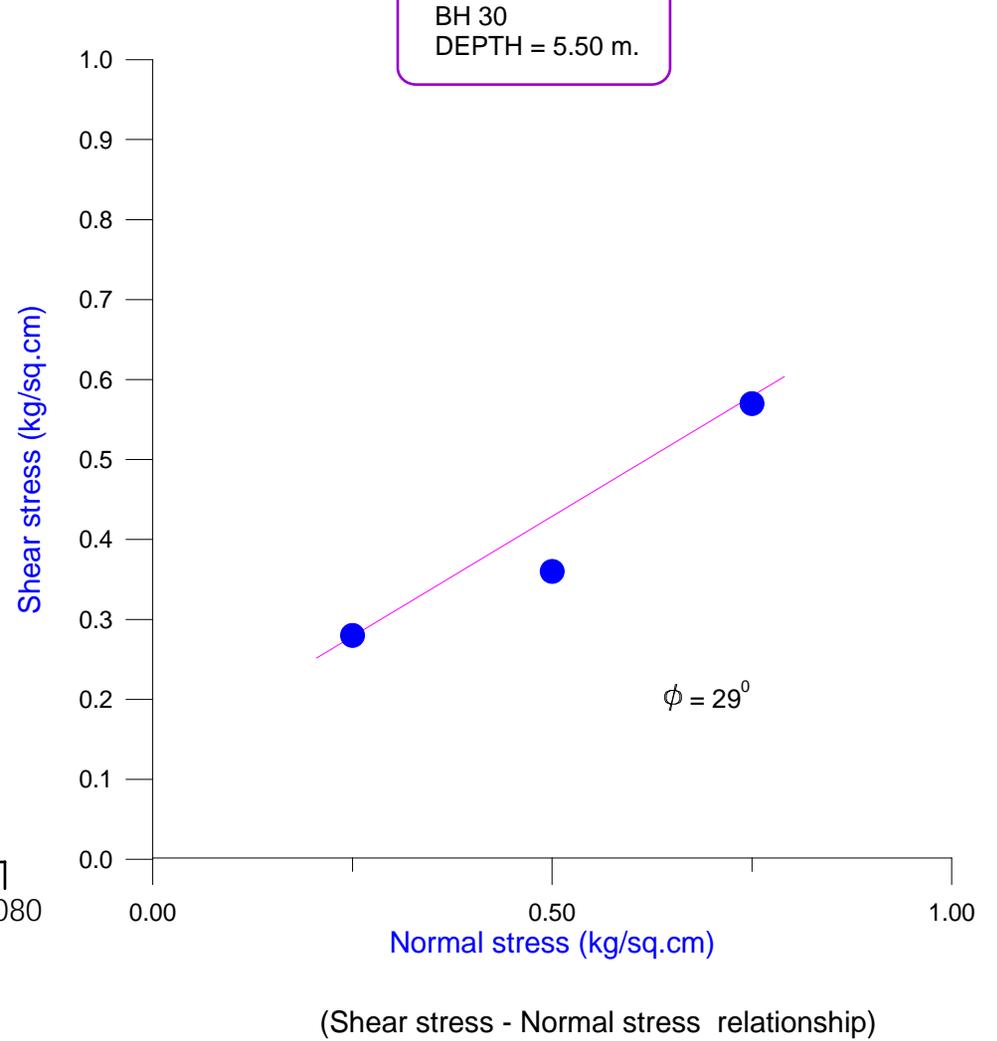
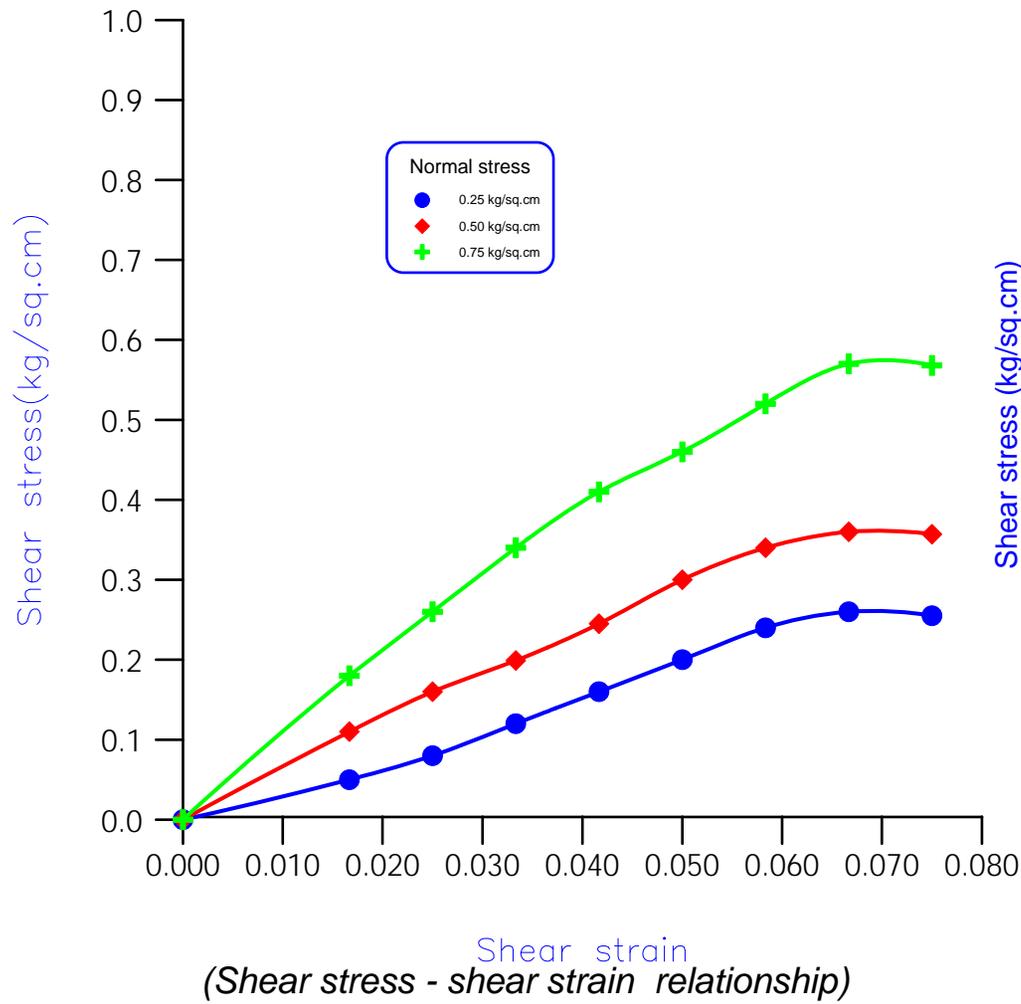
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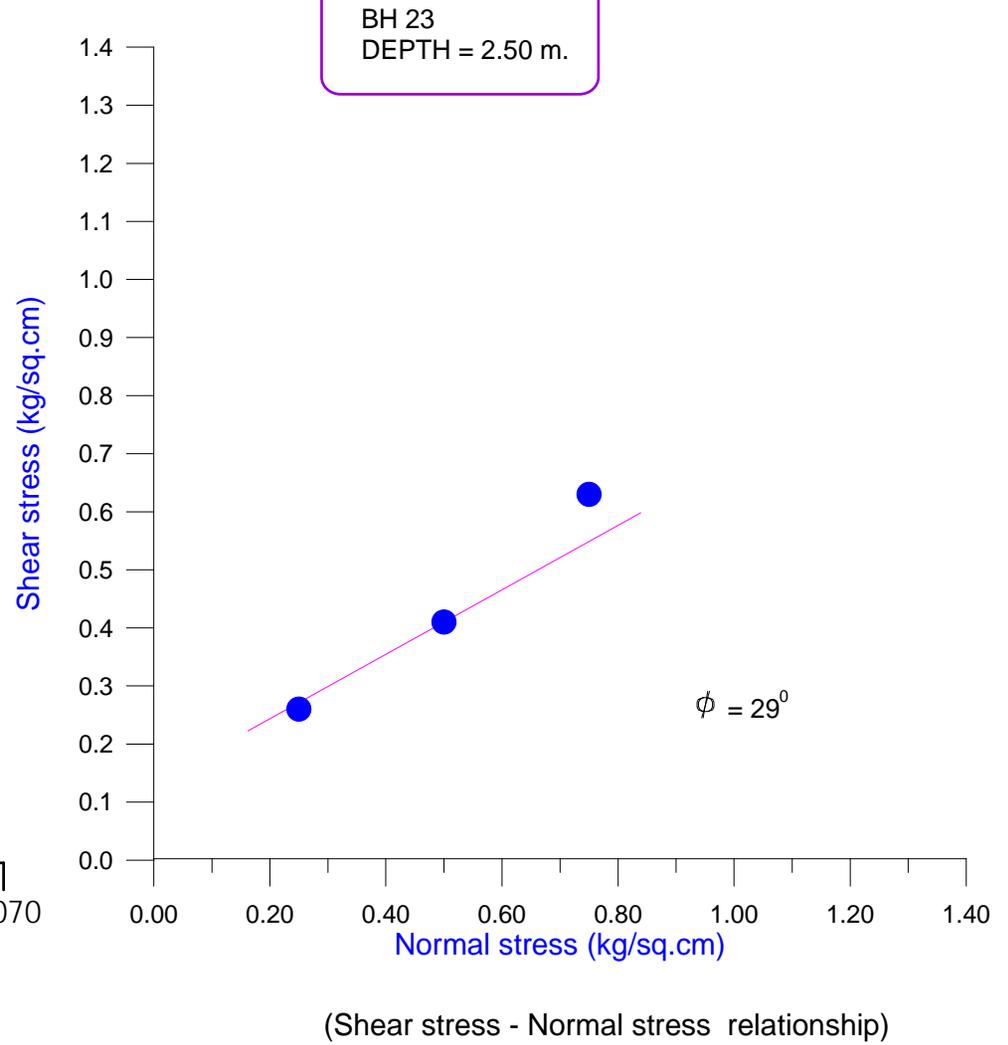
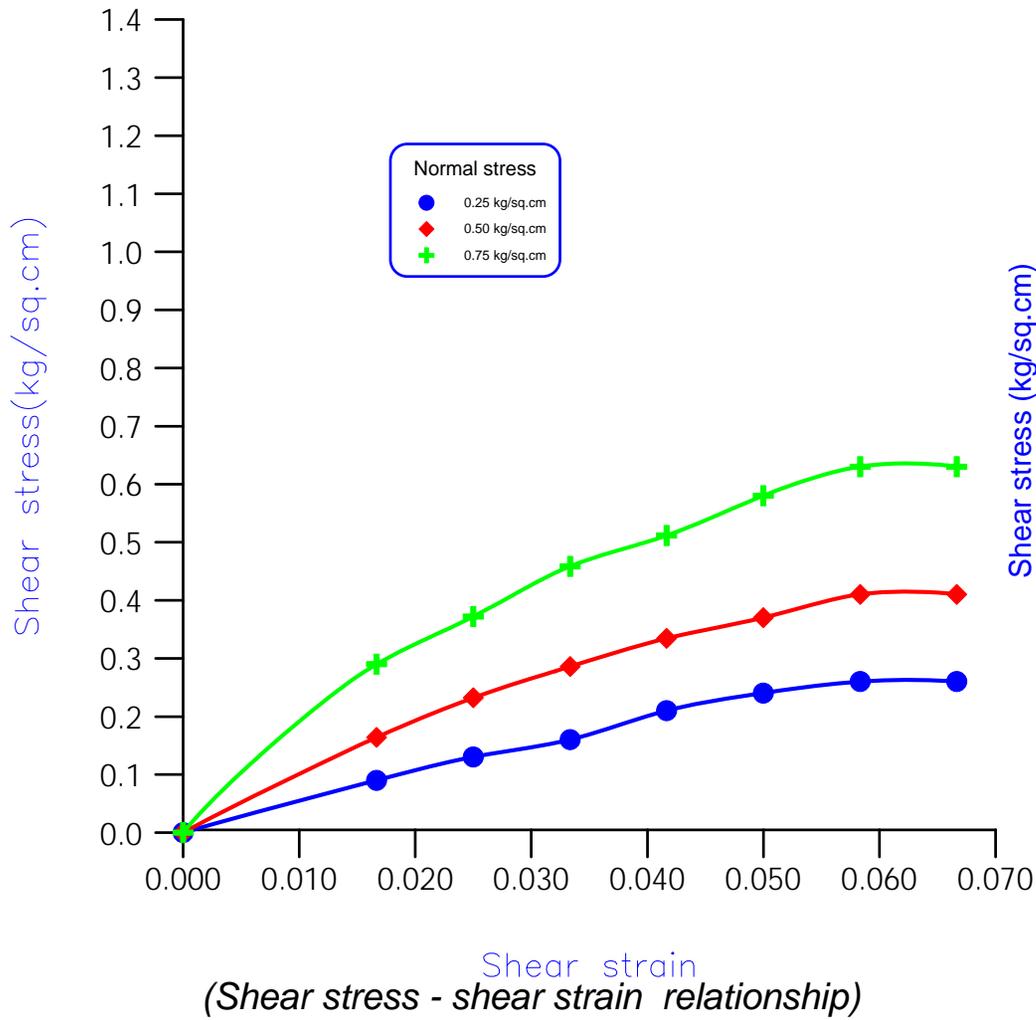


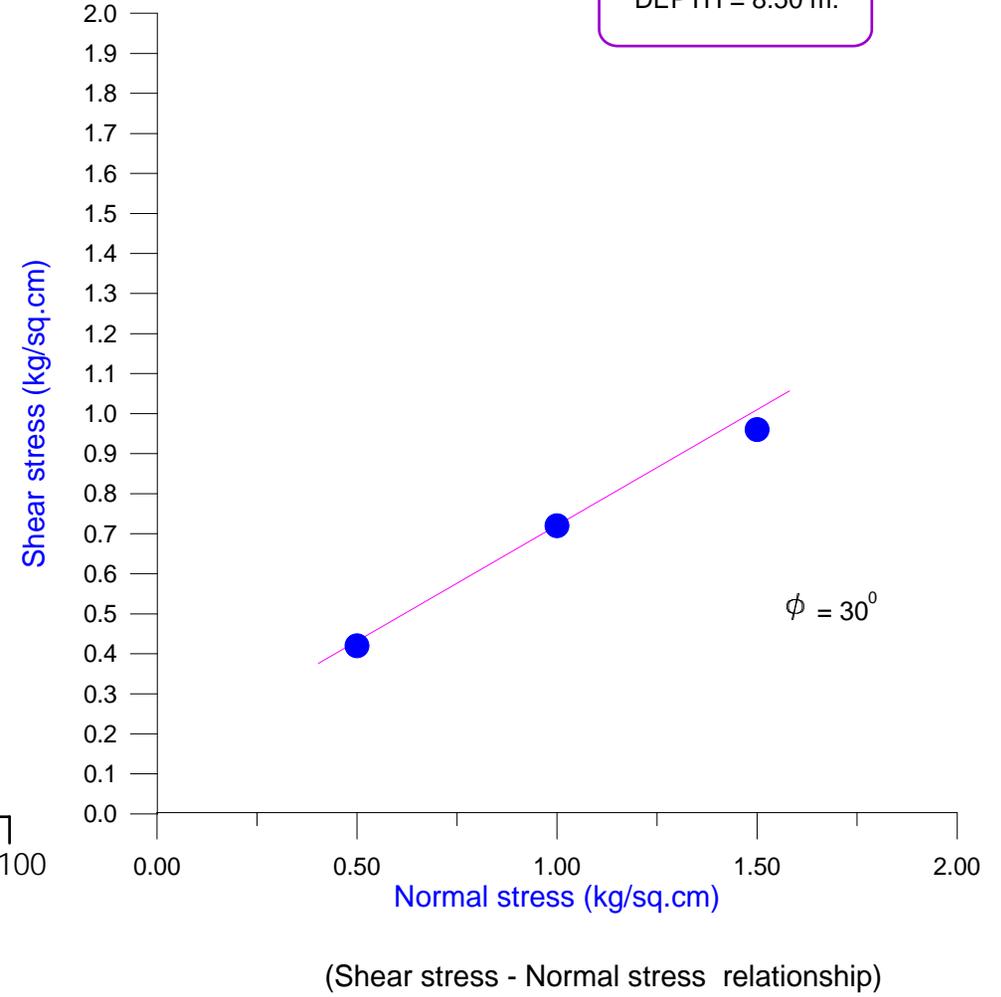
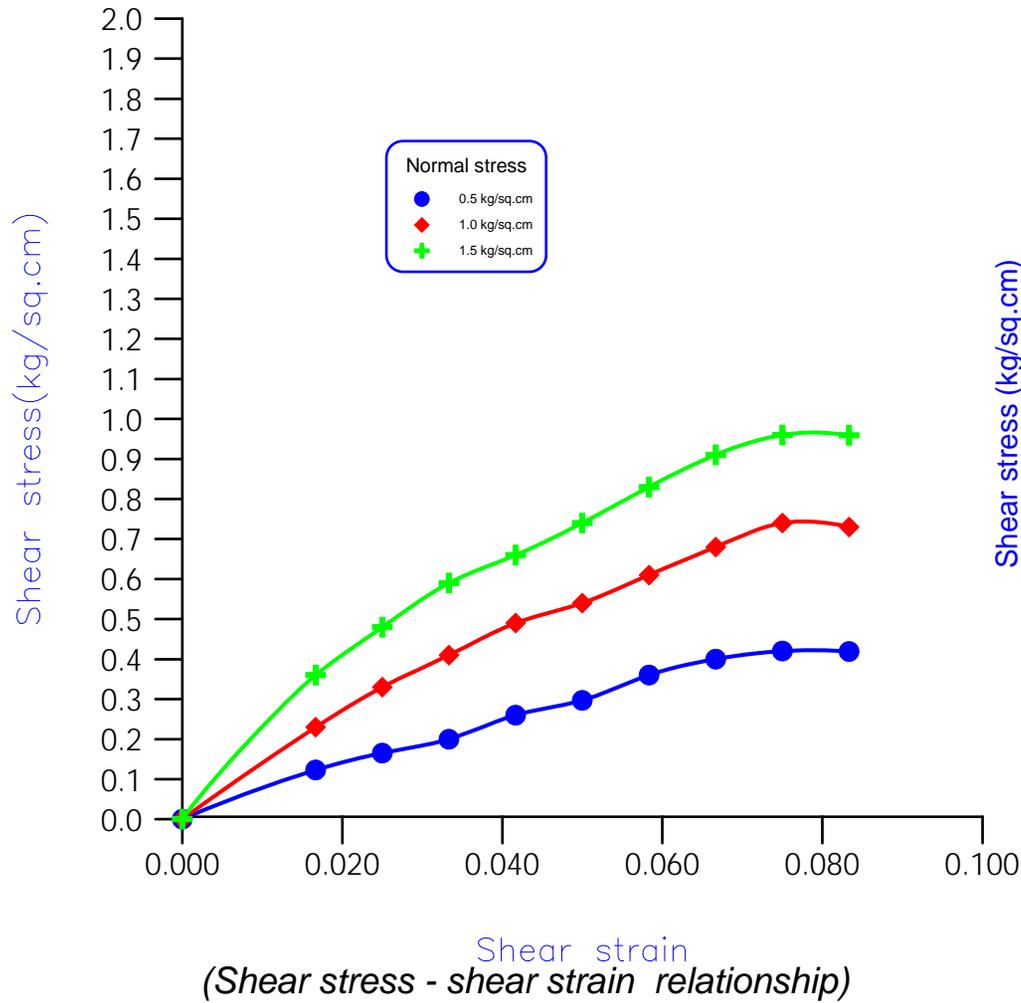


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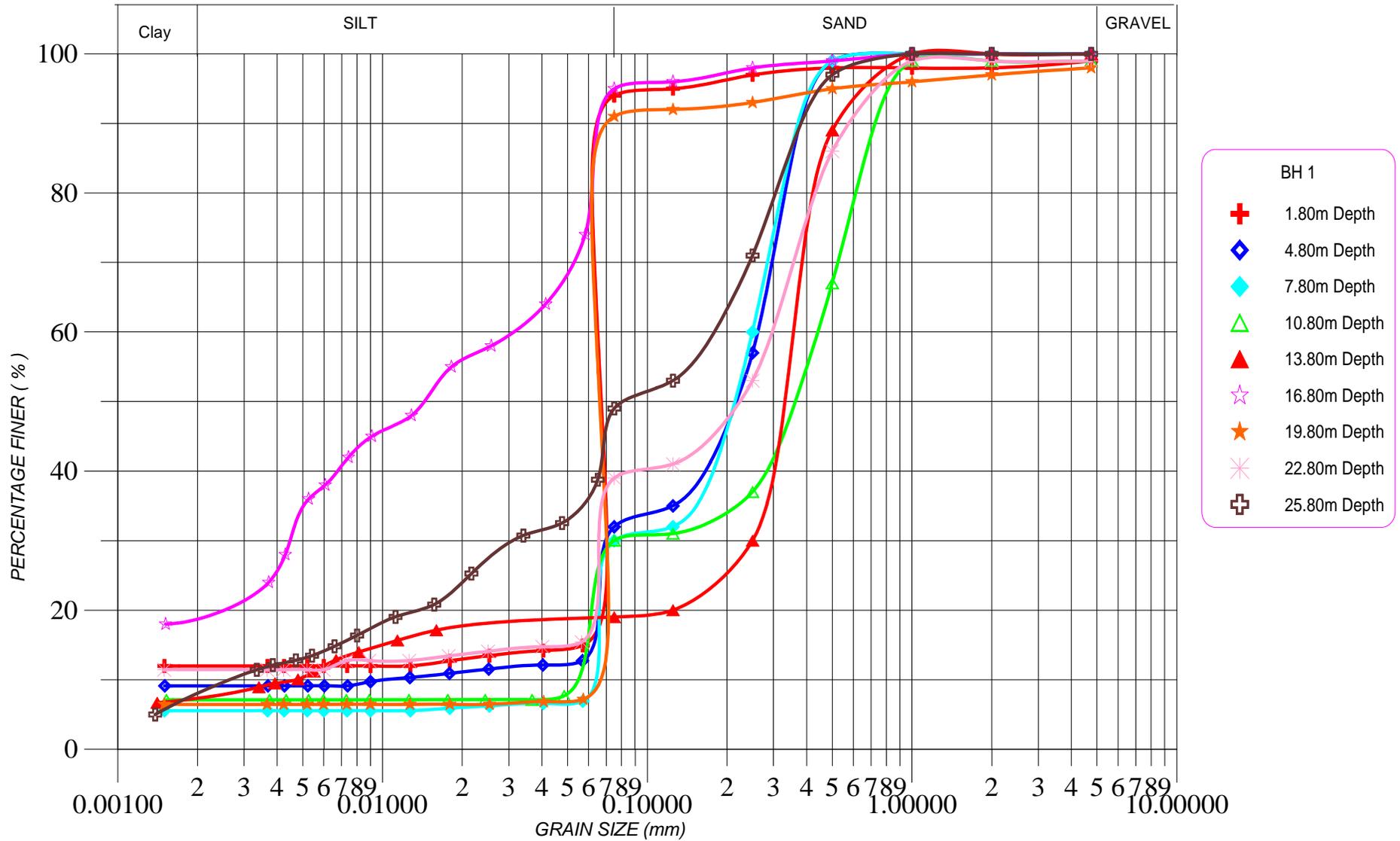
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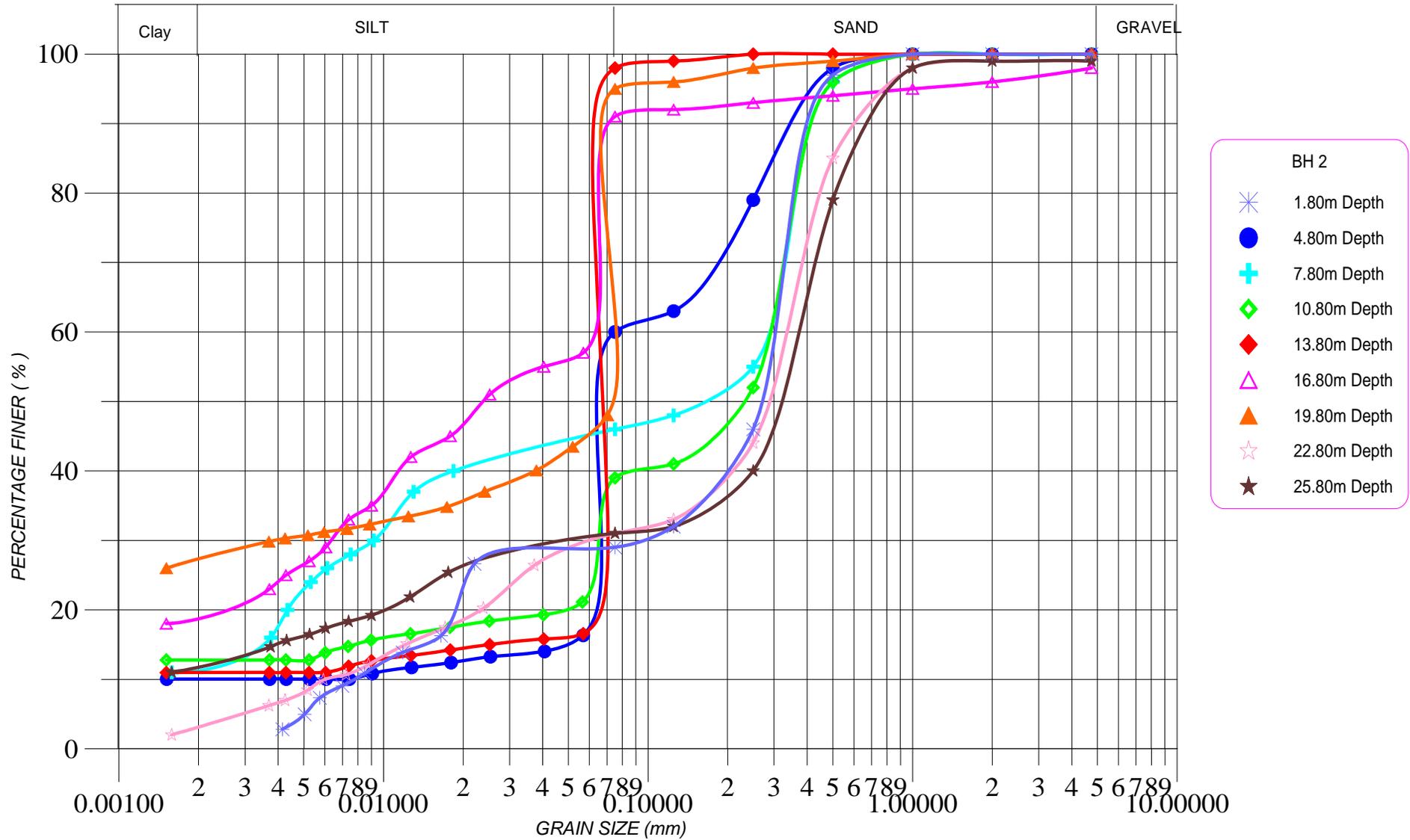


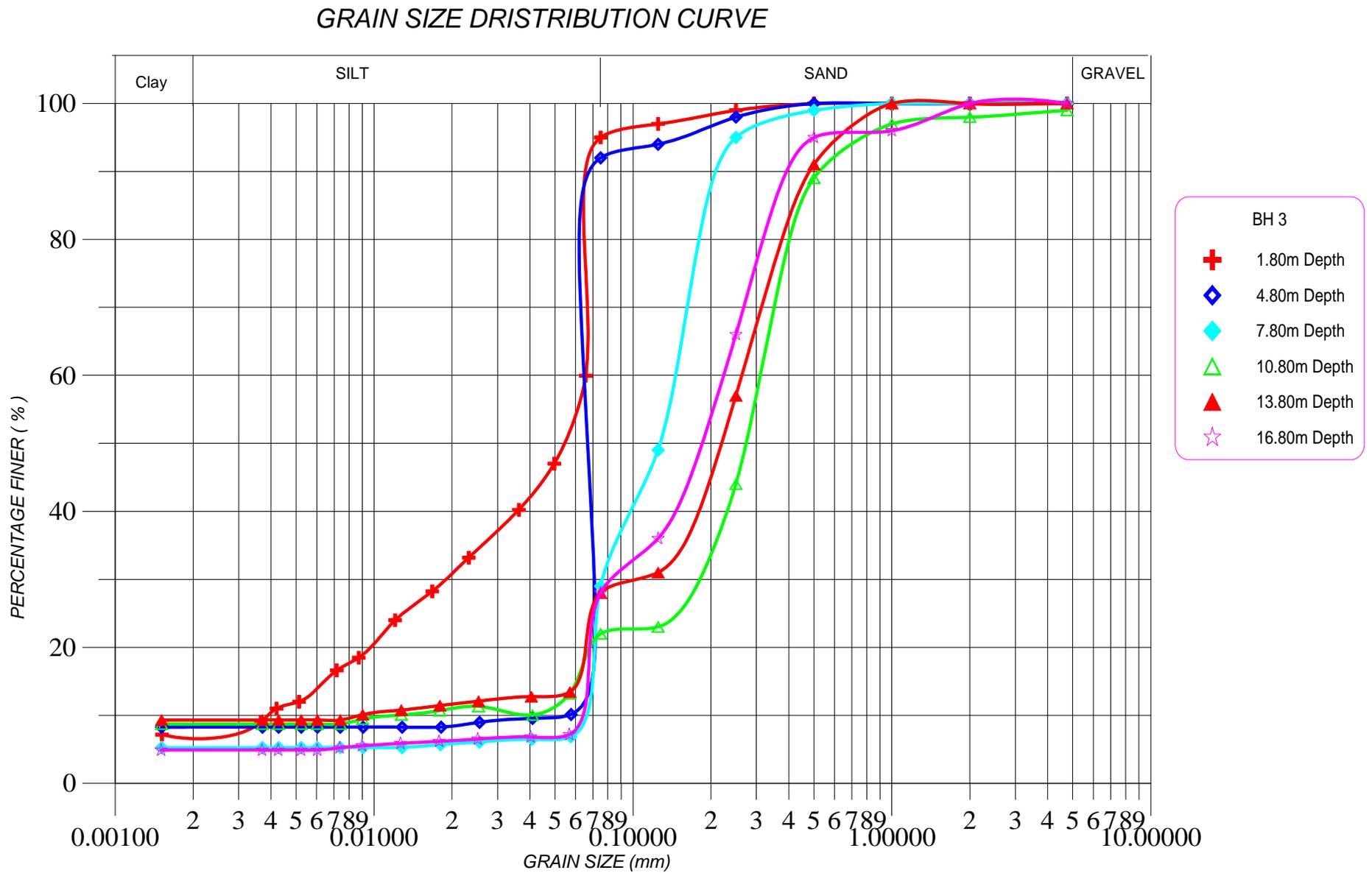


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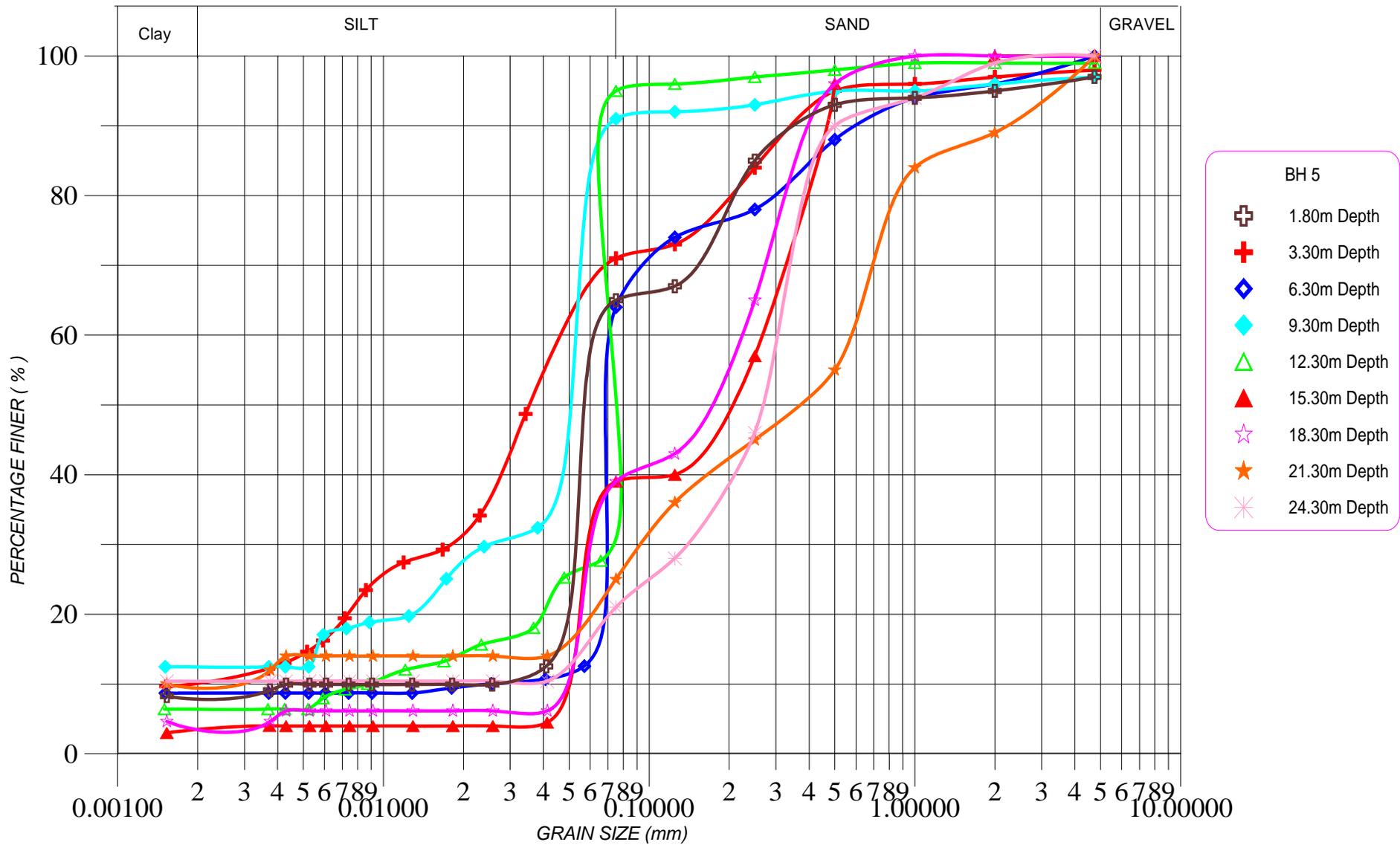


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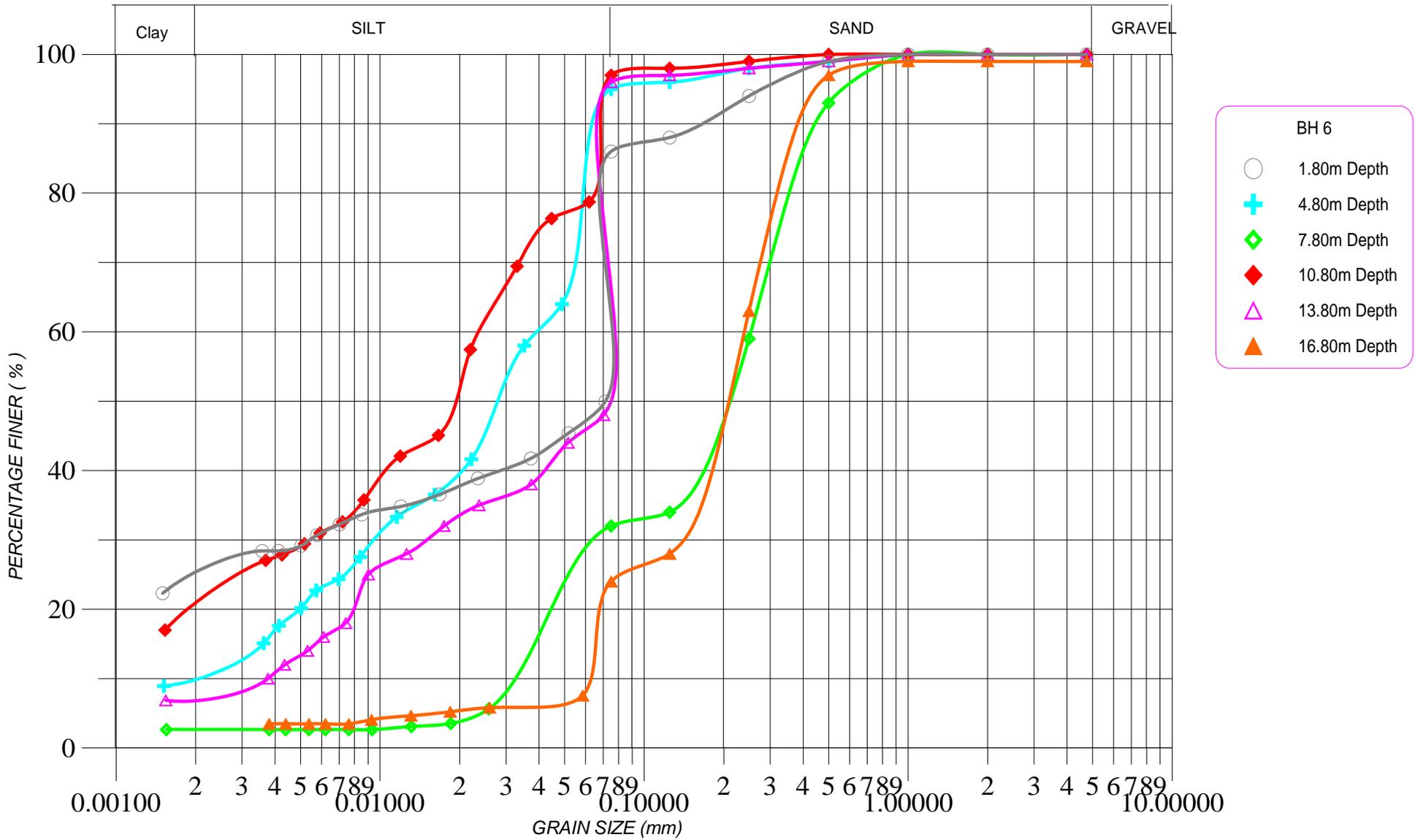




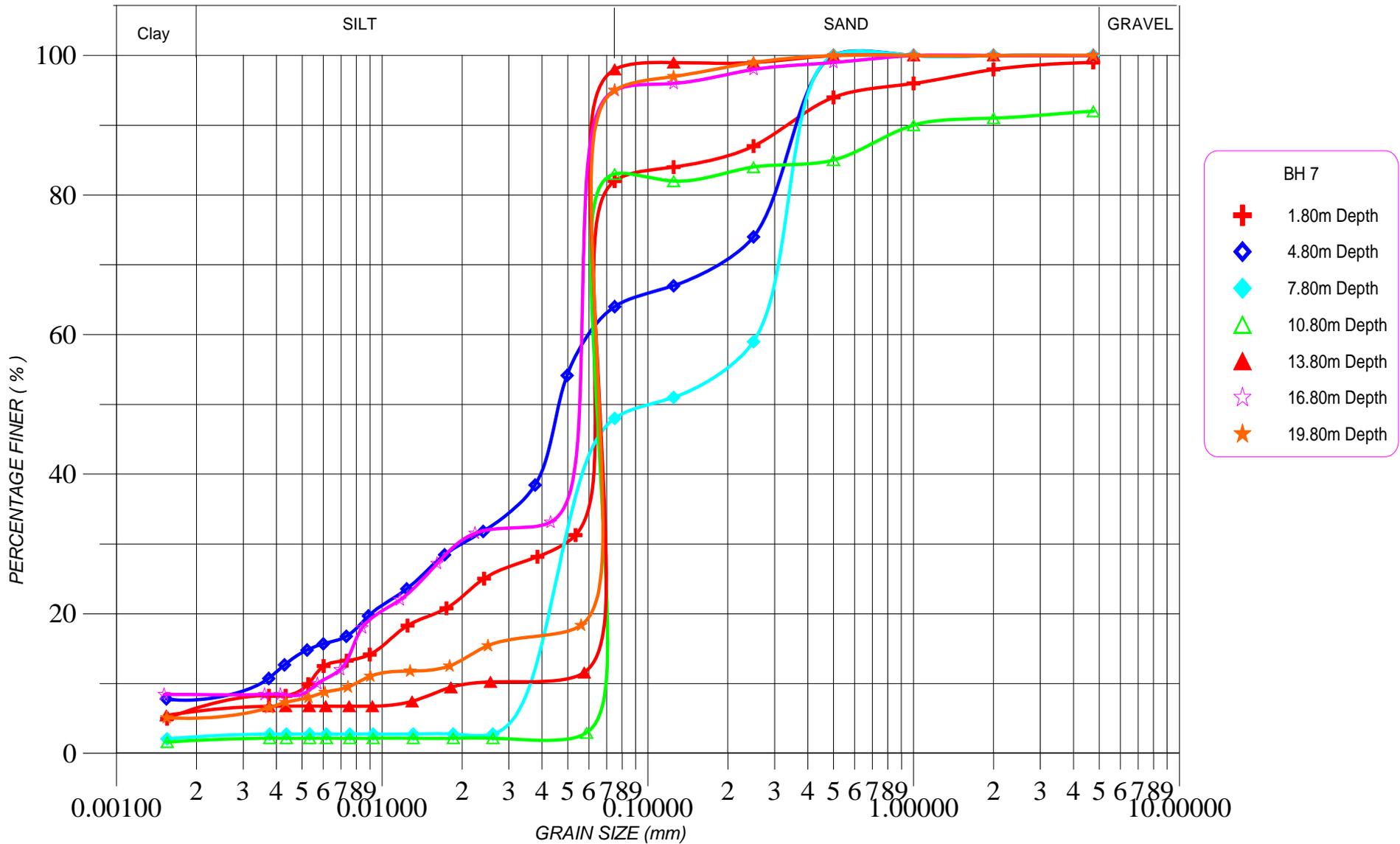
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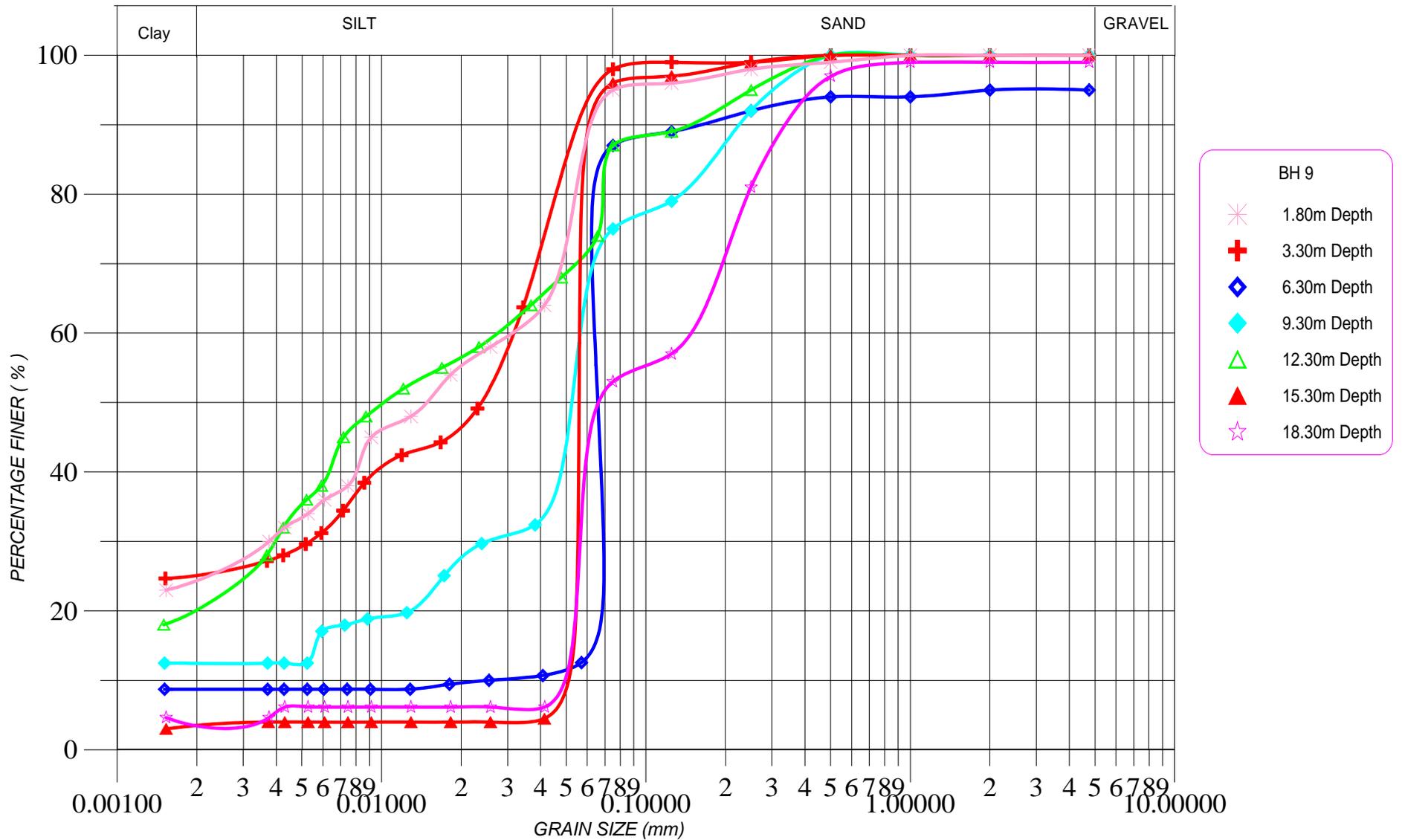
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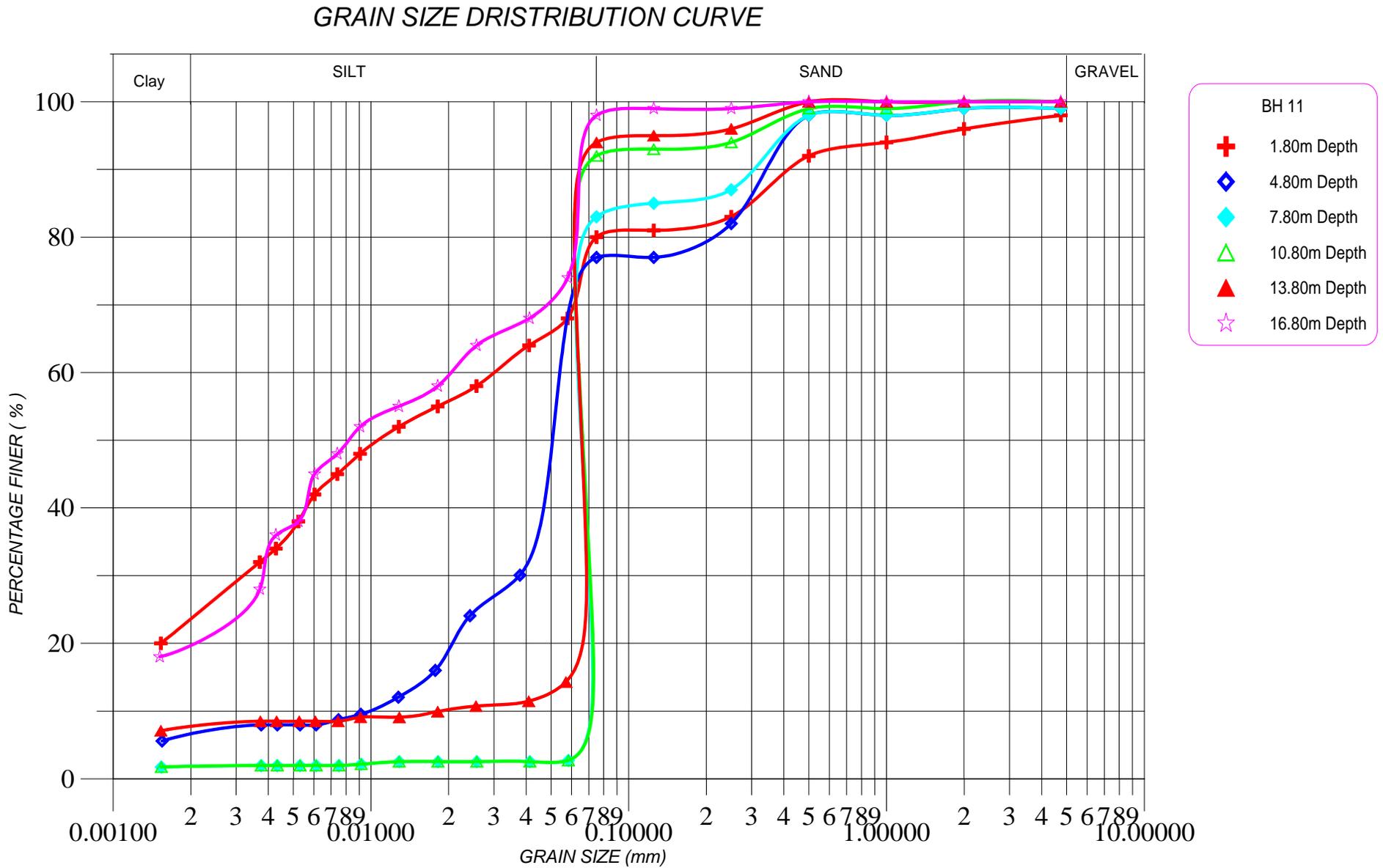


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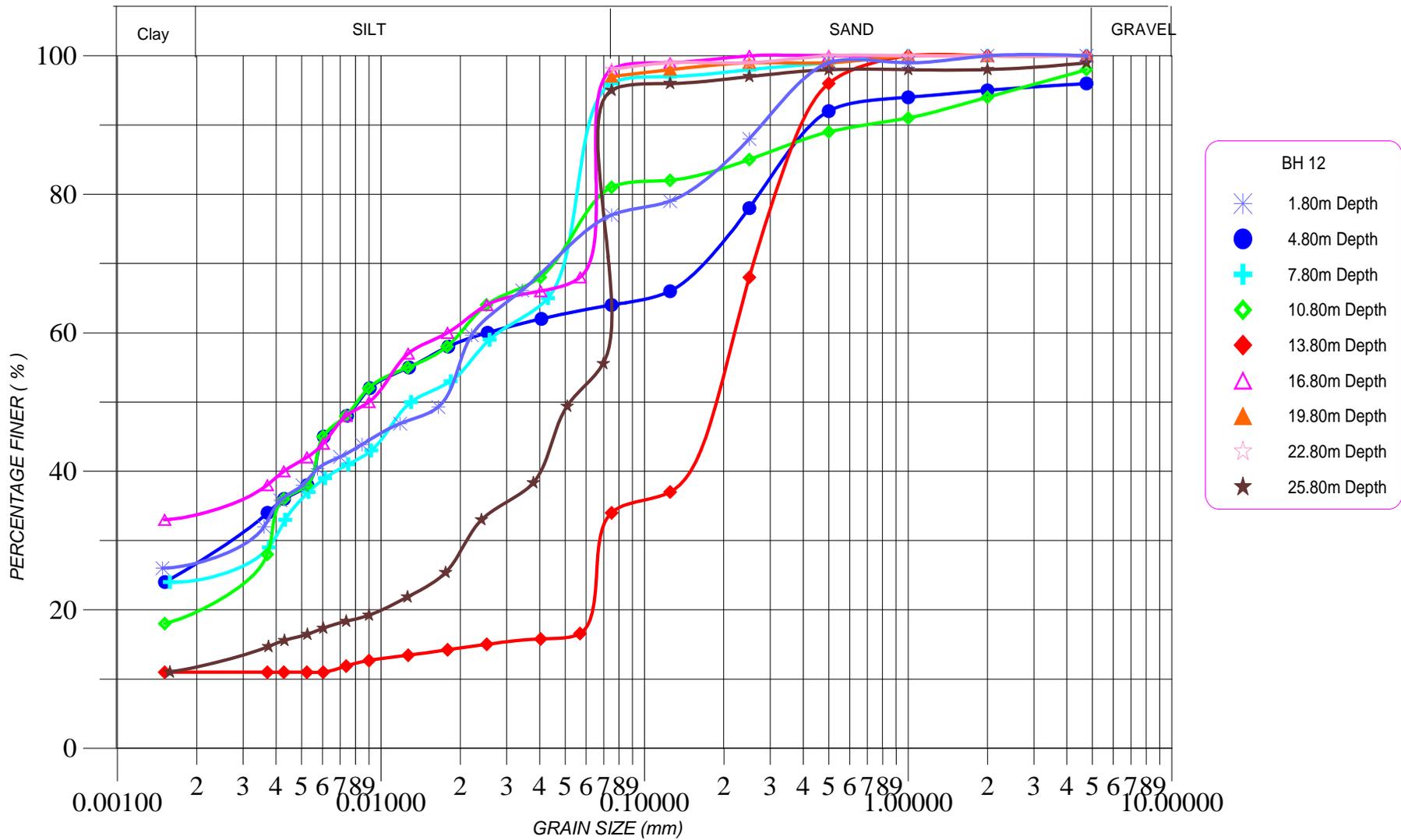


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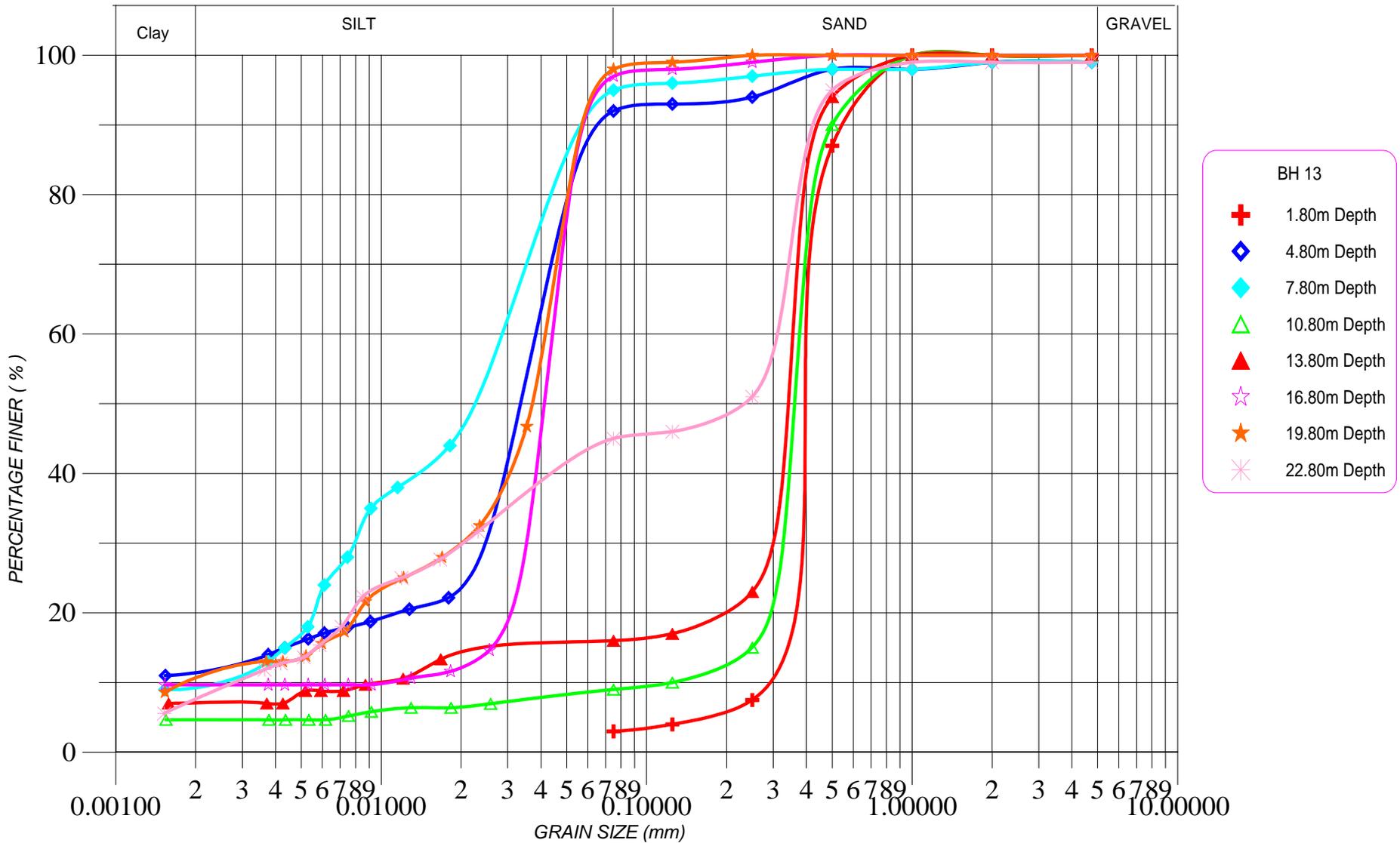




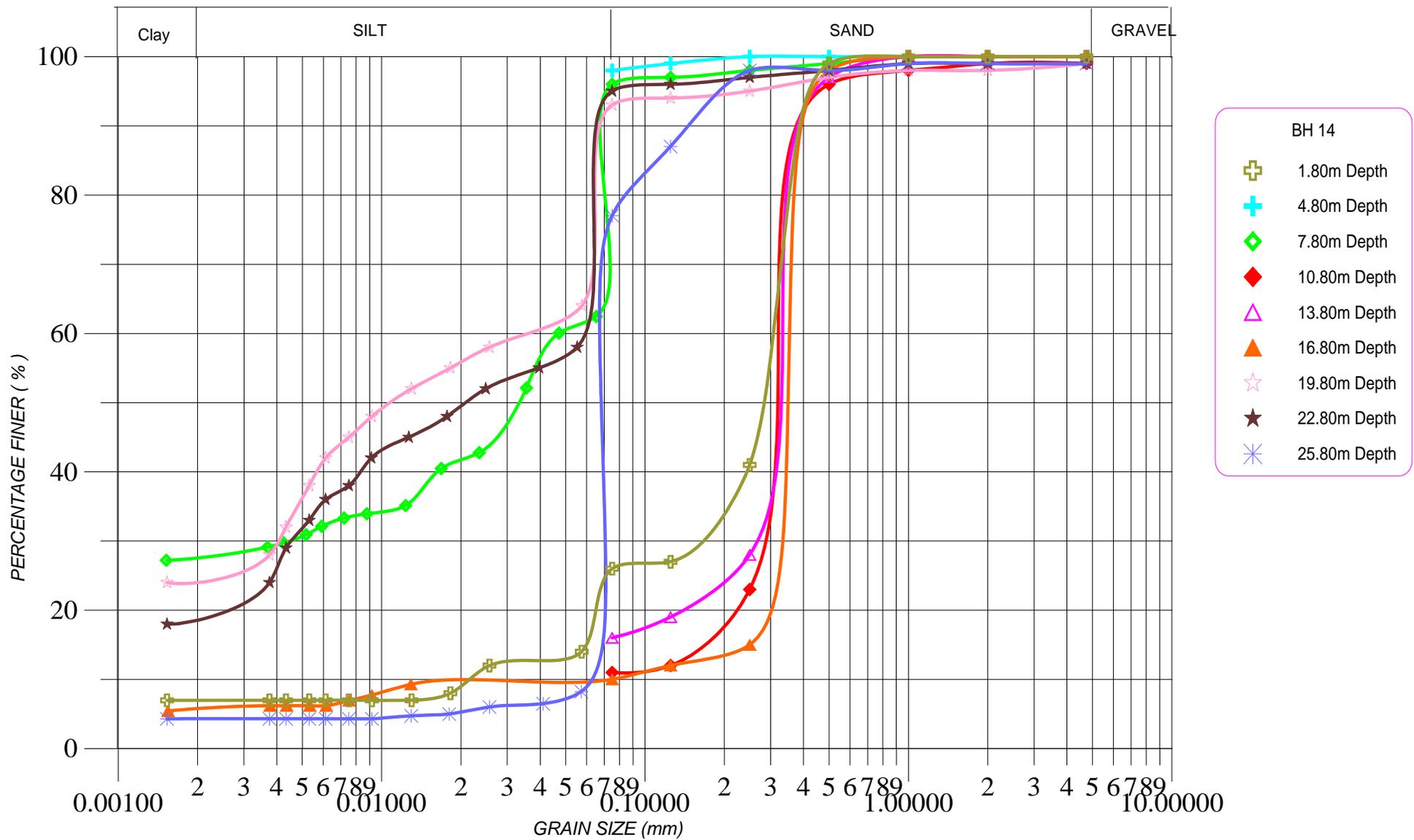
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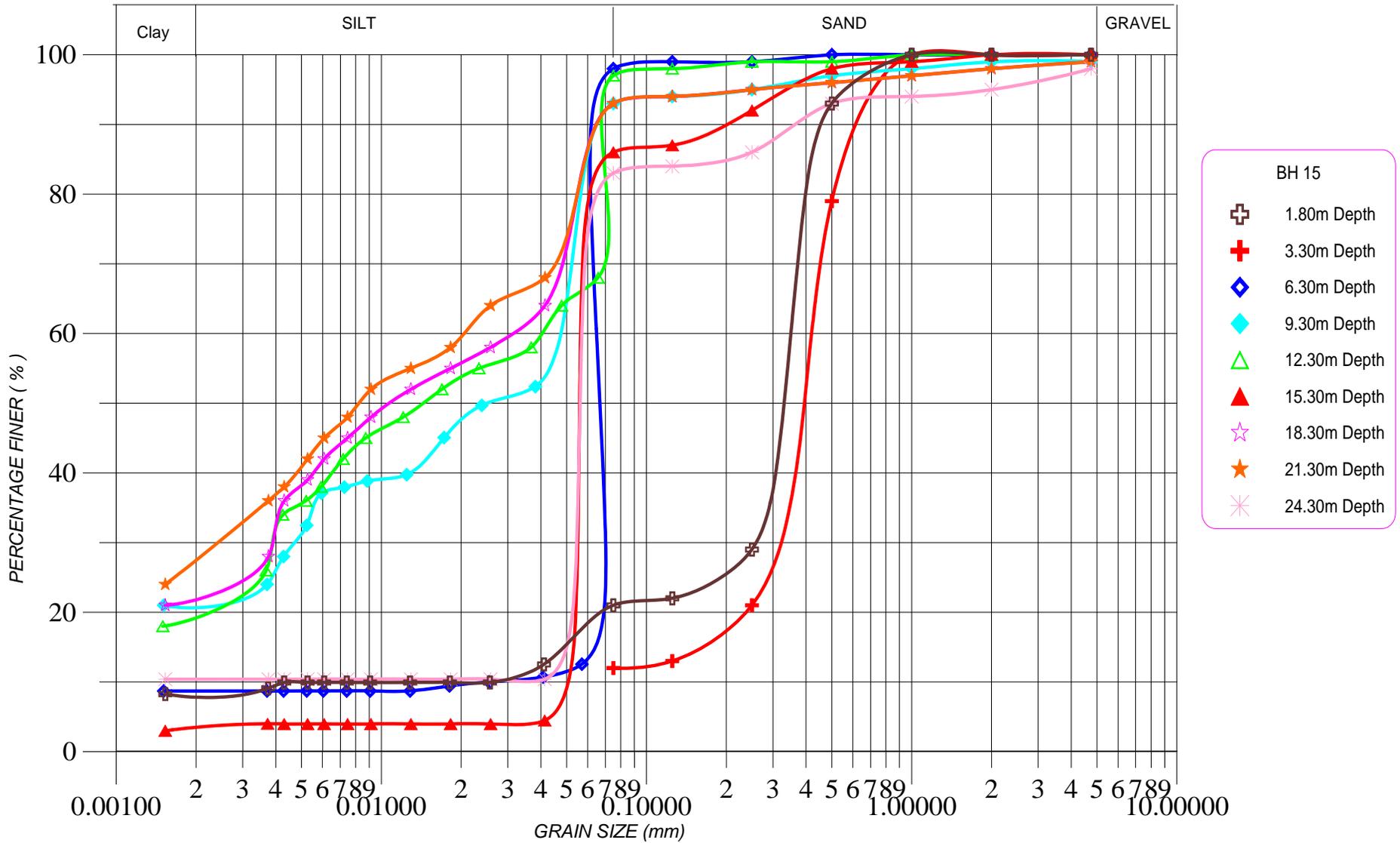
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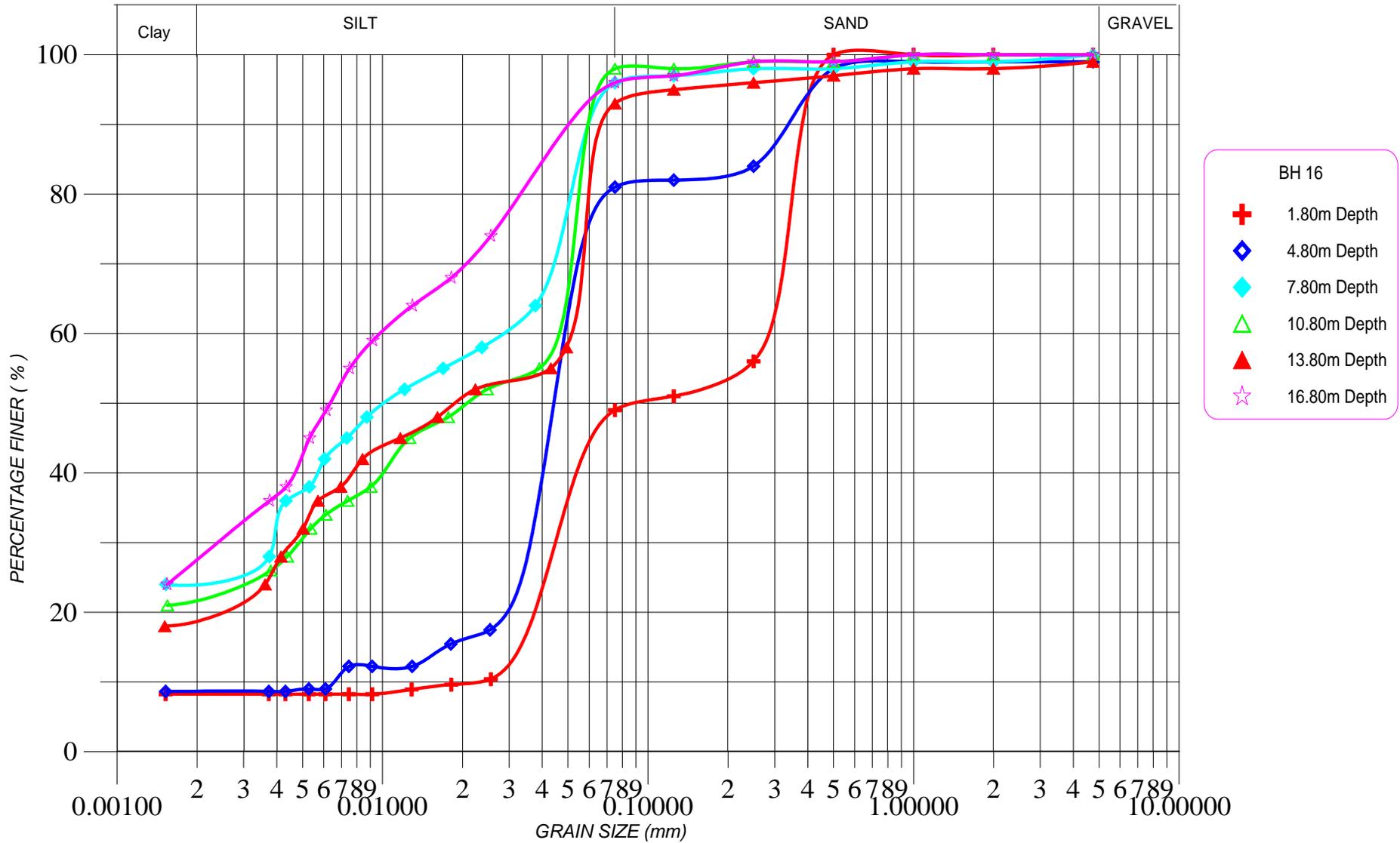
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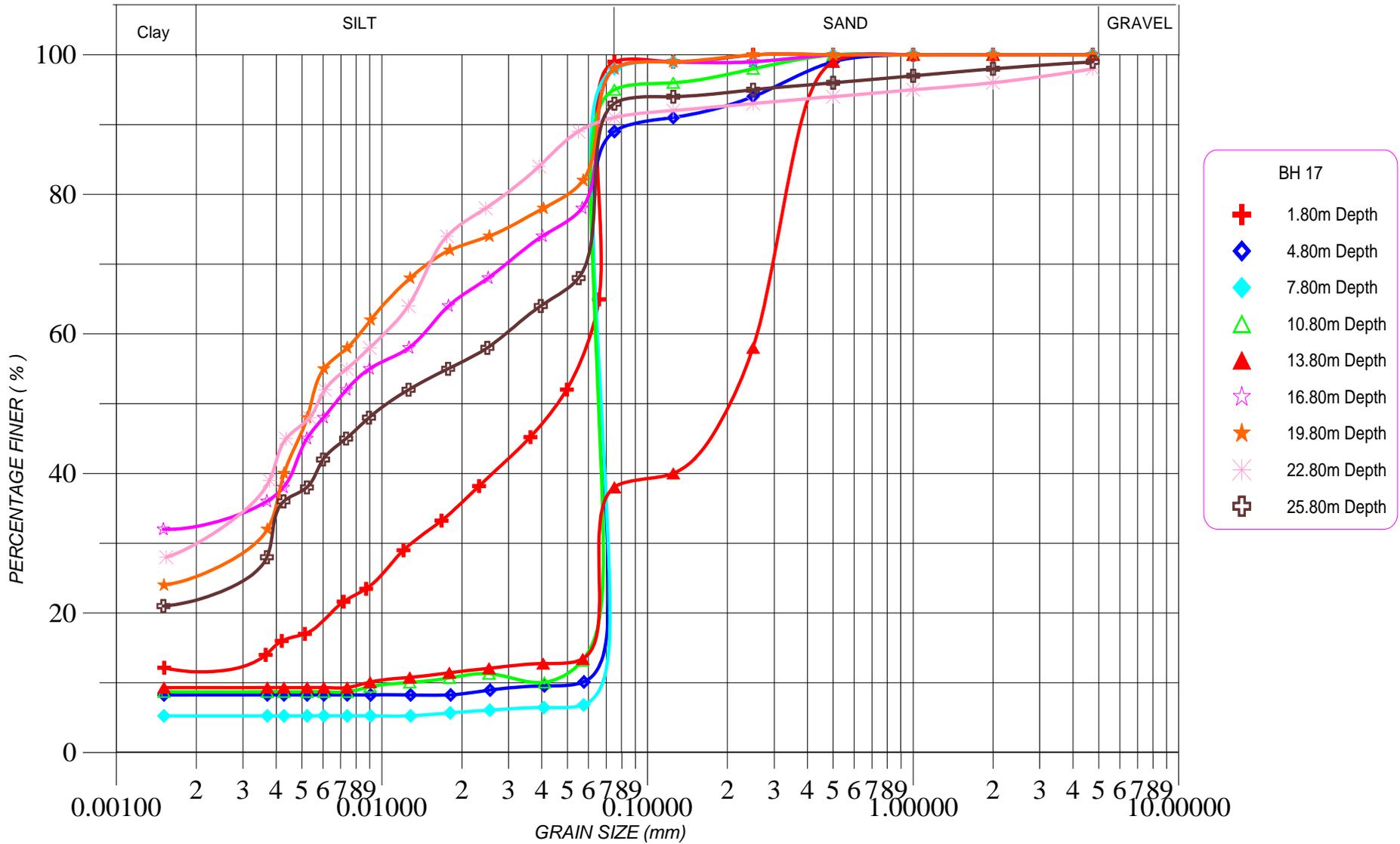
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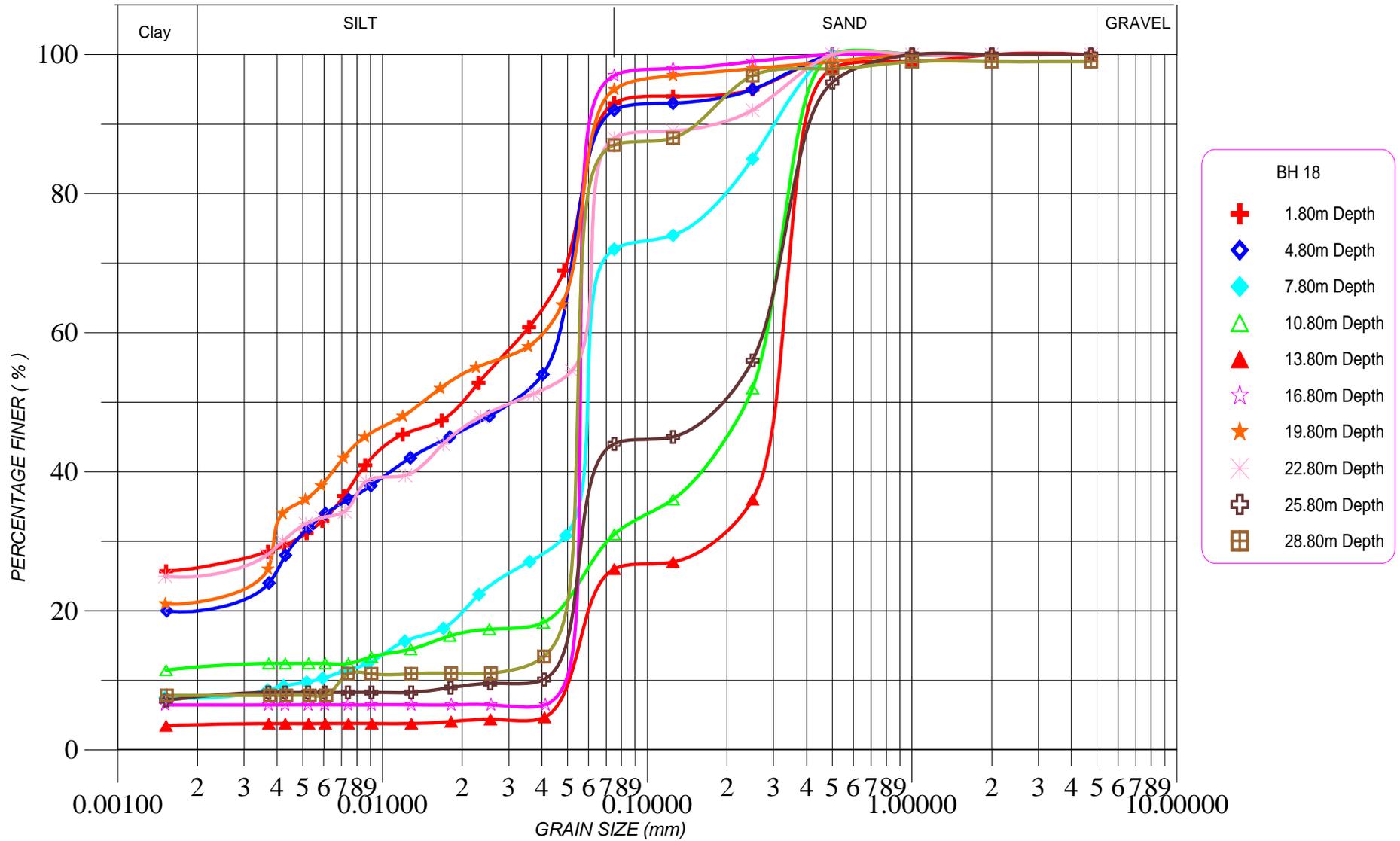
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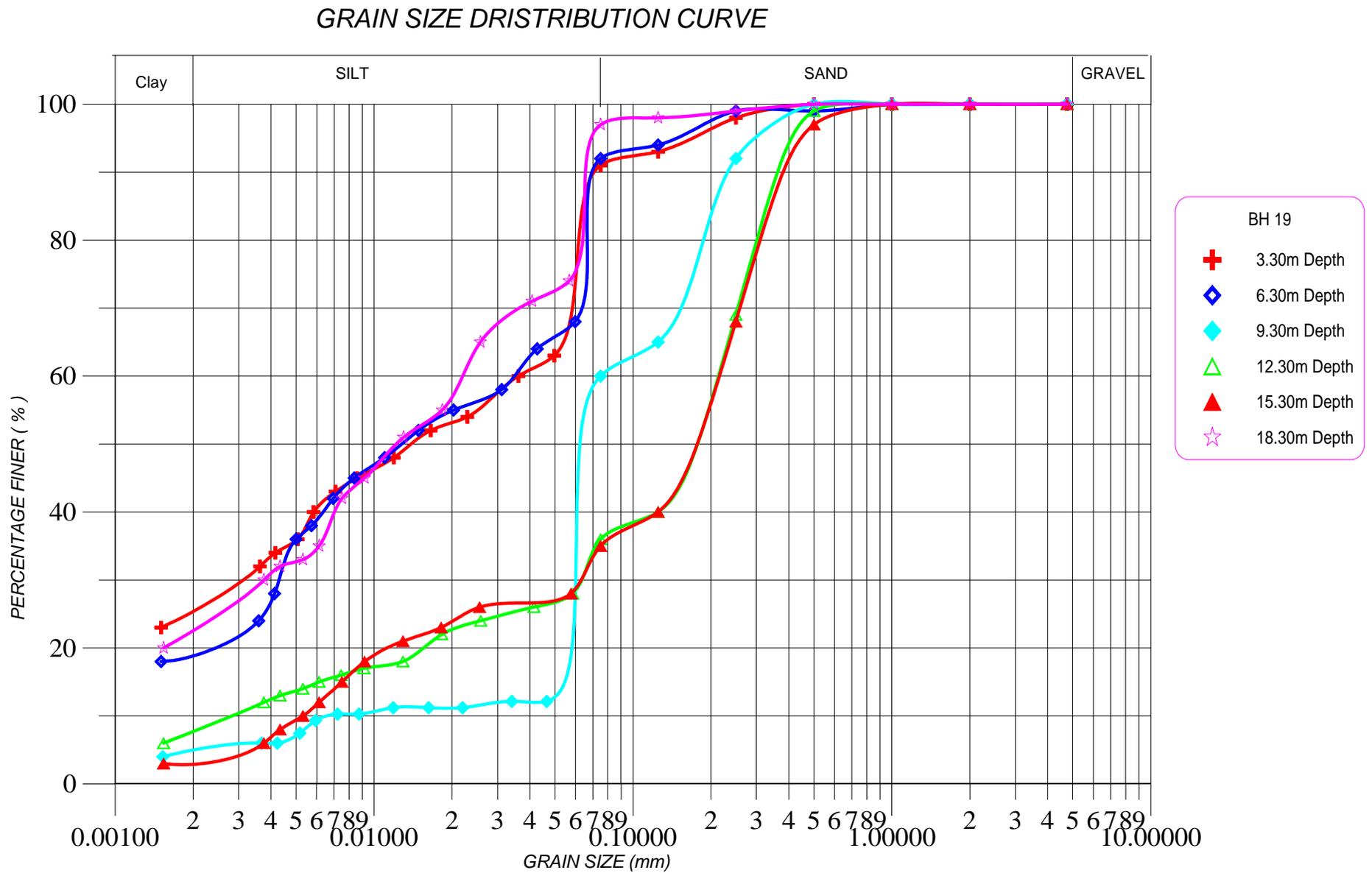


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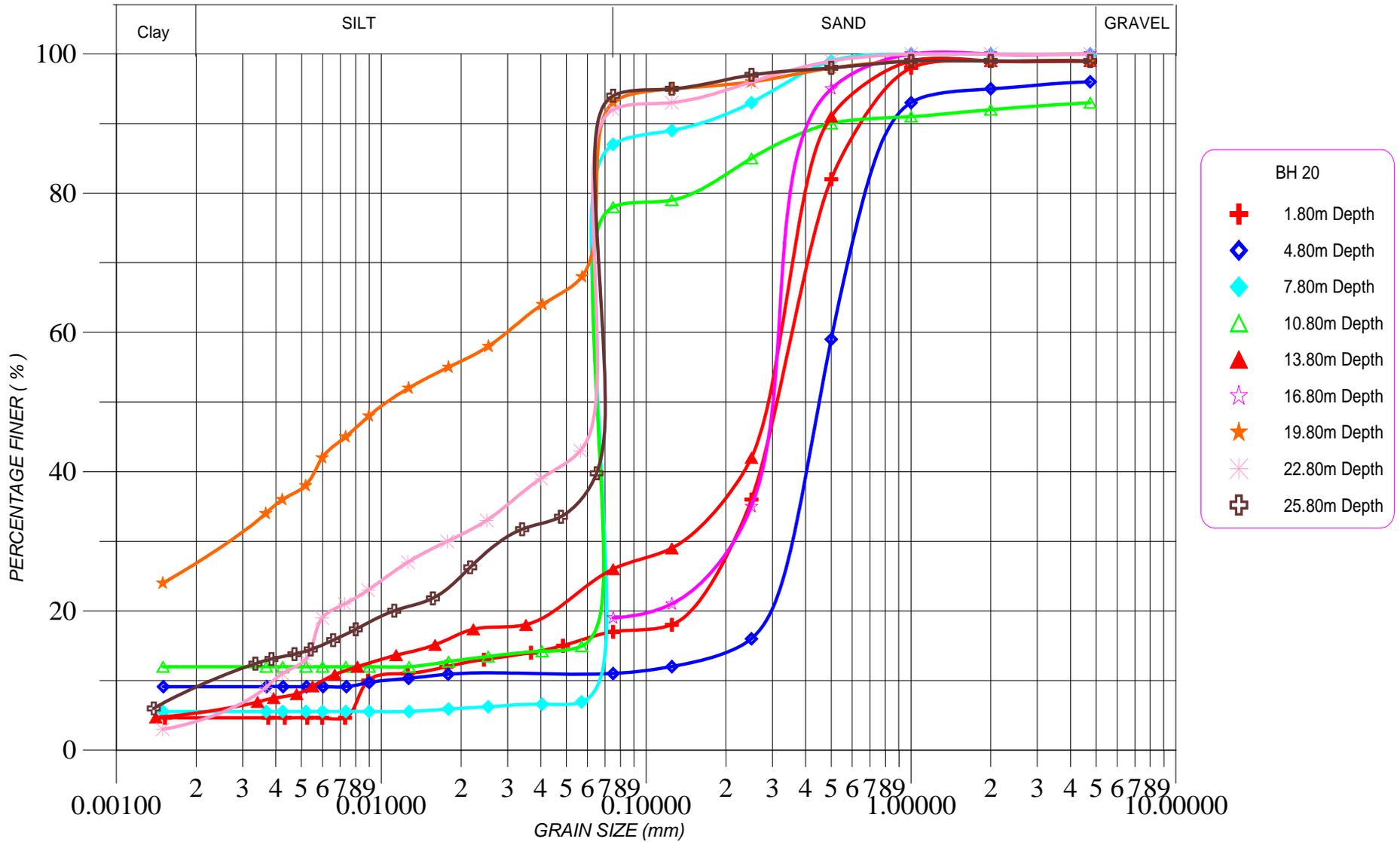


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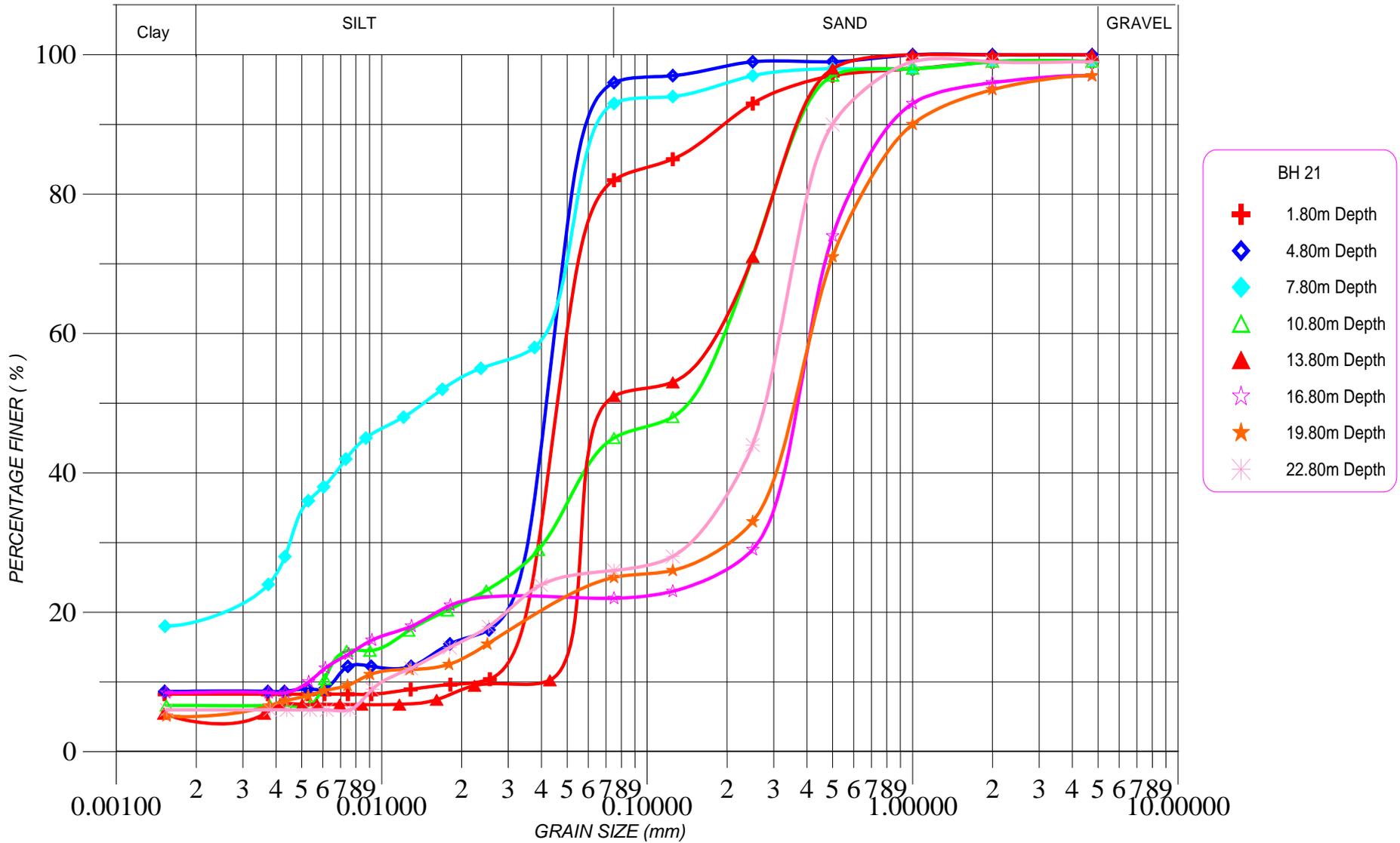




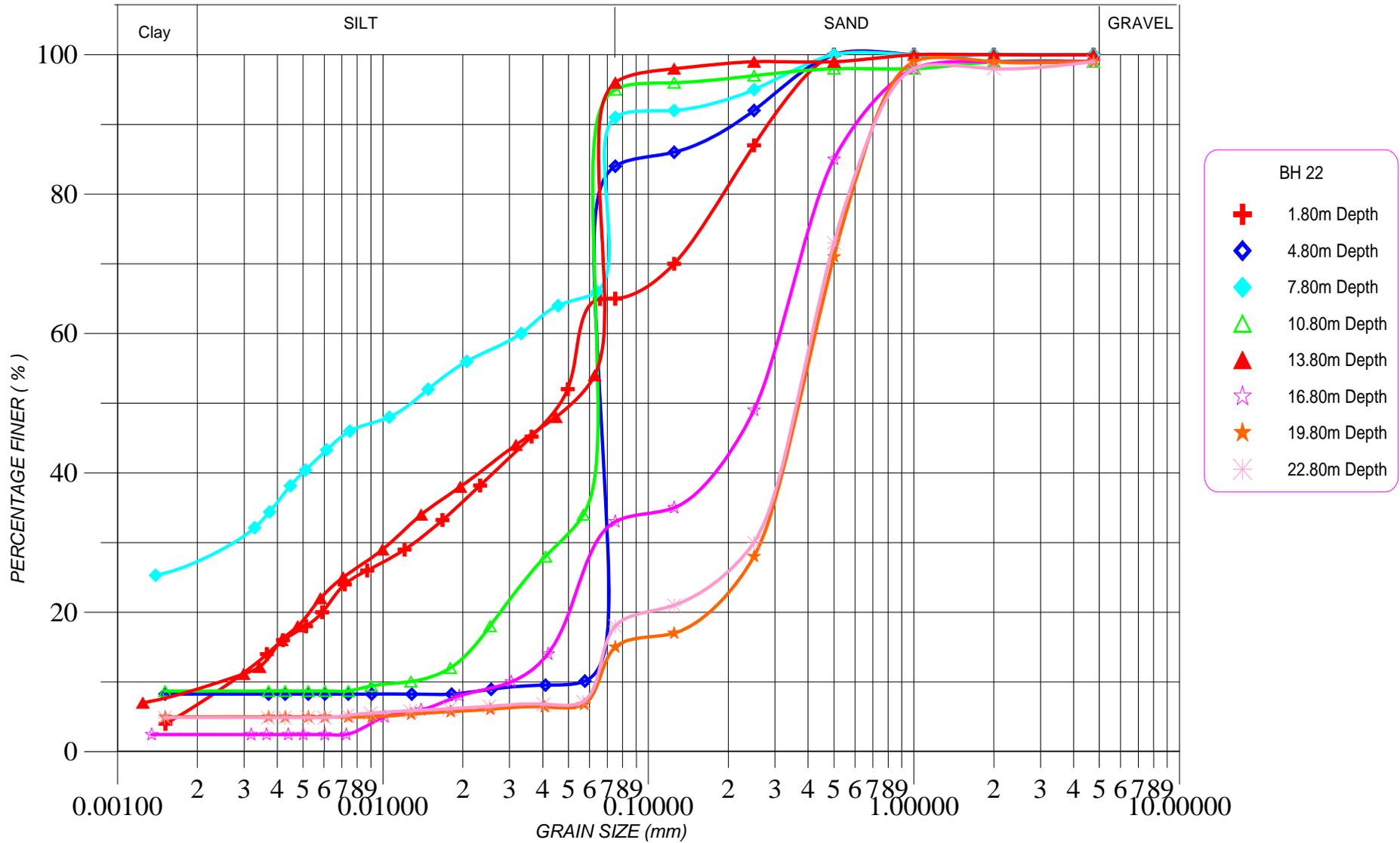
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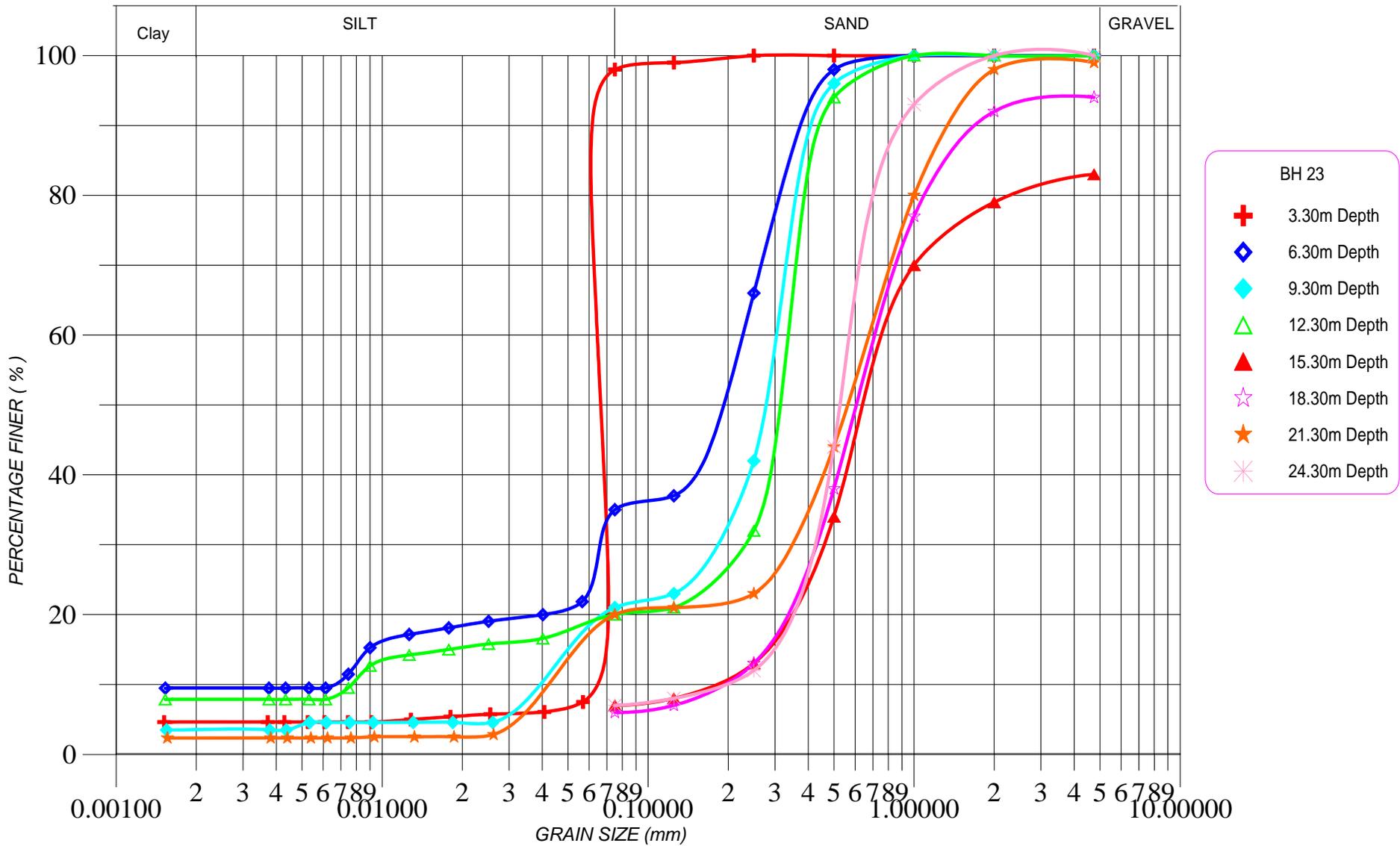
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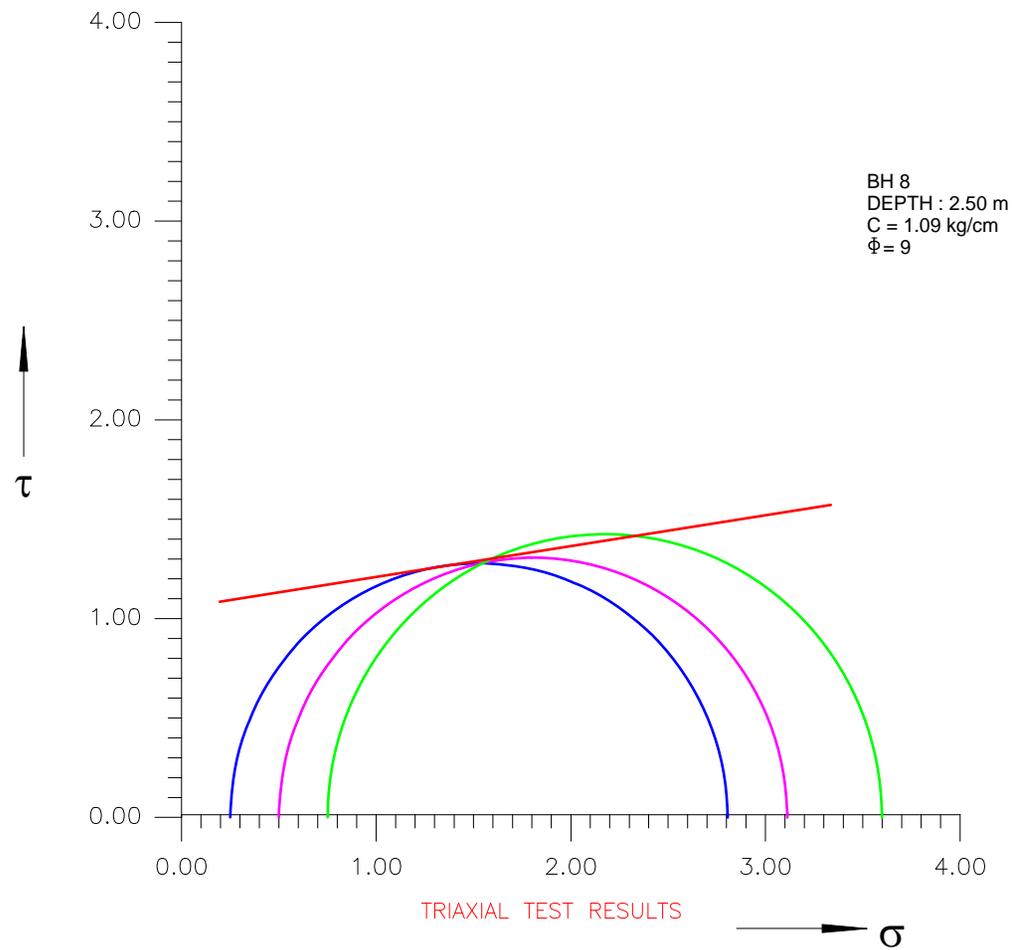


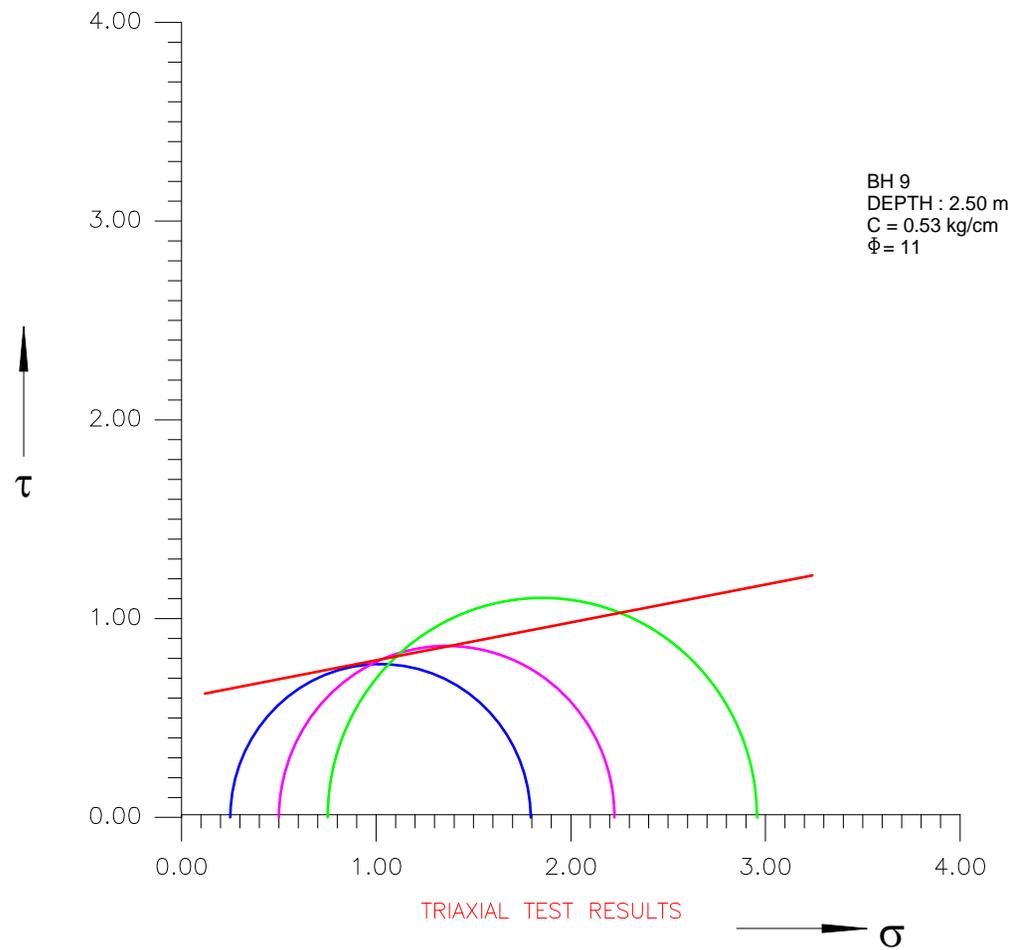
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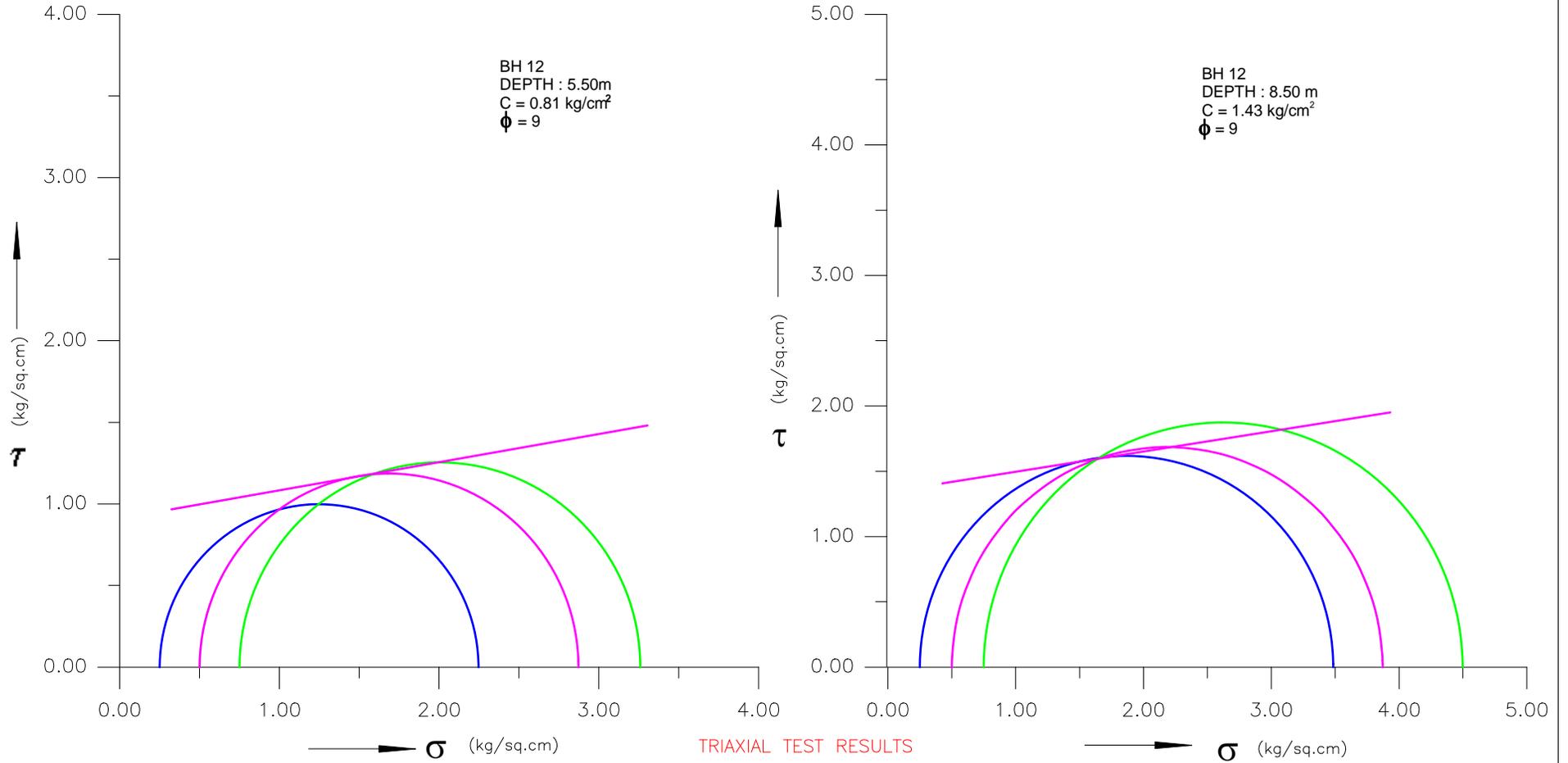


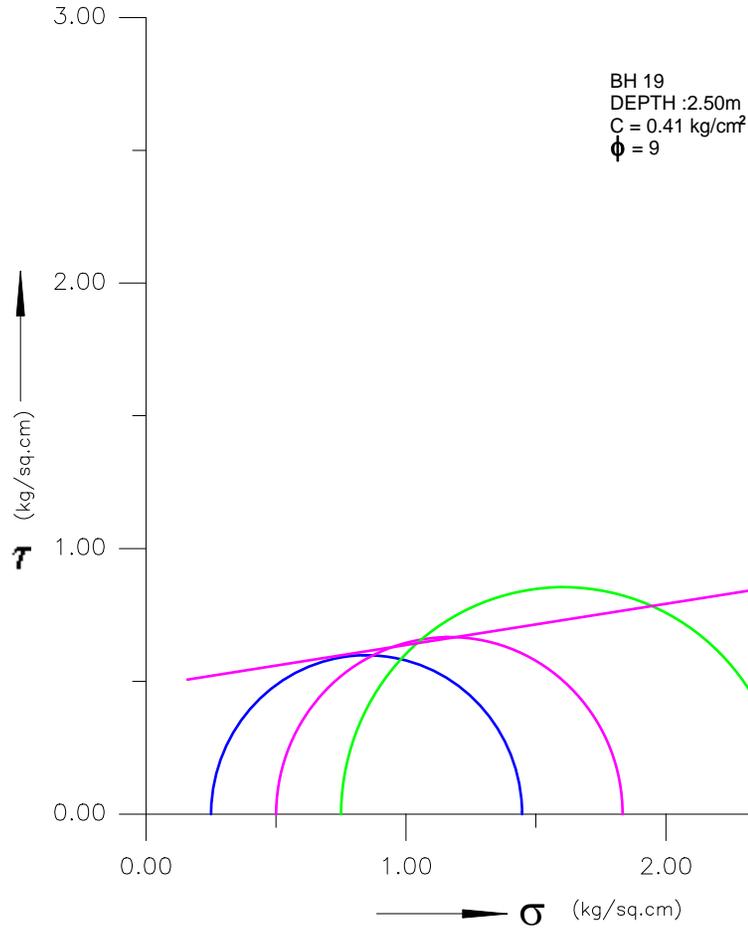
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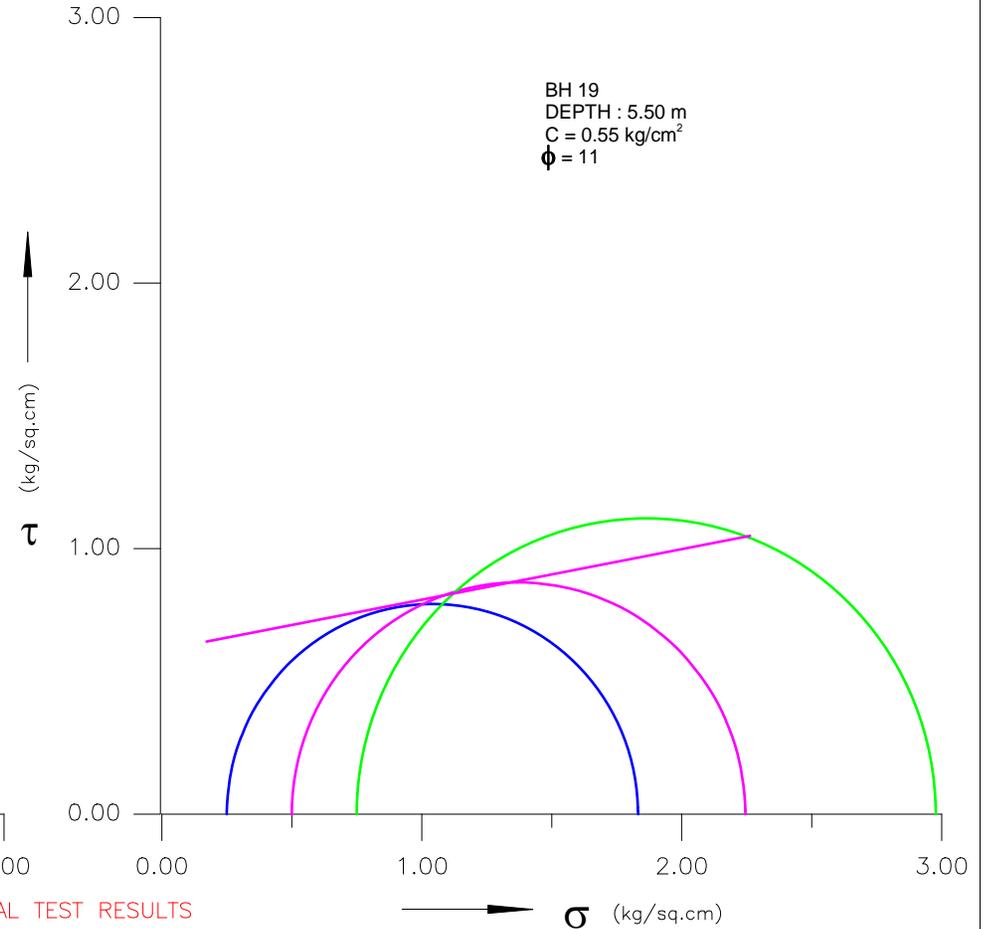


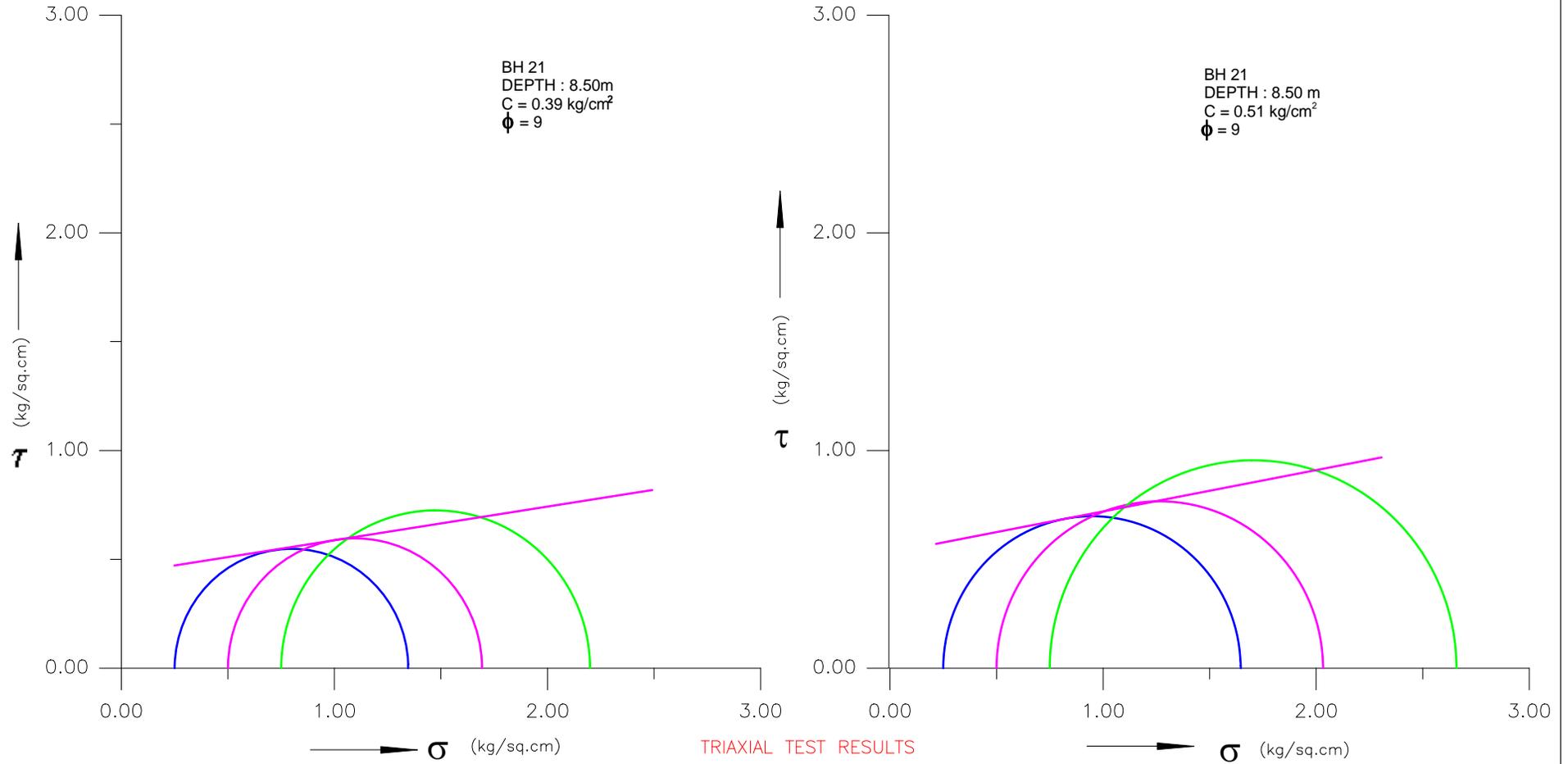






TRIAxIAL TEST RESULTS





Annexure VI  
Site Photograph's



Flyover @ 0+800



**MJB @ CH 1+530**



**VUP @ CH 6+280**



**Flyover @ CH 8+020**



VUP @ CH 16+690



VUP@ CH 22+980



**VUP @ CH 25+430**



**MNB @ CH 29+260**



**Flyover @ CH 32+170**



**MJB @ CH 33+420**



**MJB @ CH 33+490**



**MJB @ CH 35+860**



**MNB @ CH 38+010**



**MJB @ CH 39+580**



**MJB @ CH 39+690**



**VUP @ CH 40+960**



**MJB @ CH 42+550**



**Flyover @ CH 43+910**



**MJB @ CH 47+950**



**Flyover @ CH 49+900**

# Transys Consulting Pvt. Ltd

## Geotechnical Investigation work for Proposed Greenfield project from Spur to Haridwar.

Job No 2152

### *Report* *ROB @ 7+530 & 27+120-R0*



### **Soil Engineering Consultants**

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## 1.0 INTRODUCTION

M/s Transys Consulting Pvt Ltd has awarded the work of Geo technical Investigation for the proposed Greenfield project from Spur to Haridwar to M/s Soil Engineering Consultants, New Delhi.

Geotechnical investigation was conducted to characterize and assess the subsurface conditions at the locations of various Structures viz. proposed ROB's. The overall objectives of the exploration were to study and evaluate the stratigraphy of the said project corridor and to obtain geotechnical / geological parameters of the subsurface formations for design and construction of various foundations.

This report presents the details of Geotechnical investigations carried out and data obtained from various field and laboratory tests, their presentation in graphical form, and their compilation for the proposed Structures.

## 2.0 SCOPE OF WORK

- a) Drilling bore holes upto the maximum depth of 30.0 m as per IS code of practice and as per the direction of the Engineer-in-Charge.
- b) Conducting Standard Penetration tests in the bore holes at regular intervals of 1.50m or wherever possible as per IS Code of Practice.
- c) Collecting undisturbed soil samples / core samples from the bore holes at regular intervals or change of strata or wherever possible as per IS Code of Practice.
- d) Recording of water table level in the bore holes after completion of borehole.
- e) Preparation of report summarizing the details of soil classification, analysis of test data, type of foundation etc.



### 3.0 FIELD WORK

#### 3.1 Boring

Bore holes of 150 mm dia. were drilled as per IS code of practice (IS 1892-1979) and as per the directions of the Engineer in charge. The details of Bore holes drilled, Depth of bore hole and the depth of water table are as given below:

**Table 1 : Detail of the Boreholes.**

Change	BH No.	Structure	Depth of Borehole (m)	Water Table (m)
7+530	BH 7	ROB	30.00	15.30
27+120	BH 11	ROB	30.00	15.70

#### 3.2 Standard Penetration Test (SPT)

These tests were conducted at every 1.50m intervals and every change of strata or wherever possible. The tests were performed by driving into the soil (bore holes cleaned of any loose material) a standard split spoon sampler with the help of a standard hammer with a free fall of 75 cms on a driving head as described in IS: 2131. This head was attached to "A" drill rod to the other end of which the sampler was fitted. The number of blows needed to penetrate the first, second and third stages (each of 15 cms) depth of the sampler length, were noted. The number of blows (N - value) as given in the bore hole data sheets is the numerical sum of blows counted during the second & third stage only i.e. for a depth of 30 cms.

#### 3.3 Collection of Samples

Disturbed and Undisturbed soil samples were collected from the boreholes at regular intervals as per IS Code of practice.

#### 3.4 Recording of water table

Water table was met at varying depth in the boreholes at the time of Soil investigation which was carried out during the month of April 2021. The details are given at Table I above. Fluctuations may occur in measured

water levels due to seasonal variation in rainfall and surface evaporation rates as well as flow of water.

## 4.0 LABORATORY TESTS

A visual and discrete examination of all the soil samples collected was carried out for deciding the number and type of tests to be tested from each bore hole. Based on the strata met at site the following tests were conducted on samples to classify them and to evaluate their index and Engineering properties.

### 4.1 SOIL SAMPLES & BIS CODES

- a) Grain size distribution as per IS: 2720(Part IV).
- b) Hydrometer Analysis as per IS: 2720(Part IV).
- c) Specific gravity as per IS: 2720(Part III).
- d) Bulk density and dry density as per IS: 2720(Part II).
- e) Moisture content as per IS: 2720(Part II).
- f) Liquid and plastic limits as per IS: 2720(Part V).
- g) Direct Shear Tests as per IS: 2720 (Part XIII).

## 5.0 General Geology of the Area

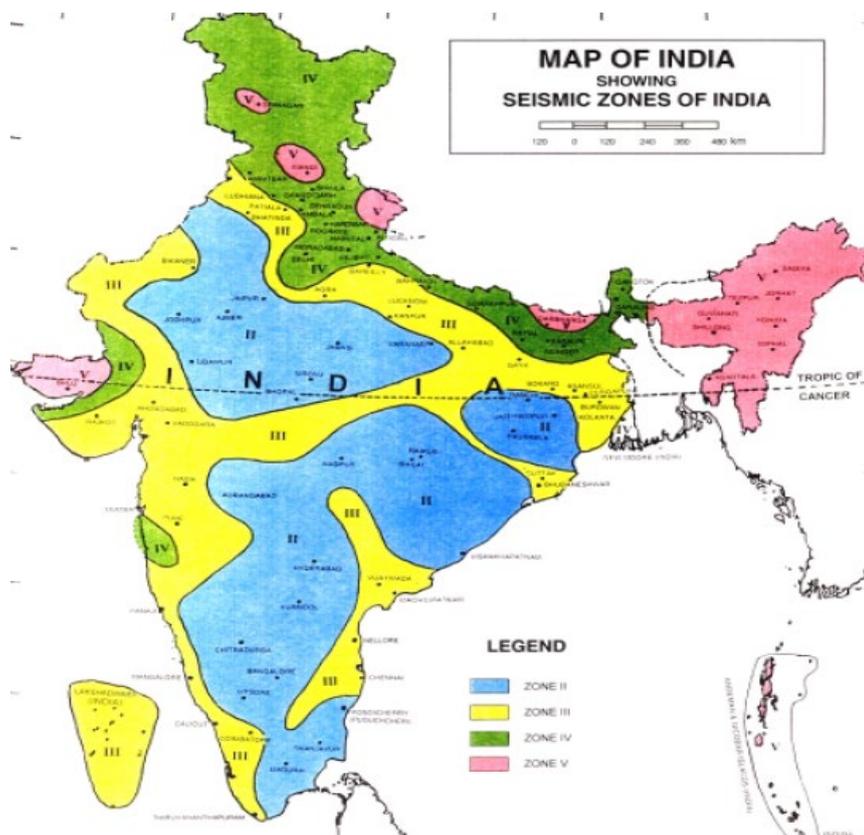
The present location is in the state of Uttarakhand situated on the northern Gangetic plains of India. Most of the state of Uttarakhand lies in the Gangetic Plain. This is a fore-deep, a downwarp of the Himalayan foreland, of variable depth, converted into flat plains by long-vigorous sedimentation. This is known as a geosyncline and the Gangetic Plain is the Indo-Gangetic Geosyncline. This has shown considerable amounts of flexure and dislocation at the northern end and is bounded on the north by the Himalayan Frontal Thrust. The floor of the Gangetic trough (if see without all the sediments) is not an even plain, but shows corrugated inequalities and buried ridges (shelf faults). Beneath Uttar Pradesh, run the Delhi-Haridwar Ridge (DHR), trending NNE-SSW along New Delhi to the Gharwal region. The Delhi-Muzaffarnagar Ridge (DMR), which trends east

to west, running from New Delhi to Kathgodam, in Nepal. The last ridge is the Faizabad ridge (FR), which runs in a curved manner, first east to west from Allahabad to Kanpur and then starts to bend towards the north-east towards Lucknow and carries on in this direction towards the Himalayas in Nepal. The depression that forms between the DMR and the FR, forms the West Uttar Pradesh shelf in the west and the Sharda Depression in the east. The region to the south of the FR, forms the East Uttar Pradesh shelf. There are several faults in the region, among them the Moradabad Fault which trends NE-SW and the Bhairwan Fault in the vicinity of Allahabad. Apart from these there are east-west running tear faults in the region that control the courses of the main rivers. Earthquakes have occurred in mostly all parts of Uttarakhand. Major earthquakes in the neighbouring states of New Delhi, Uttaranchal, Bihar and from across the Indo-Nepal border have also shaken many parts of Uttar Pradesh. However, it must be stated that proximity to faults does not necessarily translate into a higher hazard as compared to areas located further away, as damage from earthquakes depends on numerous factors such as subsurface geology as well as adherence to the building codes.

## 6.0 SEISMICITY

The seismic hazard map of India was updated in 2016 by the Bureau of Indian Standard (BIS). The project site lies in Zone IV. The tectonic elements of the area are considered capable of generating an earthquake of intensity MSK 7.0. In Seismic design Zone factor,  $Z$  of 0.24 is recommended.

### Seismic Map



## 7.0 LIQUEFACTION

Liquefaction is a process in which a saturated soil loose strength during an earthquake and acquires a degree of mobility sufficient to permit significant movements. In general, fine uniform sands are found to be most susceptible for liquefaction in terms of grain size. It can be stated that soils containing less than 10% fines,  $D_{60}$  between 0.20 mm to 1.0mm, uniformity coefficient between 2 to 5 are most susceptible to liquefaction for given relative density of soil and intensity of earthquake. Thus, uniformly graded materials are more susceptible to liquefaction than well graded materials. Also fine sands are more susceptible than gravelly soils, silty sands, silts or clays.

Assessment of liquefaction potential of foundation strata is made by simplified approach proposed by Seed & Idriss (1983 - 1985) from the SPT data and peak ground acceleration likely to occur at the site. In this method, cyclic shear stress likely to be induced in the foundation strata is

first evaluated. Next threshold cyclic shear stress, which is good enough to cause liquefaction, is determined from SPT data and the empirical relations. Finally, comparison of these two stresses is used in the estimation of liquefaction susceptibility of the foundation strata

## 7.1 Liquefaction Analysis:

### Cyclic Stress Ratio under Earth Quake (CSR)

Stress ratio under earth quake (CSR)

$$= (\tau / \sigma_o)_{\text{earthquake}} = 0.65 (\gamma h a_{\text{max}} / \sigma_o g) \lambda$$

$\sigma_o$  = Effective overburden pressure at depth h

$\gamma$  = Bulk density of soil

$a_{\text{max}}$  = Max. Ground acceleration = 0.24g

### Evaluation of Liquefaction Resistance (CRR)

$$CRR_{7.50} = 1 / \{ (34 - (N_1)_{60CS}) + (N_1)_{60CS} / 135 + 50 / \{ 10 * (N_1)_{60CS} + 45 \}^2 - 1 / 200$$

$$(N_1)_{60} = NC_{60} C_N$$

N = Uncorrected SPT count

$C_N$  = factor to normalize  $N_m$  to a common reference effective overburden stress =  $(p_o / \sigma_o)^{0.5}$

$$C_{60} = C_{HT} C_{HW} C_{SS} C_{RL} C_{BD}$$

$C_{HT}$  = Correction for Hammer Energy Ratio

$C_{BD}$  = Correction factor for the borehole diameter

$C_{RL}$  = correction factor for rod length

$C_{SS}$  = Correction for samples with or without liners

Correction for Fineness content

$$(N_1)_{60CS} = \alpha + \beta (N_1)_{60}$$

$$CRR_L = CRR_{7.50} * k_m$$

$k_m$  Correction factor

For earthquake magnitude other than 7.5 =  $10^{2.24 / (M_{7.5})^{2.56}}$

Liquefaction occurs if  $CSR_L \geq CRR$

### Data considered for Liquefaction:

Magnitude of Earth quake = 7.0.

$$a_{\max}/g = 0.24$$

Water table assumed for Calculation = considered 3.0m rise water table encounter at the time investigation.

The Liquefaction analysis has been calculated and given at **Annexure II**.

## 8.0 SUB SOIL PROFILE & STRENGTH CHARACTERISTICS OF SOIL

### ROB @ 7+ 530

At this structure One Borehole namely (BH 4) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto the depth drilled. However from 22.0m to 22.50m depth a layer of Silty Clay of Medium Plasticity (CI) was observed. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However, at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and High water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 9 to 40 upto the depth drilled. For evaluating the shear parameters Direct shear Tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is not susceptible to liquefaction.

### **ROB @ 27+120**

At this structure One Borehole namely (BH 11) was drilled upto 30.0m depth. While advancing the bore holes SPT tests were conducted at regular intervals of 1.5m and representative samples were collected. These representative samples were analysed for soil classification by conducting sieve analysis, Hydrometer analysis & Atterberg Limits. From the classification it is revealed that the strata predominately consists of medium dense Sandy Silt with Gravel (SM-ML)/ Silty Sand with Gravel (SM) upto the depth drilled. However from 23.0m to 26.5m depth a layer of Silty Clay of High Plasticity (CH) was observed. Attempts were made to collect Undisturbed soil samples at regular intervals of 3.0m depth. However, at greater depth some of the samples could not be collected due to presence of very dense/ Hard strata and water table. The SPT values has been corrected for Overburden strata and dilatancy in non- plastic strata. These corrected values have been plotted against depth and are shown in the respective borelogs. It can be seen from the plot that the SPT values are generally varying from 9 to 40 upto the depth drilled. However at greater depths SPT values above 40 were observed this might be due to the presence of Hard/Very dense strata. For evaluating the shear parameters Direct shear Tests/Unconsolidated undrained shear tests were conducted on the UDS samples collected. The results are given in the respective borelog. Liquefaction analysis has been carried out and the details are given at Annexure II. It can be seen from the results that the strata is not susceptible to liquefaction.

### **9.0 DESIGN CRITERIA**

Any foundation is to be safe against possible failure against

- a) Excessive Shear failure (the bearing pressure should be within permissible limits) and
- b) Excessive settlement.

The latter depends upon not only on the type of soil in the foundation but also on the type of foundation, material used for construction and functionality of the structure.

## 9.1 Design Methodology

### ROB @ 7+530 & 27+120

Bored - Cast - in situ Piles of 1.0m and 1.20m diameter are analyzed.

#### 9.1.1 Bored cast in-situ concrete pile

The ultimate load carrying capacity ( $P_u$ ) of piles is given by the following formula:

$$P_u = A_p ( N_c \cdot C_p + \frac{1}{2} D \gamma N_r + P_d N_q ) + \sum K P_{di} \tan \delta A_{si} + \alpha c \cdot A_s$$

$$P_u = P_{pu} + P_{su}$$

$P_{pu}$  = Ultimate bearing resistance

$$= A_p ( N_c \cdot C_p + \frac{1}{2} D \gamma N_r + P_d N_q )$$

$P_{su}$  = Ultimate shaft resistance

$$\sum K P_{di} \tan \delta A_{si} + \alpha c \cdot A_s$$

$A_p$  = Cross sectional area of the pile toe  $m^2$

$D$  = Stem diameter in mm

$\gamma$  = Effective unit weight of soil at pile toe in  $t/m^3$

$P_d$  = Effective overburden pressure at pile toe in  $t/m^2$

i.e 20 X diameter (as per IRC 78-2014).

$N_r$  &  $N_q$  = Bearing capacity factors depending upon the angle of internal friction  $\phi$  at toe

$\sum$  = Summation of n layers in which pile is installed

$K$  = Coefficient of earth pressure

= Taken 1.5 (as per IRC 78- 2014 Appendix 5)

$P_{di}$  = Effective overburden pressure in  $t/m^2$  for the  $i^{th}$  layer where  $i$  varies from  $i$  to  $n$

$\delta$  = Angle of wall friction between pile and soil (may be taken equal to  $\phi$ )

$A_{si}$  = Surface area of pile stem in  $m^2$  in  $i^{th}$  layer where  $i$  varies from 1 to  $n$ .

FOS= Factor of Safety considered as 2.5 ( as per IS 2911 part 1 sec 2)

For vertical Capacity of pile, weight of pile has not been considered.

## 10.0 COMPUTATIONS

The Vertical, Uplift and lateral carrying capacities of the Bored Cast in Situ Piles of 1.0m and 1.20m dia are calculated and are given at **Annexure I**.

## 11.0 RECOMMENDATIONS

### ROB @ 7+530 & 27+120

Bored Cast in-situ Pile Foundation of 1.0 m and 1.20m dia are recommended at cut off level of 2.0m and 2.30m respectively. The Length of pile and Safe load carrying capacity of the pile can be taken as given below:

Chainage	BH No.	Pile Dia (cms)	Length of Pile (m)	Safe Load carrying capacity of Pile (t)		
				Vertical	Uplift	Lateral
7+530	BH 7	100	25.0	340.0	180.0	30.0
		120	25.0	450.0	200.0	50.0
27+120	BH 10	100	25.0	400.0	210.0	30.0
		120	25.0	500.0	270.0	50.0

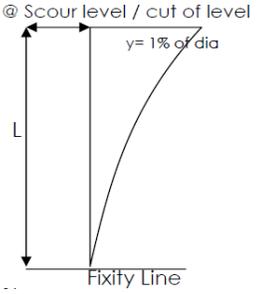
**For Soil Engineering Consultants**

**(A.V.S. RANGA RAO)  
Consultant**

Annexure I  
(Calculation)





Project no : 2152	Lateral Load Capacity of pile		
	[As per IS 2911-2010 Part 1Section-2] Annex-C		
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.		
Structure @ Chainage :	ROB @ 7+530		
Borehole no :	BH 4		
Type of pile :	Bored cast in situ	Bored cast in situ	
Diameter of the pile in "mm" :	1000	1200	
Cut off Level of the Pile in "m" :	2.000	2.300	
Length of the Pile below the cut off level in "m" :	25.0	25.0	
Type of Pile Head :	fixed	fixed	
Crossection of the Pile :	Circle	Circle	
Gade of the concrete (M):	35.0	35.0	
Type of Soil :	Granular	Granular	
Condition of Soil with w.r.t Ground water :	Submerged	Submerged	
No. of Blow (N)	21.00	21.00	
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07	
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05	
Modulus of subgrade reaction for granular soil (K1) in Kn/m3 :	2.98E+03	2.98E+03	
Stiffness factor for Cohesionless soil (T) in m :	3.43	3.97	
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	0.000	0.000	
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	0.00	0.00	
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	25.00	25.00	
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R [As per Appendix C, Clause 5.5.2 Fig 2]:	2.19	2.19	
Depth of Fixidity L <sub>f</sub> in "m":	7.51	8.69	
Depth of Fixity + free standing length (L <sub>xx</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	7.51	8.69	
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile	
<b>Considering 1% of dia for Horizontal Deflection :</b>			
Permissible Horizontal Deflection pile (Y) " in mm":	10.00	12.00	
Lateral capcity of pile ,Q (Tonnes) for 1% dia. deflection :	41.10	65.97	
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	35.00	50.00	
Equations :	$T = (EI/n_h)^{1/5}; R = (EI/K_1)^{1/4}$		
	$\text{For Free Head (Y)} = [QLxx^3]/3EI; \text{ For Fixed head (Y)} = [QLxx^3]/12EI$		





**Design of Pile Foundation**  
**Estimation of Safe Vertical Load carrying Capacity of "Bored Cast in situ Concrete Pile"as per IRC 78-2014**

Name of Project	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			Structure @ Chainage	27+120	Location	ROB	Based on Bore Hole No	BH 10	Pile Cut-off level (m)	2.3
Type of Pile Foundation	Bored Cast-in-situ Concrete Pile	Inclination of pile with Vertical Axis (deg)	0	Factor of Safety for base Resitance	2.5	Actual Water table (m)	15.70	water Level considered (m)	0.00	Scour Level @ RL(m)	
File Diameter (mm)	1200	Earth Presure Coefficient Ks	1.5	Factor of Safety for Shaft Friction	2.5	Scour Level below the cut off level (m)	0.00	Liqefaction depth below Ground level (m)	0.00	RL of the Borehole (m)	
Maximum effective overburden pressure= 20*Diameter of pile. Assuming the strata @ 30 m and below to be same.						Scour level below cut-off level(m) :		0.000			

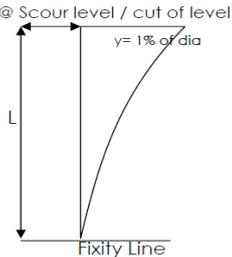
Layer No.	Type of Sub Soil Layer	Thickness of Layer (m)	Water table (W,T) m	Cohesion, C (t/m <sup>2</sup> )	Angle of Shearing Resistance, φ (deg)	Angle of Wall Friction δ(deg)	r (density of soil) t/m <sup>3</sup>	Total/ Submerged Unit Weight of Soil (t/m <sup>3</sup> )	Effective over-burden Pressure at pile tip "q <sub>tip</sub> " (t/m <sup>2</sup> )	Bearing Capacity Factors			Ultimate Base Resistance $P_{pu} = Ap^* (cN_c + P_d N_q + 0.5 \gamma_v D N_{\gamma})$					Ultimate Shaft Friction $P_{su} = (\sum (K_i P_{ai} \tan \delta) A_{si} + a.c.A_{si})$					Total Ultimate Capacity, $P_u = P_{pu} + P_{su}$ (tonnes)	Weight of pile, $W_p$ (Tonnes)	Total Safe Capacity, $P_s$ (Tonnes) $P_s = \frac{P_u}{2.5}$	Total safe uplift capacity (Tonnes)	Pile Length (meters)	
										$N_c$	$N_q$	$N_{\gamma}$	$A_p$ (m <sup>2</sup> )	$c.N_c$	$P_d N_q$	$0.5 \gamma_v D N_{\gamma}$	$P_{pu}$ (tonnes)	Effective overburden Pressure at c.g of the layer "P <sub>ai</sub> " (t/m <sup>2</sup> )	$A_{si}$ (m <sup>2</sup> )	$(K_i P_{ai} \tan \delta) A_{si}$	Adhesion Factor, a	a.c.A <sub>si</sub>						$P_{su}$
1	SM-ML / SM	1.7	0.00	0	30	30	1.84	1.03	1.75	0	20.9	22.4	1.13	0	36.66	13.000	56.11	0.87	6.4	4.82	0	0	0	56.11	2.68	22.44	2.68	1.7
2	SM-ML / SM	2	0.00	0	30	30	1.83	1.01	3.77	0	20.9	22.4	1.13	0	78.97	13.570	104.57	2.76	7.53	17.99	0	0	17.99	122.56	5.84	49.02	10.87	3.7
3	SM-ML / SM	3	0.00	0	30	30	1.83	0.99	6.74	0	20.9	22.4	1.13	0	141.19	13.300	174.57	5.25	11.3	51.37	0	0	69.36	243.93	10.58	97.57	30	6.7
4	SM-ML / SM	4	0.00	0	30	30	1.93	0.99	10.7	0	20.9	22.4	1.13	0	224.15	13.300	250.07	8.72	15.1	113.8	0	0	183.2	433.23	16.9	173.29	68.18	10.7
5	SM-ML / SM	3	0.00	0	30	30	1.9	0.99	13.67	0	20.9	22.4	1.13	0	286.37	13.300	265.69	12.18	11.3	119.19	0	0	302.4	568.04	21.64	227.21	106.29	13.7
6	SM-ML / SM	3	0.00	0	30	30	1.9	0.99	16.64	0	20.9	22.4	1.13	0	348.58	13.300	246.15	15.15	11.3	148.25	0	0	450.6	696.75	26.38	278.7	152.54	16.7
7	SM-ML / SM	2	0.00	0	30	30	1.9	0.99	18.62	0	20.9	22.4	1.13	0	390.06	13.300	213.6	17.63	7.53	114.96	0	0	565.6	779.16	29.54	311.66	187.89	18.7
8	CH	2	0.00	21	0	0	1.9	0.99	20.6	9	0	0	1.13	189	0	0.000	213.57	19.61	7.53	0	0.3	47.43	613	826.56	32.7	330.62	204.33	20.7
9	CH	1.5	0.00	21	0	0	1.9	1.02	22.13	9	0	0	1.13	189	0	0.000	213.57	21.36	5.65	0	0.3	35.59	648.6	862.15	35.07	344.86	216.67	22.2
10	SM-ML / SM	2.8	0.00	0	30	30	1.9	1.02	22.13	0	20.9	22.4	1.13	0	463.59	13.710	539	22.13	10.6	202.19	0	0	850.8	1389.77	39.49	555.9	277.7	25

**Recommendation :**

- a) Pile Diameter (mm)  
b) Pile cut off level (m)  
c) Pile Shaft Length from Cut off Level (m)  
d) Vertical Pile Capacity (tonnes)  
e) Uplift pile capacity (Tonnes)

1200
2.3
25.0
500.0
270.0

\* For vertical Capacity of Pile weight of the pile has not been considered.

Project no : 2152	Lateral Load Capacity of pile			
	[As per IS 2911-2010 Part 1Section-2] Annex-C			
Project :	Geotechnical Investigation Work for the Proposed Greenfield Project from Spur to Haridwar.			
Structure @ Chainage :	ROB @ 27+120			
Borehole no :	BH 10			
Type of pile :	Bored cast in situ	Bored cast in situ		
Diameter of the pile in "mm" :	1000	1200		
Cut off Level of the Pile in "m" :	2.000	2.300		
Length of the Pile below the cut off level in "m" :	25.0	25.0		
Type of Pile Head :	fixed	fixed		
Crosssection of the Pile :	Circle	Circle		
Gade of the concrete (M):	35.0	35.0		
Type of Soil :	Granular	Granular		
Condition of Soil with w.r.t Ground water :	Submerged	Submerged		
No. of Blow (N)	15.00	15.00		
Moment of Inertia , I in "cm <sup>4</sup> " :	4.909E+06	1.018E+07		
Modulus of elasticity of the Pile , E (Kg/cm <sup>2</sup> ) :	2.96E+05	2.96E+05		
Modulus of subgrade reaction for granular soil (K1) in Kn/m <sup>3</sup> :	2.12E+03	2.12E+03		
Stiffness factor for Cohesionless soil (T) in m :	3.67	4.25		
Free standing length of pile or length of the pile below cut off level not contributing substantially to lateral capacities (L <sub>1</sub> ) in "m":	0.000	0.000		
therefore L <sub>1</sub> /T or L <sub>1</sub> /R :	0.00	0.00		
Embedded Length of the Pile (L <sub>e</sub> ) in "m" :	25.00	25.00		
Reading from the graph L <sub>f</sub> /T or L <sub>f</sub> /R [As per Appendix C, Clause 5.5.2 Fig 2):	2.19	2.19		
Depth of Fixidity L <sub>f</sub> in "m":	8.04	9.31		
Depth of Fixity + free standing length (L <sub>fix</sub> =L <sub>1</sub> +L <sub>f</sub> ) in "m"	8.04	9.31		
Type of Pile Behaviour :	Long Flexible Pile	Long Flexible Pile		
<b>Considering 1% of dia for Horizontal Deflection :</b>				
Permissible Horizontal Deflection pile (Y) " in mm" :	<b>10.00</b>	<b>12.00</b>		
Lateral capcity of pile ,Q (Tonnes) for 1% dia. deflection :	33.56	53.77		
<b>Recommended Lateral Capacity of Pile (T) for 1% dia deflection :</b>	30.00	50.00		
Equations :				
$T = (EI/\eta_0)^{1/5}$ ; $R = (EI/K_1)^{1/4}$				
For Free Head (Y) = [QLxx <sup>3</sup> ]/3EI ; For Fixed head (Y) = [QLxx <sup>3</sup> ]/12EI				

Annexure II  
Liquefaction Analysis

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



**Project :** Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring		
<b>Location</b>		Magnitude of Earthquake	7.0	Efficiency in SPT Boring (for $C_E$ factor) "%"	60		
Structure @ Chainage	MNB @ 21+810	Design PGA	0.24 g	Borehole diameter (mm)	150		
Borehole no :	BH 7	Importance Factor of the Structure	1	Was liner used in SPT boring	No		
Water Table Depth (m)	11.30						
Water Table Depth considered (m)	7.00						

Depth below EGL, m	Type of Strata	Field SPT $N_{field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content ( % )	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_o$ ), $kN/m^2$	Effective overburden ( $s_o$ ) at site, $kN/m^2$	Effective overburden ( $s_o$ ) considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60cs</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM-ML	6	17.90	7.90	82	0.99	32.22	32.22	32.22	0.15	1.70	1.06	10.81	5.00	1.20	17.97	0.19	0.23	1.48	Non Liquefiable
3.3	SM-ML	10	17.90	7.90	70	0.97	59.07	59.07	59.07	0.15	1.30	1.06	13.79	5.00	1.20	21.55	0.24	0.28	1.85	Non Liquefiable
4.8	SM-ML	28	17.90	7.90	64	0.96	85.92	85.92	85.92	0.15	1.08	1.06	32.02	5.00	1.20	43.42	NA	NA	>1	Non Liquefiable
6.3	SM-ML	31	18.70	8.70	58	0.95	113.97	113.97	113.97	0.15	0.94	1.06	30.78	5.00	1.20	41.94	NA	NA	>1	Non Liquefiable
7.80	SM	18	18.70	8.70	48	0.94	142.02	142.02	134.02	0.16	0.84	1.06	16.01	5.00	1.20	24.21	0.28	0.33	2.13	Non Liquefiable
9.30	SM-ML	13	18.70	8.70	87	0.93	170.07	170.07	147.07	0.17	0.77	1.06	10.57	5.00	1.20	17.68	0.19	0.22	1.34	Non Liquefiable
10.80	SM-ML	11	18.20	8.20	83	0.89	197.37	197.37	159.37	0.17	0.71	1.06	8.30	5.00	1.20	14.96	0.16	0.19	1.11	Non Liquefiable
12.30	SM-ML	18	18.20	8.20	91	0.85	224.67	214.67	171.67	0.17	0.66	1.06	12.54	5.00	1.20	20.05	0.22	0.26	1.49	Non Liquefiable
13.80	SM-ML	19	18.20	8.20	98	0.81	251.97	226.97	183.97	0.17	0.63	1.06	12.77	5.00	1.20	20.32	0.22	0.26	1.52	Non Liquefiable
15.30	SM-ML	24	18.20	8.20	82	0.77	279.27	239.27	196.27	0.17	0.61	1.06	15.58	5.00	1.20	23.69	0.27	0.32	1.88	Non Liquefiable

## Liquefaction Potential Evaluation as per IRC SP 114-2018

## Computation Sheet



Project : Geotechnical Investigation Work for Proposed Greenfield project from Spur to Haridwar.

Borehole Details		Seismic Parameters			Parameters from SPT Boring	
<b>Location</b>		Magnitude of Earthquake	7	Efficiency in SPT Boring (for $C_E$ factor) "%"	60	
Structure @ Chainage	ROB @ 27+120	Design PGA	0.24 g	Borehole diameter (mm)	150	
Borehole no :	BH 10	Importance Factor of the Structure	1	Was liner used in SPT boring	No	
Water Table Depth (m)	15.70					
Water Table Depth considered (m)	11.00					

Depth below EGL, m	Type of Strata	Field SPT $N_{Field}$	Bulk unit weight ( $kN/m^3$ )	Submerged unit weight ( $kN/m^3$ )	Fines Content (%)	Stress reduction coefficient ( $r_d$ )	Total overburden pressure ( $s_v$ ), $kN/m^2$	Effective overburden ( $s_v$ ) at site, $kN/m^2$	Effective overburden ( $s_v$ ) at considered, $kN/m^2$	Cyclic Stress ratio (CSR)	$C_N$	$C_{60}$	SPT ( $N_1$ ) <sub>60</sub>	$\alpha$	$\beta$	SPT ( $N_1$ ) <sub>60CS</sub>	$CRR_{M=7.5}$	CRR	FOS	Conclusion
1.8	SM-ML	14	18.30	8.30	71	0.99	32.94	32.94	32.94	0.15	1.70	1.06	25.23	5.00	1.20	35.27	NA	NA	>1	Non Liquefiable
3.3	SM-ML	15	18.30	8.30	70	0.97	60.39	60.39	60.39	0.15	1.29	1.06	20.46	5.00	1.20	29.55	0.44	0.52	3.44	Non Liquefiable
4.8	SM-ML	18	18.30	8.30	74	0.96	87.84	87.84	87.84	0.15	1.07	1.06	20.36	5.00	1.20	29.43	0.43	0.52	3.43	Non Liquefiable
6.3	SM-ML	10	18.30	8.30	86	0.95	115.29	115.29	115.29	0.15	0.93	1.06	9.87	5.00	1.20	16.85	0.18	0.21	1.44	Non Liquefiable
7.80	SM-ML	13	18.30	8.30	87	0.94	142.74	142.74	142.74	0.15	0.84	1.06	11.53	5.00	1.20	18.84	0.20	0.24	1.64	Non Liquefiable
9.30	SM-ML	26	18.60	8.60	90	0.93	170.64	170.64	170.64	0.14	0.77	1.06	21.10	5.00	1.20	30.32	NA	NA	>1	Non Liquefiable
10.80	SM-ML	30	18.60	8.60	89	0.89	198.54	198.54	198.54	0.14	0.71	1.06	22.57	5.00	1.20	32.08	NA	NA	>1	Non Liquefiable
12.30	SM-ML	29	18.60	8.60	96	0.85	226.44	211.44	213.44	0.14	0.66	1.06	20.40	5.00	1.20	29.49	0.44	0.52	3.71	Non Liquefiable
13.80	SM-ML	26	18.60	8.60	76	0.81	254.34	224.34	226.34	0.14	0.64	1.06	17.61	5.00	1.20	26.13	0.32	0.38	2.67	Non Liquefiable
15.30	SM-ML	27	19.80	9.80	92	0.77	284.04	239.04	241.04	0.14	0.61	1.06	17.54	5.00	1.20	26.04	0.31	0.37	2.66	Non Liquefiable

# Borelogs and Figures

# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

ROB @ CH 7+530  
 BH :4  
 Depth : 30.00m  
 Depth of Water table : 15.30 m

Date of start : 24/03/2021

Date of finish : 26/03/2021



**Project No. 2152**

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc						
				Observed	Corrected	Gravel	Sand	Silt/Clay	r (wet)	r (dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)							
				*	*																			
	0.00																							
	1.00																							
	1.80	SPT	Sandy Silt with Gravel (SM-ML)	7	9	2	13	85	1.82	1.63	11.58	Non Plastic	2.61	DST	0.14	29								
	2.50	UDS																						
	3.30	SPT				12	6	82																
	4.80	SPT																						
	5.50	UDS				2	34	64	1.86	1.64	13.41	Non Plastic												
	6.30	SPT				5	21	74																
	7.80	SPT	Silty Sand with Gravel (SM)	18	18	2	34	64	1.86	1.64	13.41	Non Plastic	2.61	DST	0.14	31								
	8.50	UDS																						
	9.30	SPT				0	12	88	1.90	1.63	16.79	Non Plastic												
	10.80	SPT				0	5	95				Non Plastic												
	12.30	SPT				0	35	65				Non Plastic												
	13.80	SPT				0	85	15				Non Plastic												
	15.30	SPT				0	82	18				Non Plastic												
	16.80	SPT				0	84	16				Non Plastic												
	18.30	SPT				0	77	22				Non Plastic												29 *
	19.80	SPT				0	68	32				Non Plastic												
	21.30	SPT				0	82	18				Non Plastic												
	22.80	SPT		Silty Clay of Medium Plasticity (CI)	33	23	0	82	18								Non Plastic							
	24.30	SPT				0	84	16				Non Plastic												
	25.80	SPT	Sandy Silt with Gravel (SM-ML)	37	24	1	77	22				Non Plastic												
	27.30	SPT				0	70	30				Non Plastic												
	28.80	SPT				0	5	95				Non Plastic												
	29.80	SPT				0	70	30				Non Plastic												
	30.30	SPT				0	5	95				Non Plastic												

\* Based on SPT values

# BORE LOG

**PROJECT: Geotechnical Investigation work for the proposed Greenfield project from Spur to Haridwar**

ROB @ CH 27+120  
BH : 10  
Depth : 30.00m  
Depth of Water table : 15.70 m

Date of start : 03/04/2021

Date of finish : 05/04/2021



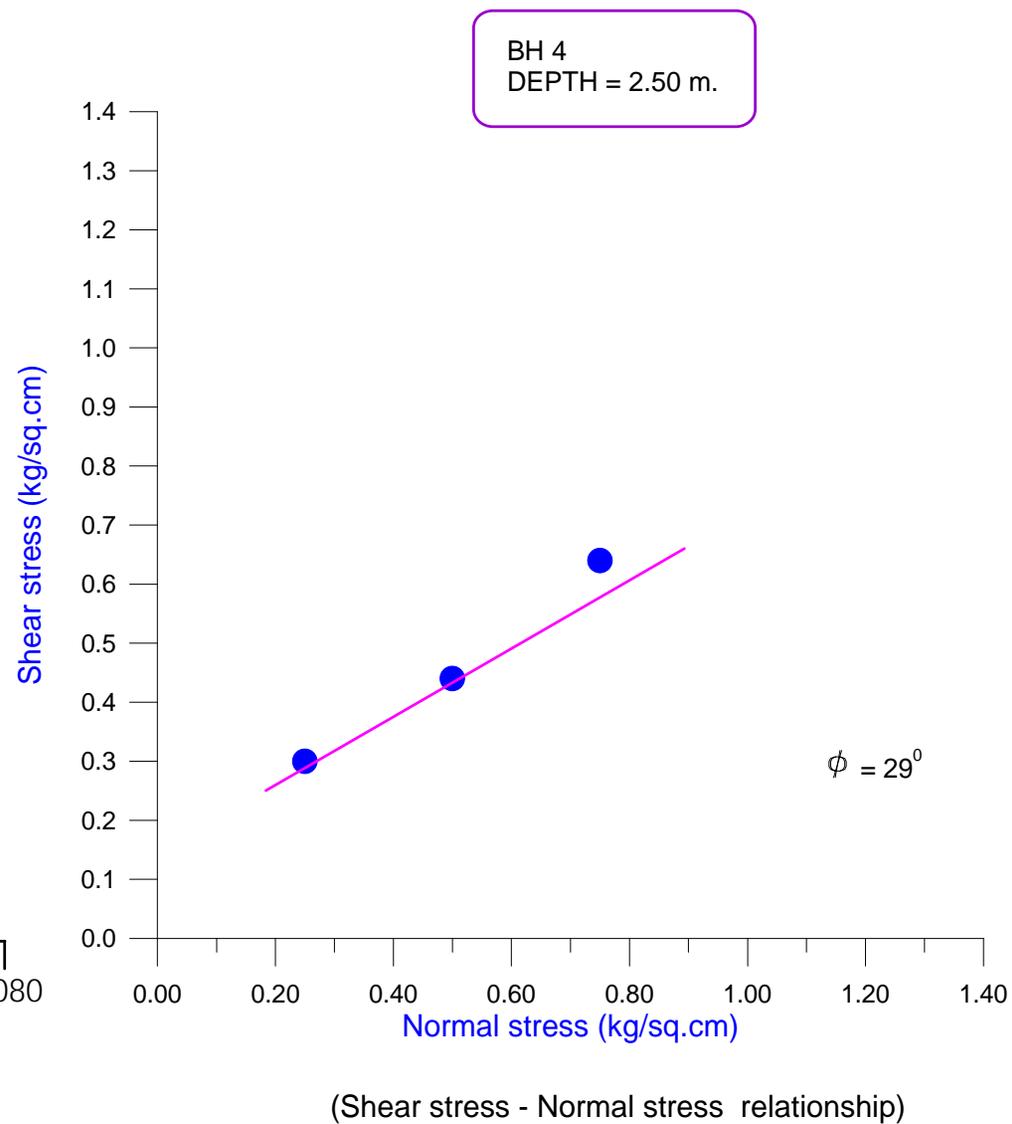
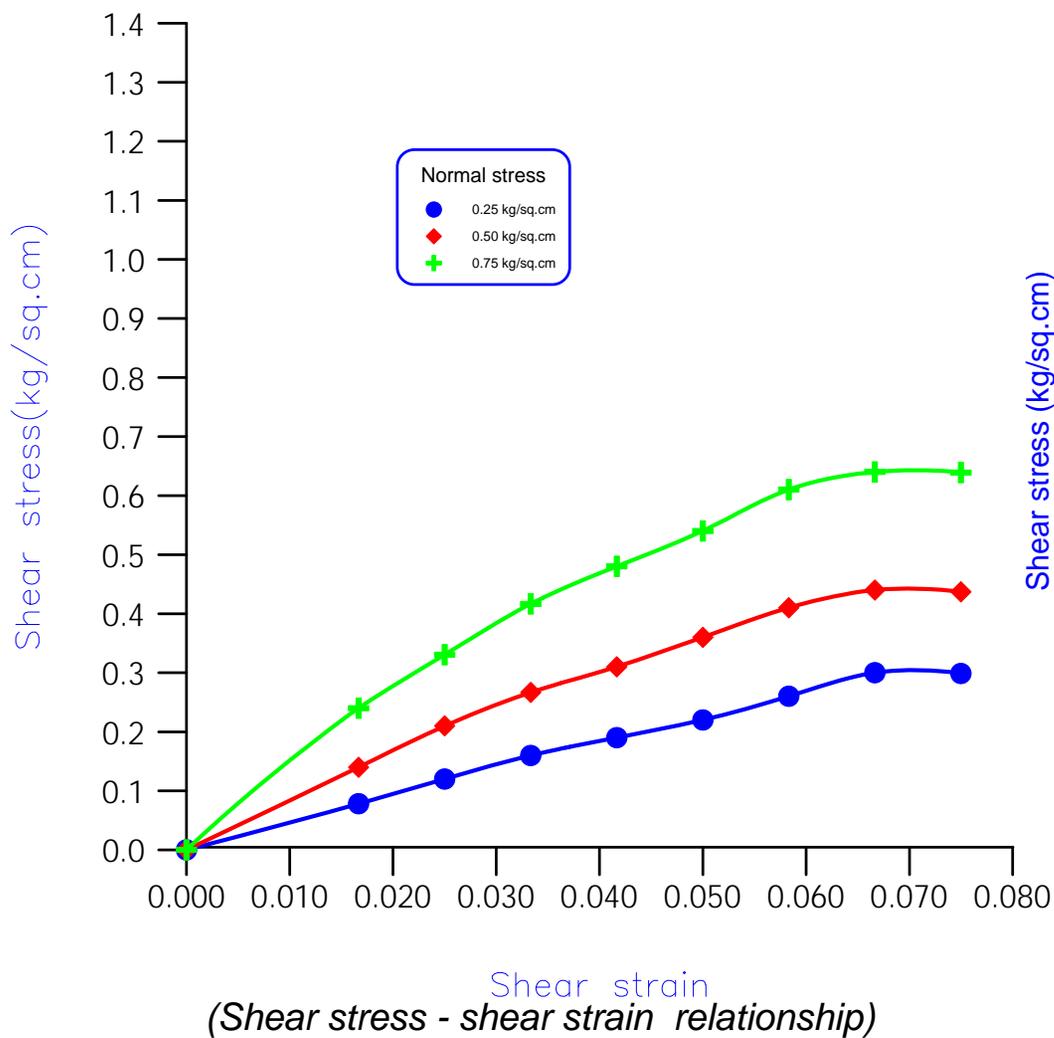
Project No. 2152

Reduced Level	Depth (m)	Type of sample	Soil Classification	S.P.T Plot		Grain size (%)			Density (gm/cc)		W/C	Limits (%)		Sp.Gr	Shear Parameters			Cc	
				Observed	Corrected	Gravel	Sand	Silt/Clay	r (wet)	r (dry)	W(%)	L.L	P.L		Type of test	C(kg/sq.cm)	phi(degrees)		
				✱	✱														
	0.00																		
	1.00																		
	1.80	SPT	Sandy Silt with Gravel (SM-ML)	14	19	0	29	71	1.84	1.67	10.45	Non Plastic	2.61	DST	0.14	30			
	2.50	UDS		15	17	0	30	70				Non Plastic							
	3.30	SPT		18	18	0	26	74	1.83	1.64	11.57	Non Plastic							
	4.80	SPT		10	9	4	10	86				Non Plastic							
	5.50	UDS		13	11	2	11	87	1.83	1.62	12.65	Non Plastic			DST	0.14	31		
	6.30	SPT		26	21	0	10	90				Non Plastic							
	7.80	SPT		30	23	1	10	89	1.85	1.62	14.44	Non Plastic			DST	0.12	30		
	8.50	UDS		29	21	0	4	96				Non Plastic							
	12.30	SPT		26	18	0	24	76				Non Plastic						30	
	13.80	SPT		27	17	0	8	92				Non Plastic							
	15.30	SPT	44	21	0	7	93				Non Plastic								
	16.80	SPT	45	21	0	48	52				Non Plastic								
	18.30	SPT	46	21	0	72	28				Non Plastic								
	19.80	SPT	Silty Sand with Gravel (SM)	46	21	0	72	28				Non Plastic							
	21.30	SPT		38	18	0	82	18				Non Plastic					30*		
	22.80	SPT	42	19	0	44	56				Non Plastic								
	24.30	SPT	Silty Clay of High Plasticity (CH)	46	46	0	2	98				55	28						
	25.80	SPT		49	49	1	4	95							2.10*				
	27.30	SPT	Sandy Silt with Gravel (SM-ML)	36	17	4	7	89				Non Plastic							
	28.80	SPT		45	19	0	6	94				Non Plastic					30*		
	29.00	SPT	Silty Sand with Gravel (SM)	71	26	1	78	21				Non Plastic							
	30.30	SPT																	

\* Based on SPT values

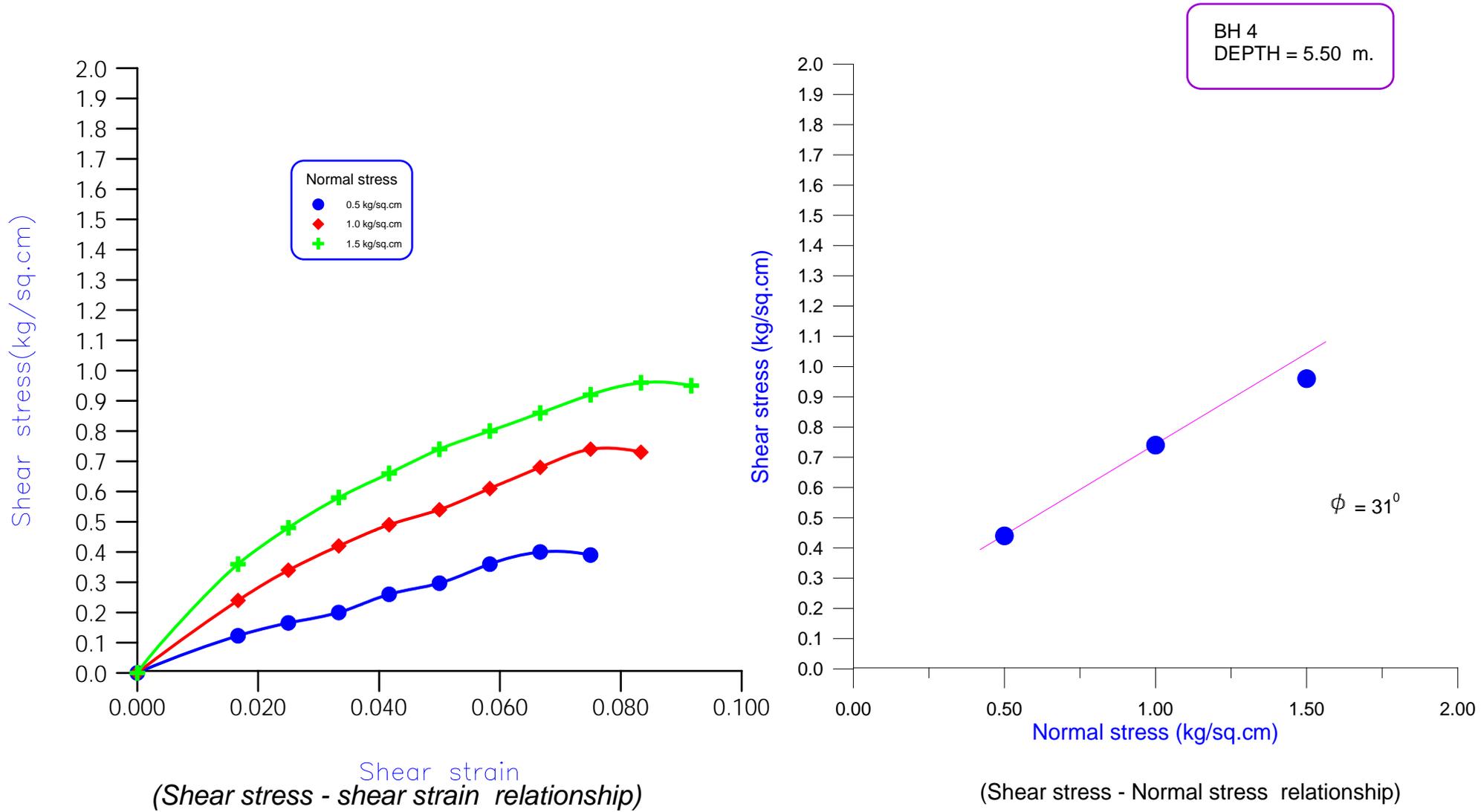
Soil Engineering Constants

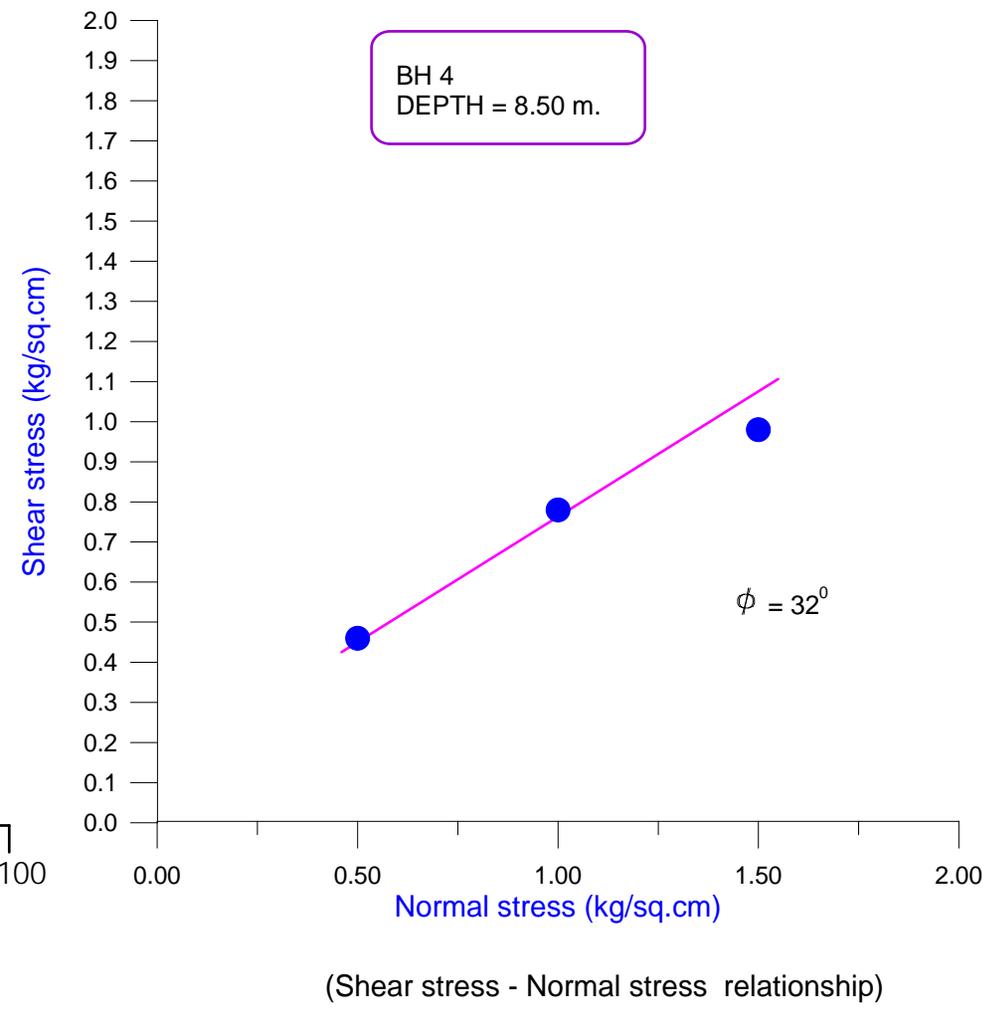
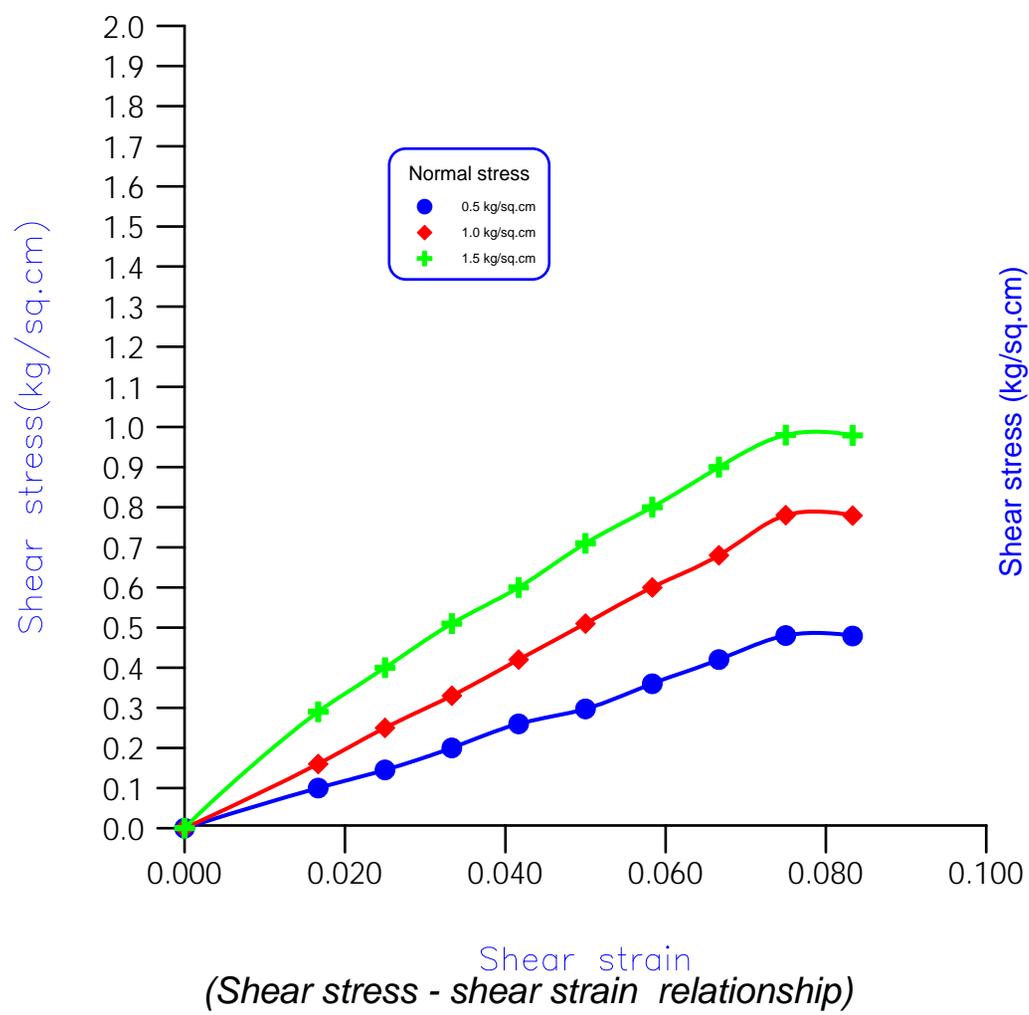
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Soil Engineering Constants

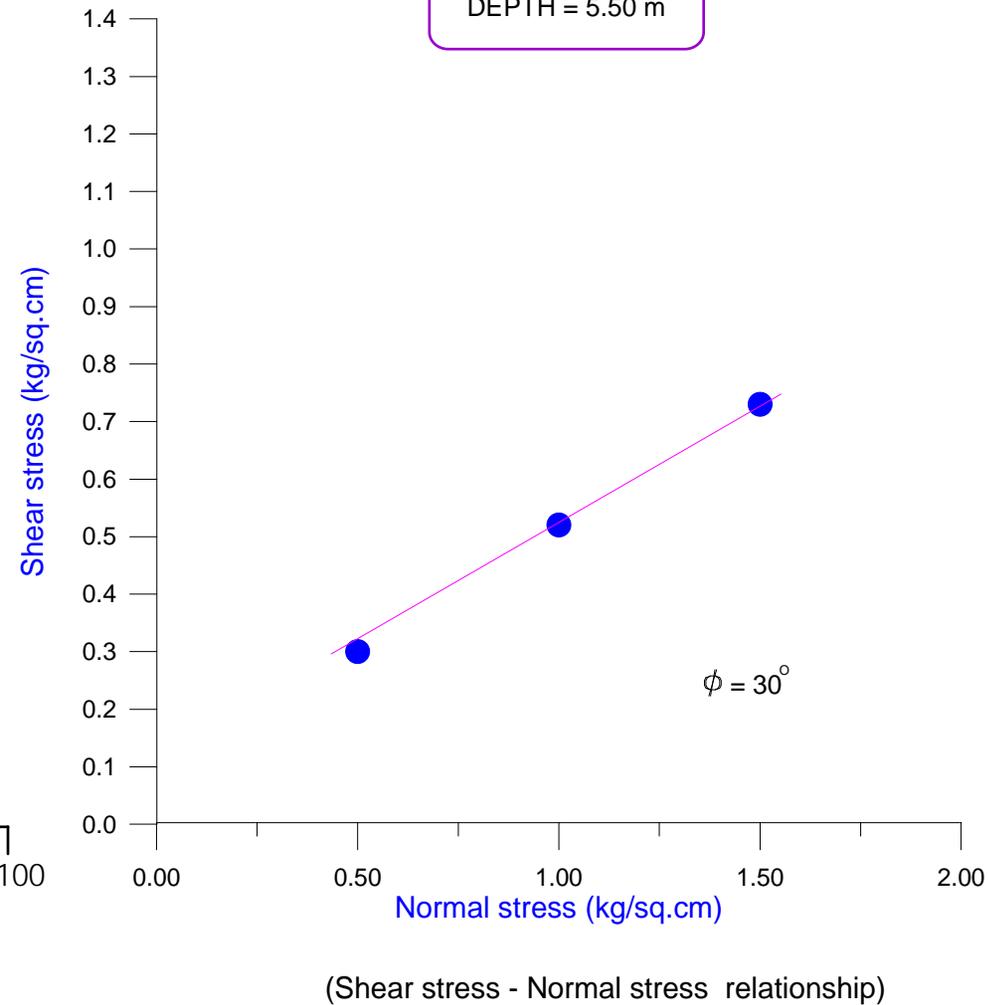
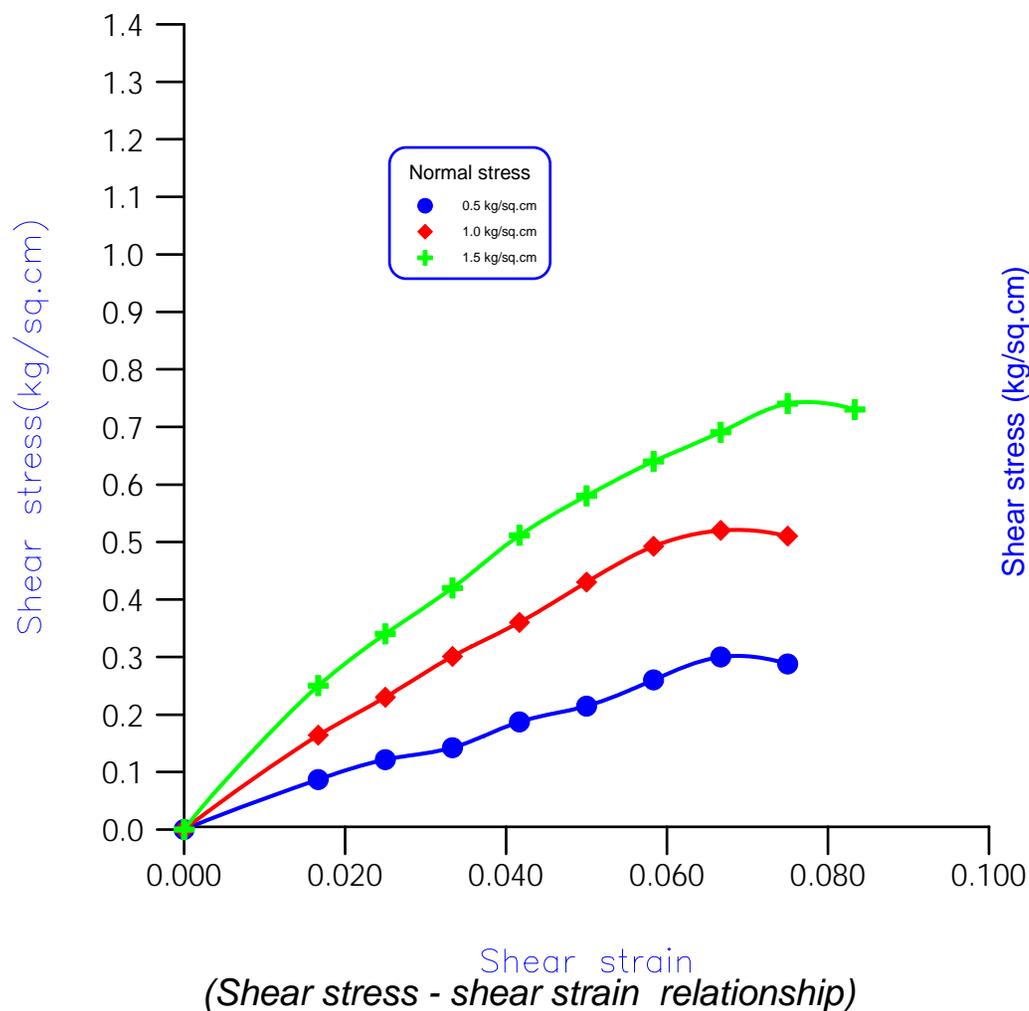
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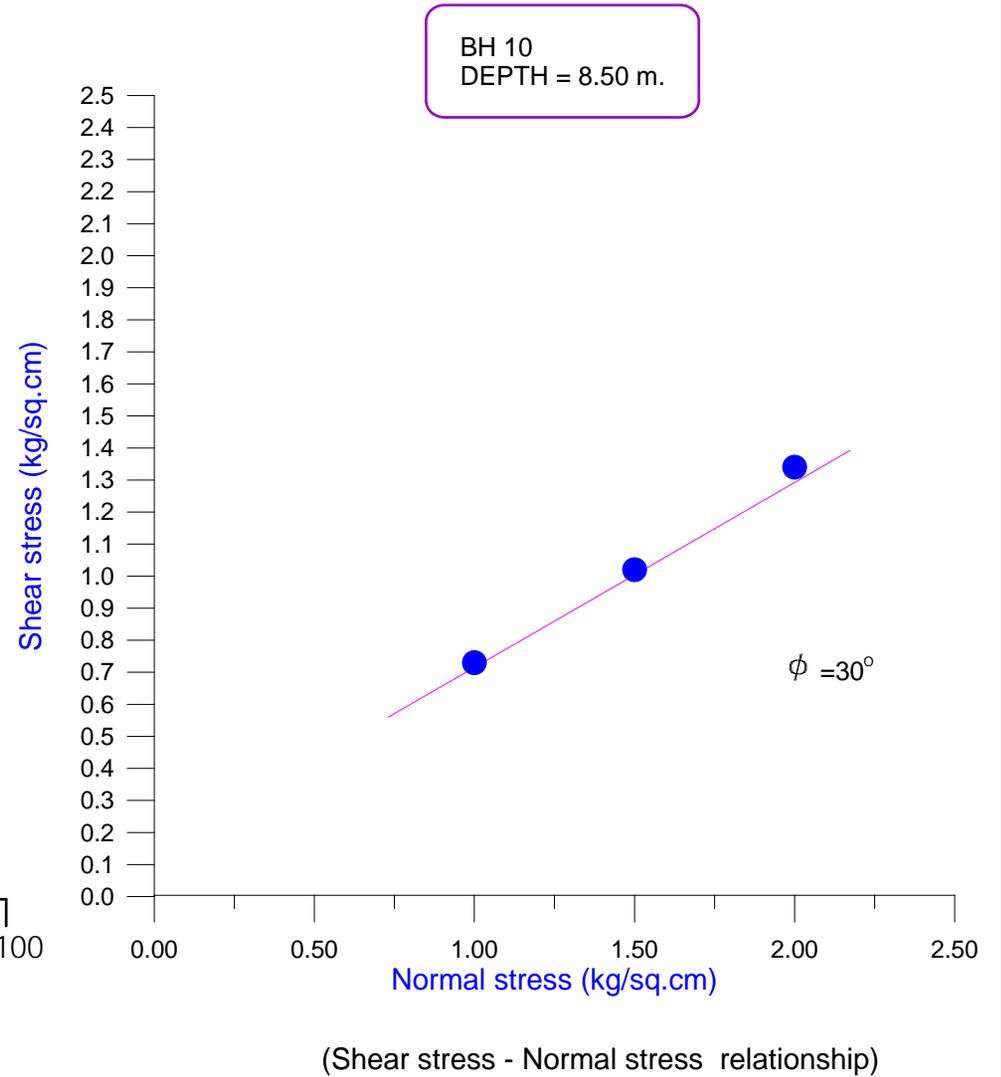
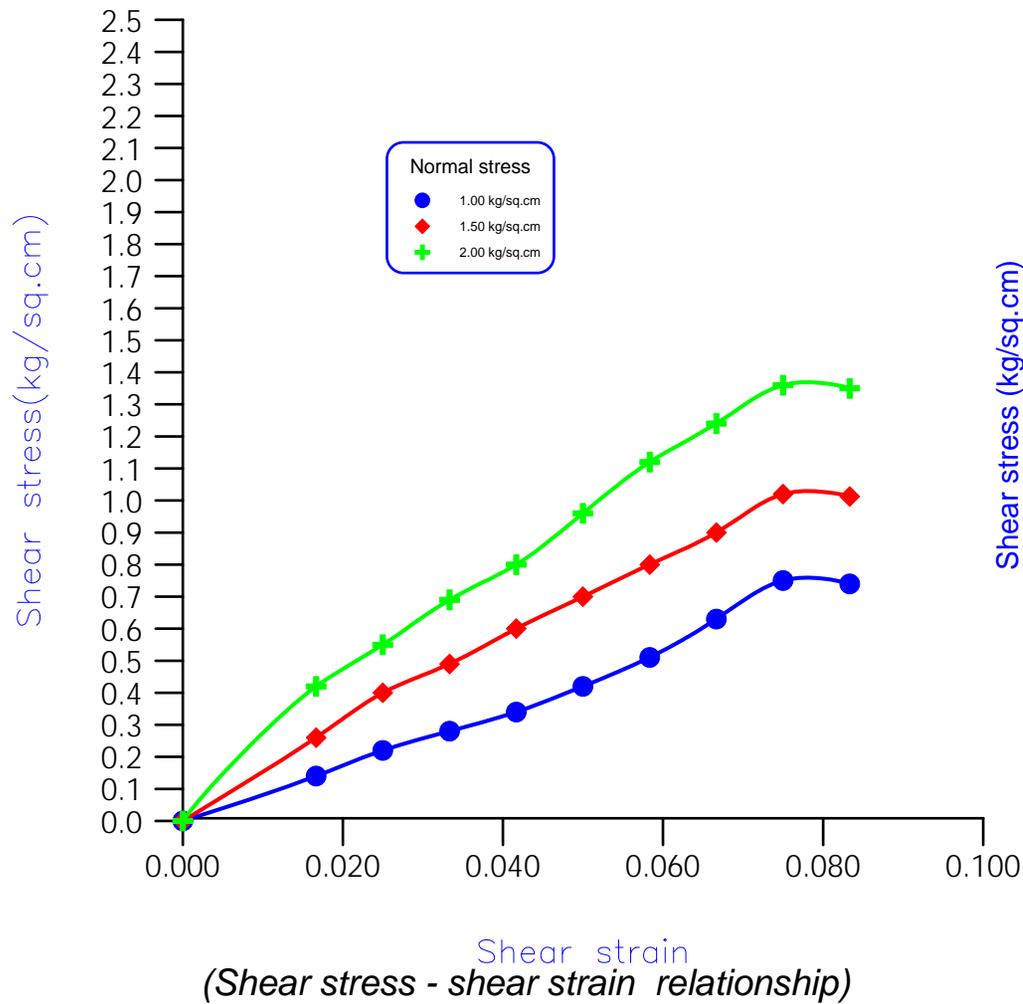


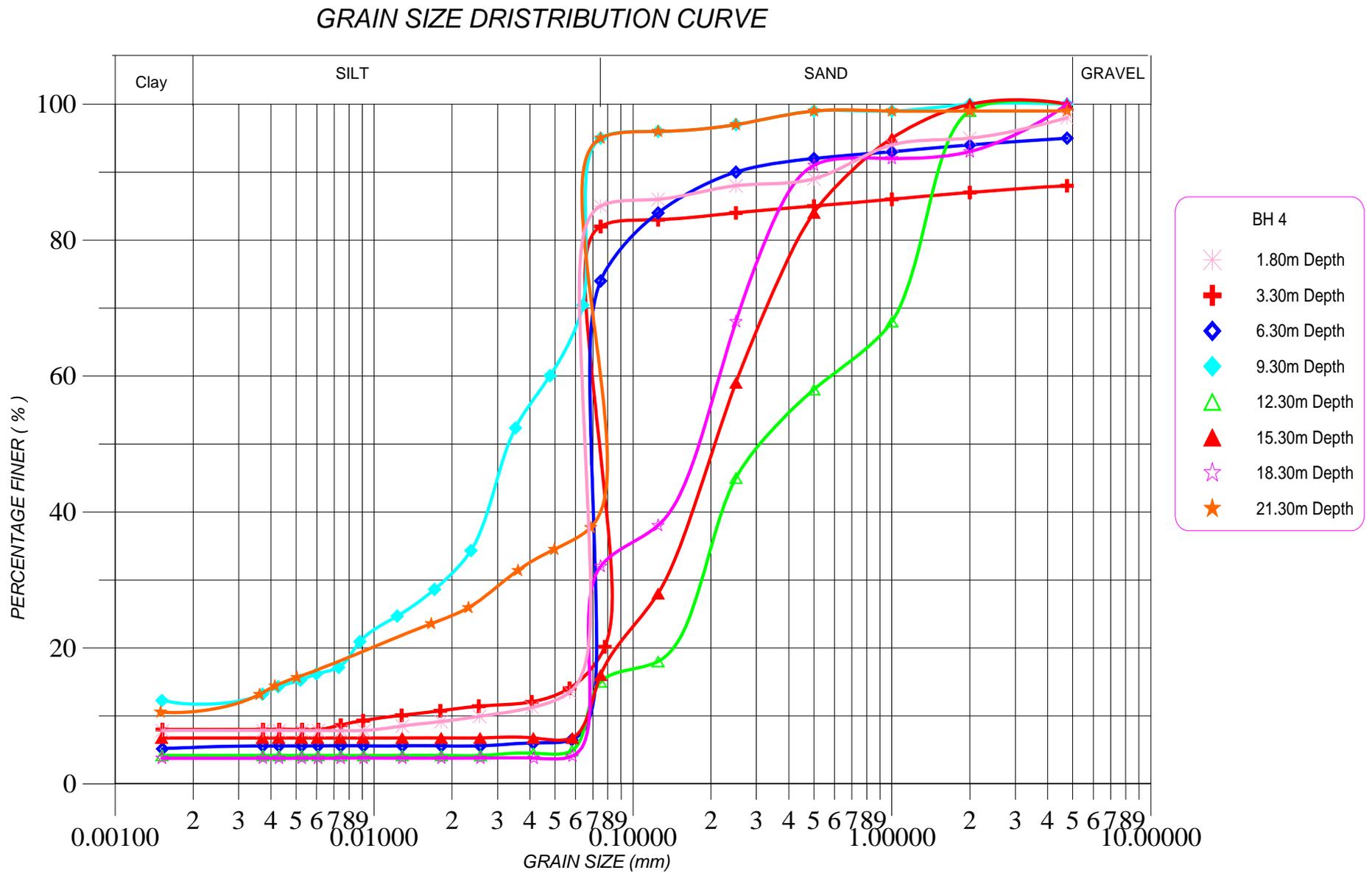


Soil Engineering Constants

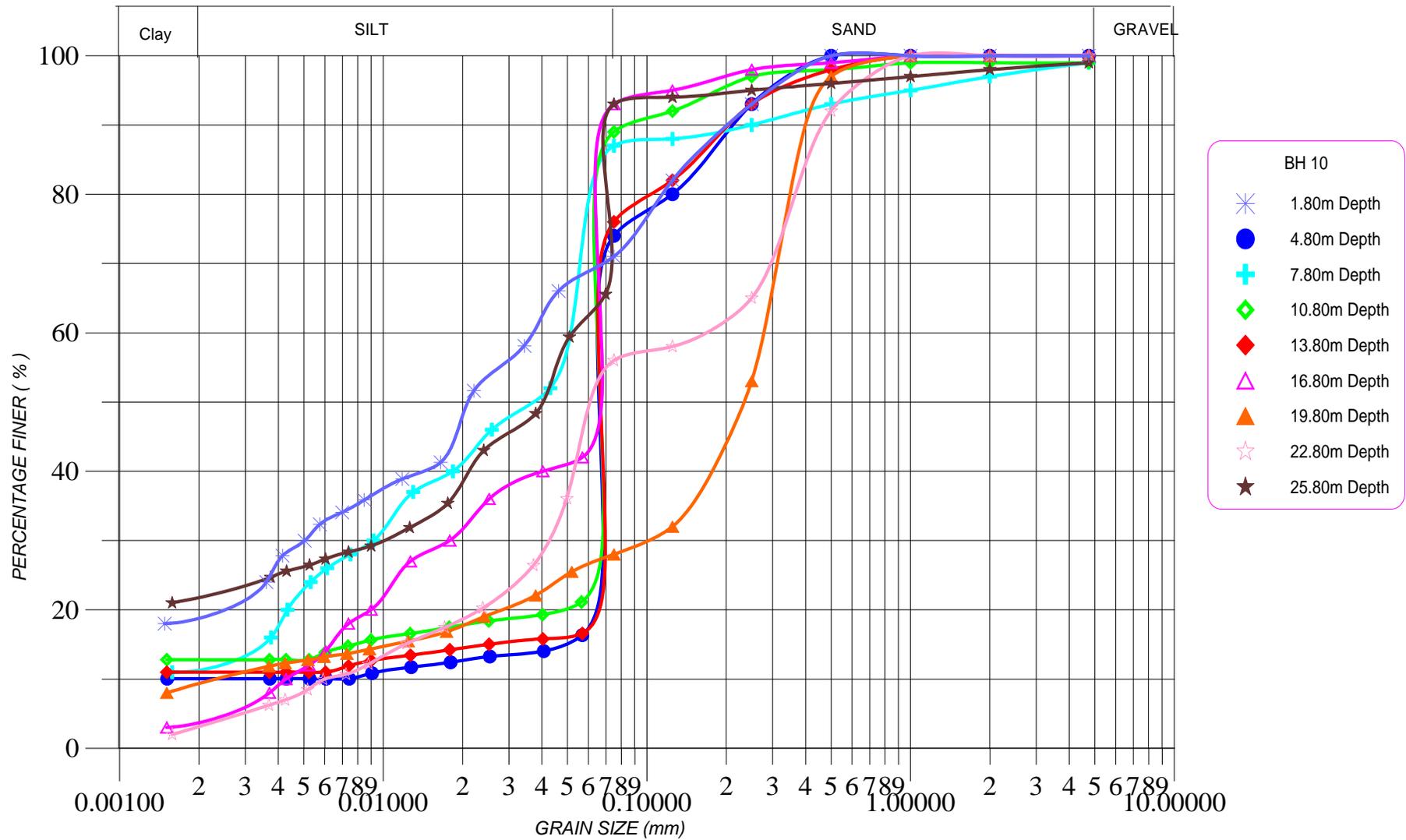
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GRAIN SIZE DRISTRIBUTION CURVE



Annexure VI  
Site Photograph's



ROB @ CH 7+530 BH 4



ROB @ CH 27+120 BH 10

